

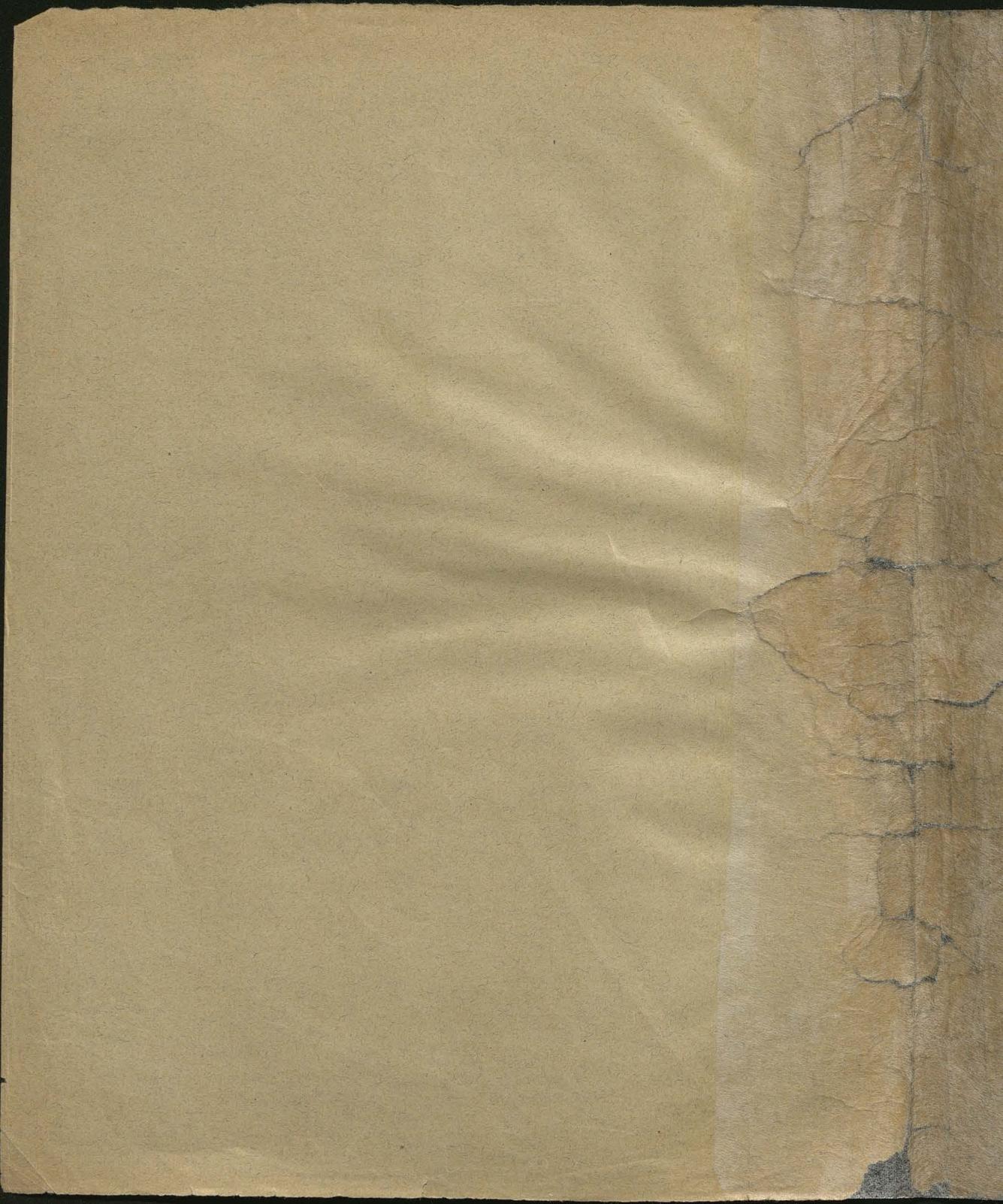
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Bibl. Jap.



Tesnya postimach

bts 1900



## Nerka o potencjale

Jedna z najważniejszych wizji fizyki matematycznej, stworzona wcześniej należąca do matematyki niż do fizyki, bo nie wykorzystana na podstawach ~~do~~ empirycznego poznania praw fizyki, tylko na ogólnych stwierdzeniach prostych i obiektywnie <sup>oddzielnie</sup> (zatem rodzącej geometrii). Tylko ze względu na dodatkowe i po raz pierwszy konieczne, że traktuje się ten przedmiot w fizyce, możliwość oznakowania i objaśnienia poniższej objawy to prawnie całego elektromagnetyzmu i magnetyzmu. ~~Właściwie~~ Podekonomujemy się na przykład tak jak dalej ~~do~~ gromadzone poznania teorię potencjału statycznego całego świata o elektromagnesii. Podeknomymy mogły skorzystać statyczne i statyczno-kwotowe warunki i ~~do~~ potencjał specjalnie zajmował się dynamikią elektromagnetyczną, teorię elektromagnetyzmu światła i optyki.

Nerwa potencjałowa nauka zajmuje potencjał z mechaniki = funkcja kwantowa potencjału = sila. Tylko sila konservatywna może potencjał, reprezentującą (tarcia, opór órzałek itd.) nie moga. Jeżeli sila mówią o teorii potencjału, to sila rozwinięta jednak specjalnie sily typu Newtonowskiego  $\frac{1}{r^2}$  nazywa potencjałem Newtonowskim [przez tego jenku nazywam tzw. potencjałem hydrostatycznym].

Wybrane przez Lipperta, ~~W. Grossa~~, nerwa wprowadzone przez Greena.

Gauss

Clausius, Dirichlet,  $\rho = 8\pi r^2 \sigma^2$  - Korn

Riemann, Mercart-Jacob, Maxwell, Lamé, Helmholtz,

### Testos orane:

w grawitacji  $f = \frac{m_1 m_2}{r^2}$

w elektrostatyce hipoteza Coulomba  $f = \frac{q_1 q_2}{r^2}$

Tenże jednak te różnice nie brzmiały przesądnie, lecz wydawały się zbyt małe aby m.

Na tą hipotezę nikt się wybudował z tego elektrostatyki.

Podobna hipoteza pojawiała się wówczas w fizyce magnetycznej  
ale tyleż nikt nie ją rozwinął do konklamacji, iż mimo to robiła sens.

2 jednego końca + 2 drugiego równie male. Ale Wyszło to jednak tak, iż się objęły dwie te Newtonowskie t.j. dwie potencjały. Ich jasne nie były tunc.

Helmholz mianiąc podzielił hydrodynamiczną h. nuklearną na dwa (potencjały)

i rotacyjną. Tannenfeld w pracy wykazał potencjały hydrodynamiczne z dodatkowymi równaniami  $\frac{\partial \psi}{\partial r} = 0$  na które natychmiast wrócił w tworząc pot. t. i. w tym

tego do przeprowadzonej siedmiu analogii mimo to kochał elektrostatyk.

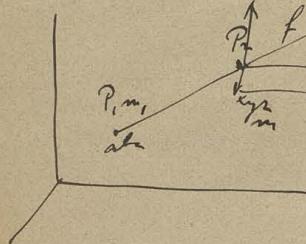
Dziwne się to wydaje, my mówimy jakieś skarby tunczące zasiek? Ale podobni pionierzy są akustycy, przewodnicy elekt. itp. Nasze poznawanie mianowicie tunc

wektora i quaternionów dopiero wyraźnie pokazyły te analogie, w których których w różnych dziedzinach fizyki te same prawo Newtonowskie  $\frac{d}{dt}$  i te same tuncze potencjały zachowały się mimo, że leżały na odrębnych ośrodkach funkcyjnych przestrzennych.

~~Wszystko~~ Pokazują się tu kiedy takie funkcie t.j. jakieś funkcje całkowite (funkcje całkowite) w przestrzeni np. itp. itp. itp. mówiąc robią w 2 rzeczach (tak samo

3

zak hydrodyn. sive i miaz) z krych jeho zaly o Newtonovce plyn  
a druge o t.m. potreby viktorova. Tyc mi jut to prepadek, i many  
tak rysy o fyzie o rytadku - 2, když ~~zlatka~~ polya to nazcasni pridne  
zlaty, tedy neni vlastnosti mina zlatova, jen vlastnosti vodice když mazne  
tak jimi aranji. Hl. býzí rozumění zlatka bývají v základním  
interpretaci dynamického mazání elektrostatisky, pouze i maz představují  
býzí základ obstrukce. Tyc recenzejší ab ovo:



$$f = \frac{q_1 q_2}{r^2}$$

Elektrostat. maz. jich gravit. kruž.

$$X = f_{x1} x$$

$$r^2 = (x_2 - x_1)^2 + \dots$$

$$X = \frac{q_1 q_2}{r^2} \frac{x - x_1}{r}$$

$$\frac{x_2 - x_1}{r} = \omega x \dots$$

$$Y = \frac{q_1 q_2}{r^2} \frac{y_2 - y_1}{r}$$

$$Z = \dots$$

$$r = \sqrt{(x_2 - x_1)^2 + \dots}$$

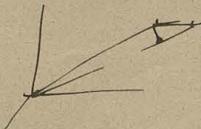
Tak funkce je:

$$U = \frac{q_1 q_2}{r} \quad \text{to maz je } X = -\frac{\partial U}{\partial x} \text{ at.}$$

$$\text{Zatímco: } -\frac{\partial}{\partial x} \left[ \frac{q_1 q_2}{\sqrt{(x_2 - x_1)^2 + \dots}} \right] = +\frac{q_1 q_2}{r} \frac{1}{\sqrt{3}} = \frac{q_1 q_2}{r^2} \frac{x - x_1}{r}$$

(Kterou zde rovnice znamená, že  $\frac{\partial r}{\partial x} = \omega x$  at.) Lze prodat do to maz  
přesnou vlnkovou fází  $x$  a maz mazání:

$$\text{Vzdály: } \frac{\partial U}{\partial x} = \frac{dU}{dr} \frac{\partial r}{\partial x} = \dots$$



Tak samy  $Y = -\frac{\partial U}{\partial y}$  at. maz symetrii i pouze u volej termink  
mi XY2 jut doloženy [to bylo f.(r)] to volej  $F = -\frac{\partial U}{\partial s}$

$\text{Tr} \text{ w} \text{ p} \text{acy} = \sum \text{ ilo} \text{znych} \text{ z} \text{ s} \text{ty} \text{ d} \text{ek} \text{t} \text{oj} \text{c} \text{y} \text{ u} \text{ kierunku dr} \text{u} \text{f} \text{ i} \text{ z} \text{ } \text{d} \text{u} \text{p} \text{r} \text{y} \text{ d} \text{r} \text{u}$

$$\begin{aligned} & \int f \cos \varepsilon \, ds = \int (k_x dx + k_y dy + k_z dz) \, ds = \\ & = \int f \, dr = \sqrt{\left(\frac{dx}{ds}\right)^2 + \left(\frac{dy}{ds}\right)^2 + \left(\frac{dz}{ds}\right)^2} (U_2 - U_1) \\ & = \int -\frac{\partial U}{\partial s} \, ds = (U_1 - U_2) \quad \text{w} \text{y} \text{e j} \text{u} \text{l} \text{ punkt} \, 1 \text{ i} \, 2 \text{ m} \text{u} \text{z} \text{ u} \text{z} \text{lo} \text{m} \end{aligned}$$

to one inzdby od kierunku dru mody masy, przyjmujac do samego wektora gely punkt docelny i to same położenie (jedna o tylu dozwolonej dla razy)

z tego nowa definicja funkcji potencjalnej:

Jedn punkt powzduj do niskiego poziomu:  $P = U_1 - U_\infty$

~~zakladajac~~ Jeli jedna wartość U przypada to jeli innemu w celu przeniesienia wtedy punkt  $U_\infty = 0$  wtedy  $P = U_1$ . A j.:  
punkta pot. (= masy wykorzystanej dla jeli <sup>masy m</sup> oddeleg. z 2 masy do niskiego poziomu) jakiej bedzie drode

Jaka krytyczna jest praca? Dajmy jeli masy mas

$$X = \frac{m_1 m_1}{r_1^2} \frac{x - x_1}{r_1} + \frac{m_2 m_2}{r_2^2} \frac{x - x_2}{r_2} + \dots = \sum_m \frac{m_m (x - x_m)}{r_m^3}$$

$$Y = \frac{m_1 m_1}{r_1^2} \frac{y - y_1}{r_1} + \dots$$

$$Z = \dots$$

$$\begin{aligned} X &= -\frac{\partial}{\partial x} \left( \frac{m_1 m_1}{r_1^2} \right) + -\frac{\partial}{\partial x} \left( \frac{m_2 m_2}{r_2^2} \right) + \dots = -\frac{\partial}{\partial x} \left[ \frac{m_1 m_1}{r_1^2} + \frac{m_2 m_2}{r_2^2} + \dots \right] \\ &= -\frac{\partial}{\partial x} [U_1 + U_2 + \dots] \end{aligned}$$

first mesy urodzone w ciekaj rastni za porownanie

4

$$U = k \int \frac{G \cdot dS}{r} \quad \delta = \rho \cdot \sigma$$

$$U_1 = \frac{4\pi k \rho}{3} \left( \frac{A^3 - a^3}{2} \right) \frac{1}{r}$$

$$r = A : \quad U_1 = U_2$$

$$U_2 = \frac{4\pi k \rho}{3} \frac{A^3 - a^3}{2} + 2\pi k \rho (A^2 - r^2)$$

$$r = a : \quad U_2 = U_3$$

$$U_3 = 2\pi k \rho (A^2 - a^2)$$

$$\begin{aligned} \frac{\partial U_1}{\partial r} &= -\frac{4\pi k \rho}{3} \frac{A^3 - a^3}{r^2} \\ \frac{\partial U_2}{\partial r} &= k \rho \left( \frac{4}{3} r - \frac{4}{3} \frac{a^3}{r^2} \right) \\ \frac{\partial U_3}{\partial r} &= 0 \end{aligned}$$

It's k w dolnych wzg slaski = 1

przyjmijec je jednothe mas w odnosci zysk dobrane

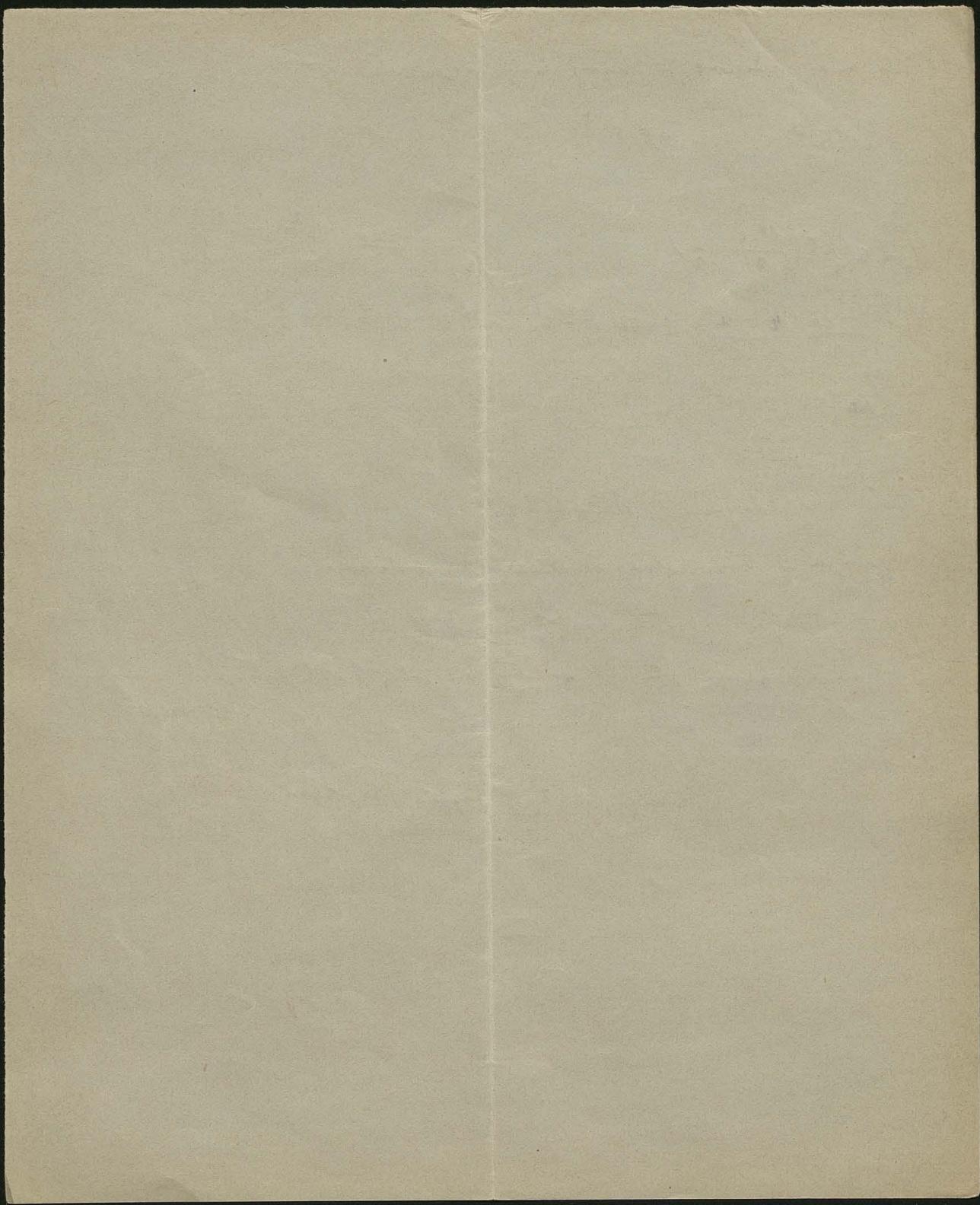
M.p.w elektryczne : niski startowy

w granicy innego systemu, zatem ten nalicz ty stale rozwijajac, wynosi

$$k = 0.0000000648$$

szybkość startowa k = 1

trudno zamiast g pugge jaka jidlowi 15.430 kg



$$\text{Wzr. } X = -\frac{\partial U}{\partial x}$$

$$U = \sum u_i +$$

funkcja pot. pozwala dodziaływać aby styczne i wypadkowa były

$$\text{też sam: } Y = -\frac{\partial U}{\partial y} \text{ at.}$$

To staje się szczególnym wearem jakaś wile punktu

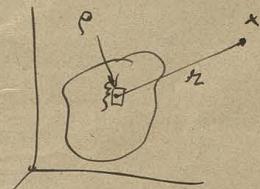
Dajmy na to znamy isolatora w którym wypadkowe siły elektromagnetyczne (admi) i grawitacyjne [jakiże masy ten wytworzony bimis kątym], obie masy

$$\rho = \rho_0 \cdot \rho_{\text{stoc}}$$

$$m_1, m_2, \dots = \rho_0 \rho \Delta v$$

wysokość powstająca:

$$X = \sum \frac{m \rho \Delta v}{r^2} \frac{x - \xi}{r}$$



$$X = m \int \frac{\rho(x - \xi)}{r^3} dv \quad \text{przyjmując hyponezm równe}$$

$$Y = m \int \frac{\rho(y - \eta)}{r^3} dv \quad \text{wtedy powstaje rezultat } X = -\frac{\partial U}{\partial x} \dots$$

$$Z = \sum u_i + = m \int \frac{\rho dv}{r}$$

wysokości masy powstające której jest konieczne aby system, nie jakaś całkowita, podnosiła się do masy powstającej proporcjonalnie do całkowitej i to do tego stopnia stopniowo, a chęć masy wykonać istotny krok do

$F$  skutek tego zauważmy  $\frac{\partial U}{\partial x} = f_{\text{nat}} - f_{\text{nat}}$ , podnoszącą natomiast  $F = w$  dającą normę  $= -\frac{\partial U}{\partial x}$

$$\frac{\partial U}{\partial x} = \left( \frac{\partial U}{\partial x} \frac{dx}{ds} + \frac{\partial U}{\partial y} \frac{dy}{ds} + \frac{\partial U}{\partial z} \frac{dz}{ds} \right) = f_{\text{nat}} - f_{\text{nat}} = f_{\text{nat}}$$

$$\text{Z tego żelazna wypatrywanie w postaci } P = - \int \frac{\partial U}{\partial s} ds = U_1 - U_2 \quad \text{wysokość powstającej}$$

wysokości jakaś to sam zatem żelazna postać  $U_1 = 0$  to funkcja pot. grawitacyjna

$= \text{postac}$

Als to same process that sometimes it may happen that, opposite to our originality  $F$ , magnitude of force  $m$  is not known up to 1.

To move under condition that we can't determine deflection function  $\varphi$  which has to be in such a manner defined, <sup>Chandrasekhar's method</sup> consider <sup>deflection function</sup>  $P_1$  and  $P_1'$  which satisfy  $P_1 - P_1' = \frac{F \Delta s}{m}$

$$P_1, P_1' \text{ steady state } P_1' = \frac{F \Delta s}{m}$$

$$\text{then } F \Delta s = \frac{P_{1'} - P_{1'}}{m} = U_1 - (U_1 + \Delta U)$$

$$F = \frac{\Delta U}{\Delta s} = \frac{\Delta U}{\Delta s}$$

With this we can't yet determine  $P_1$  and  $P_1'$  since we have to satisfy  $P_1 - P_1' = \frac{F \Delta s}{m}$  and  $P_1 - P_1' = \frac{F \Delta s}{m}$ . But if  $\theta = \text{constant}$  then we have to satisfy

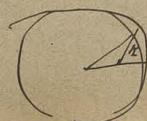
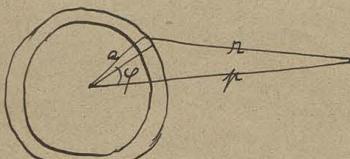
$$m = \frac{\partial dF}{\partial r} \quad \text{where} \quad U = \int \frac{\partial dF}{\partial r} \quad \begin{aligned} & \text{Added by taking moments about center} \\ & \text{mass distribution} \\ & \text{Satisfy from left boundary angle to } d\theta = 0 \quad \text{at } F = \infty \quad \text{at } V = \infty \end{aligned}$$

Then product of moment to  $d\theta = r^2 d\theta dr$

$$\frac{d\theta}{r^2} = d\theta dr \quad \text{we know } d\theta \propto$$

$$\therefore M \cdot V = \int \frac{d\theta}{r^2} r^2 dr = \infty$$

Mass rotation or rotation bullet is not circular



$$\begin{aligned} U &= m \int \frac{2\pi a^2 \sin \varphi d\varphi}{r} \rho dr = m \cdot 2\pi a^2 \int \frac{\sin \varphi dr}{\sqrt{a^2 + r^2 - 2ar \cos \varphi}} \\ &= m \frac{\rho a^2}{r} \int_{r_0}^{r_0 + 2a \cos \varphi} \frac{-2a \sin \varphi dr}{\sqrt{a^2 + r^2 - 2ar \cos \varphi}} = m \frac{\rho a^2}{r} \left[ 2 \sqrt{a^2 + r^2 - 2ar \cos \varphi} \right]_{r_0}^{r_0 + 2a \cos \varphi} \\ &= \frac{2m \rho a^2}{r} [(a + r) - (a - r)]_{\text{ext.}} = \frac{4a^2 m \rho}{r} \\ &= \frac{2m \rho a^2}{r} [(a + r) - (a - r)]_{\text{int.}} = 4am \rho a \end{aligned}$$

Przy tym  $\frac{4\pi r^2 \rho}{2} = \text{całkowite mase} = M$

$$U_{ext} = \frac{Mm}{r}$$

$U_{int} = \frac{Mm}{a}$  wtedy dla punktu zewnetrznego tak jak gdyby cała mase skoncentrowana w środku, wtedy sila  $F = -\frac{Mm}{r^2}$

dla punktu zewnetrznego  $F=0$ , ponieważ potencjał = stały

[czyli gdyby przyjąć dalsze rozważanie, że dalej od punktu masy nie znajdują się żadne inne punkty]

że tego utrzymuje się bezwzględnie wyrażenie dla kuli stały pełnej

$$\textcircled{O} \quad U_{int} = \int \frac{4\pi r^2 \rho}{r} f dr = \frac{4\pi \rho}{r} \left[ \frac{r^2}{2} \right] = \frac{Mm}{r}$$

co natomiast bezpośrednio prowadzi do wyniku wyżej

To jest wzroszczenie tego w wewnętrznych itd. masy mówiąc inaczej jako położenie w środku planety itd. [Dla kuli to nie jest warunek powstania właściwego potencjału, ale jedynie warunek dla prawidłowej pracy i istnienia procesów i reakcji] tak samo w lekkim momencie, kiedy zauważymy, że kula ma średnicę Coulomb'a i to dla spowodowania, aby ~~do~~ spowodować  $\frac{m^2}{r^2}$

To ostatni fakt nie całkiem jest do tego, aby robić ją jakąkolwiek masy, ale tylko w tych doświadczeniach daje masy masy i masy da się masy masy, o co mówiąc masy.

$$\textcircled{O} \quad U_{int} = m \int_a^R 4\pi r^2 \rho dr = m 4\pi \rho \frac{R^2 - a^2}{2} = m \cdot 2\pi \rho (R^2 - a^2)$$

$F=0$  nie da się wyrazić powszechnie

jeśli ten punkt leży w odległości  $a$  od  $O$  w kierunku  $\vec{F}$ :

$$8) U = \left[ \frac{4\pi\rho}{3} \frac{r^3 - a^3}{r} + 2\pi\rho (A^2 - r^2) \right]_a$$

$$= m\pi\rho \left[ 2A^2 - \frac{2}{3}r^2 - \frac{4}{3} \frac{a^3}{r} \right]$$

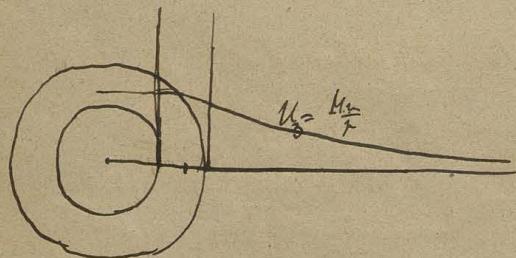
$$\frac{\partial U}{\partial r} = - \frac{\partial U}{\partial r} = m\pi\rho \left[ \frac{4}{3}r - \frac{4}{3} \frac{a^3}{r^2} \right]$$

jeli  $a=0$  tole pole

trybował nasz działy my matematyczne

$$= m \cdot \frac{4}{3} \frac{\pi\rho r^3}{r^2}$$

Przyjęty po przedstawiony w obu grafach:



$$U_2 \Big|_{r=A} = m \frac{4\pi\rho}{3} \frac{A^3 - a^3}{A} = \frac{Mm}{A} = U_1 \Big|_{r=a}$$

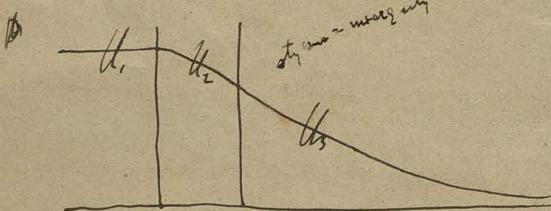
$$U_2 \Big|_{r=a} = m 2\pi\rho (A^2 - a^2) = U_1$$

$$\frac{\partial U_2}{\partial r} = - \frac{Mm}{r^2}$$

$$\frac{\partial U_2}{\partial r} = m\pi\rho \left[ -\frac{4r}{3} + \frac{4a^3}{3r^2} \right]$$

$$r=A : = m\pi\rho \frac{4}{3} \frac{a^3 - A^3}{A^2} = \frac{\partial U_2}{\partial r}$$

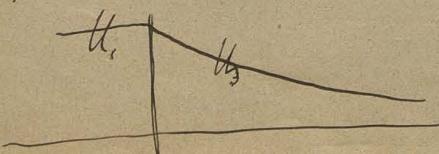
$$r=a : m\pi\rho [0] = 0 = \frac{\partial U_1}{\partial r}$$



$$\frac{\partial U}{\partial r} \text{ toki}$$

więc  $U$  jest funkcja wglębia

Ten rezultat pokazuje, że masy skoncentrowane na powierzchni, bo stąd grawitacji wewnątrz  $U=0$  wtedy zmiana  $U$  będzie wglębiała się do niejże



wyjąco to toki bezpośrednio z odniesieniem  
do samej

$$U_{ex} = m \frac{4\pi^2 n^2}{r}$$

9

7

$$r=\infty : U_e = U_i$$

$$U_{int} = m \cdot 4\pi n^2$$

$$\text{de } \frac{\partial U_e}{\partial r} = -m \cdot 8\pi n^2$$

$$\text{tym sam } \frac{\partial U_i}{\partial r} = 0$$

Jest to oznaczenie pozytywnego boku gilnego równania  $\frac{\partial U_e}{\partial r} + \frac{\partial U_i}{\partial r} = -4\pi n^2$   
które powinno powstawać

Jest to jedno złożone bardziej skomplikowane:

$$\frac{\partial U}{\partial x} + \frac{\partial U}{\partial y} + \frac{\partial U}{\partial z}$$

$$U_{ex} = \frac{M}{r} = \cancel{M}$$

$$\frac{\partial U}{\partial x} = -\frac{M}{r^2} \frac{x-a}{r}$$

$$\frac{\partial U}{\partial y} = \cancel{M} \frac{\frac{3}{r^3} \frac{(x-a)^2}{r^2} - \frac{1}{r^3}}{r^3} \quad \left. \begin{array}{l} \\ \end{array} \right\} \Sigma = 0 \quad [\text{Równanie Lektor}]$$

$$\frac{\partial U}{\partial z} = \cancel{M} \frac{\frac{3}{r^3} \frac{(y-b)^2}{r^2} - \frac{1}{r^3}}{r^3} \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{Tak samo naturalnie } U_z$$

$$\frac{\partial U}{\partial z} = \cancel{M} \frac{\frac{3}{r^3} \frac{(z-c)^2}{r^2} - \frac{1}{r^3}}{r^3}$$

$$\text{A więc } U_2 = U_2 = \cancel{M} \rho \left[ 2A^2 - \frac{2}{3}(x+y+z^2) - \frac{4}{3} \frac{a^3}{r^3} \right]$$

$$\frac{\partial U_2}{\partial x} = \cancel{M} \rho \left[ -\frac{4}{3}x + \frac{4}{3} - \cancel{\frac{\partial^3}{\partial x^2} \frac{\partial}{\partial x} \left( \frac{1}{r} \right)} \right]$$

$$\frac{\partial^2 U_2}{\partial x^2} = \cancel{M} \rho \left[ -\frac{4}{3} + \frac{4}{3} \frac{2}{r^2} \frac{2}{r^2} \left( \frac{1}{r} \right) \right]$$

$$\Sigma = -4\pi \rho + \frac{4}{3} a^3 \left( \frac{2}{r^2} + \frac{2}{r^2} + \frac{2}{r^2} \right) = -4\pi \rho \quad [\text{Równanie Pionów}]$$

Oznaczenie tzw. równanie Lektorów w nim jest zawarte jako oznaczenie pozytywnego boku gilnego tym samym tylko dodatkowy tyc dla kuli, ale zatem zawsze jest to ogólny rezultat i  $\nabla^2 U = -4\pi \rho$

10

Do ~~zadania~~ do nas, które mamy do końca,

$$U = \sum \rho \frac{\Delta v}{r} = \int_{\alpha}^{\beta} \rho d\varphi dy dz$$

$$\alpha \sqrt{(y-\varphi)^2 + (y-y_1)^2 + (y-2)^2}$$

$$\frac{U' - U}{\Delta x} = \int_{\alpha}^{\beta} \rho d\varphi dy dz \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$\frac{\partial U}{\partial x} = \int \rho dv \frac{\partial(\frac{1}{r})}{\partial x}$$

$$\frac{\partial U}{\partial x} = \int \rho dv \frac{\partial(\frac{1}{r})}{\partial x}$$

$$\frac{\partial U}{\partial y} = \int - \frac{\partial(\frac{1}{r})}{\partial y}$$

$$\frac{\partial U}{\partial z} = \int - \frac{\partial(\frac{1}{r})}{\partial z}$$

$$\left. \begin{aligned} \nabla U &= \rho dv \left( \frac{\partial}{\partial x} - \frac{\partial}{\partial y} \right) \\ &= \end{aligned} \right\}$$

Gdy punkt leży wewnątrz sfer, to tą mówimy symetrii, bo nie tylko wokół takie granice, i to wewnątrz której deje maksimum prędkości

Ogólne prawo do różnicowania po czasie całkowite:

Zróżnicowanie po czasie: zmiana rowiązania granicznego, albo jako parametry po czasie

$$\frac{d}{dt} \int f(x, t) dx = \lim_{\Delta t \rightarrow 0} \frac{1}{\Delta t} \int_a^{a+\Delta t} f(x, t) dx = \int_a^b f(x, t) dx = \frac{f(b)}{dt} dt = f(b)$$

$$\frac{d}{dt} \int f(x, t) dx = \lim_{\Delta t \rightarrow 0} \frac{1}{\Delta t} \int_a^b f(x, t+\Delta t) dx = \int_a^b f(x, t+\Delta t) dx$$

zgodnie z definicją pojęcia granicy po czasie

jeśli  $f'$  jest funkcja

wtedy i tylko wtedy

~~$x(t)$~~



to jakaś mówiąc położenie

jakaś faza mówiąc położenie

mówiąc jakaś stojąca

jeśli  $U$  do jakiegoś wypadku namówić to:

$$U = \int \frac{dv}{r} \quad \text{zdarzyły się odcinki ale } dv = r^2 dr dw \quad \frac{dv}{r} = dr dw$$

$$\text{czyli } \frac{dr}{r} \text{ dla } \frac{dv}{r} \text{ dla } ? \quad \int \frac{dr}{r} = \int dr dw \quad \text{to jasne że ciągle się rośnie}$$

$$\text{czyli } \frac{dr}{r} \text{ dla } \frac{dv}{r} \text{ dla } ? \quad \frac{dr}{r} = \dots \quad \text{ale } \frac{dr}{r} = \int r^2 dr dw \left[ \frac{3(x-e)^2}{r^5} - \frac{1}{r^3} \right] \quad b_0 = \infty - \infty$$

minimale kąt  
następnie do zwiększenia  
maksymalnego kąta

de moine euron vrdid! kule tok nld<sup>no skote</sup> w<sup>o</sup> gressie puth eyr za emunose  
moe byd v mij zandbang

8



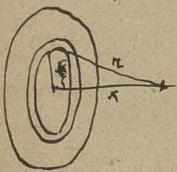
$$\nabla^2 U = \nabla^2 U_0 + \nabla^2 u$$

" " -ngp w<sup>o</sup> Tornon'a rorami ofhni osine.

Ajihle dene johi hyle fungsing U -

Jihi w<sup>o</sup> U dan to euron mien indik w<sup>o</sup> bled ne

Teror co do drji go ~~fest~~ rodrigis meoy, ~~pan~~ roderlong na porusahus:  
Tij argumenteay nre moiney w<sup>o</sup> durny ie ny puy huli jihi powne roduan  
se meoy gtu.



$$U = \int_0^A \frac{2\pi b \xi \, d\xi}{\sqrt{\xi^2 + x^2}} = \sqrt{2\pi b} \int_0^A \sqrt{\xi^2 + x^2} \, d\xi = 2\pi b \left[ \sqrt{A^2 + x^2} - x \right]$$

Jihi w<sup>o</sup> A = 0 (minimiaza fungsing) to U = 2\pi b

$$\text{Teror } \frac{\partial U}{\partial x} = 2\pi b \left[ \frac{x}{\sqrt{A^2 + x^2}} - 1 \right] \Big|_{x=0} = -2\pi b$$

Gaflysing nre tok same vrdid: no huy' storn hyle tokin  $\left(\frac{\partial U}{\partial x}\right) = -2\pi b$

ponekoi ji hyle komulk x porotgi ter sam, to musta y ngelei:  $-\frac{\partial U}{\partial x} = -2\pi b$

$$\frac{\partial U}{\partial x} - \frac{\partial U'}{\partial x} = -2\pi b = \frac{\partial U}{\partial x} + \frac{\partial U'}{\partial x}$$



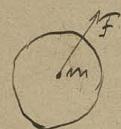
Johini moine w<sup>o</sup> - teh mely begin i<sup>6</sup> tan ~~\* minnowemic~~  
x moine tok hyle byd, in ~~want~~ anians  $\frac{\partial U}{\partial x} = 0$  C

anoreja apfni komulk x pun n:

$$\frac{\partial U}{\partial x} - \frac{\partial U'}{\partial x} = -2\pi b$$

12

## Twierdzenie Gausse

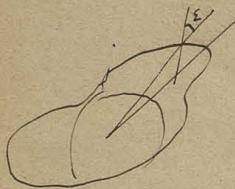


$$\vec{F} = \frac{\vec{m}}{r^2}$$

$$\oint \frac{\vec{m}}{r^2} d\vec{l} = \int \frac{\vec{m}}{r^2} \cdot \vec{r} dw = \int m \cos \theta d\theta \cdot d\varphi = 4\pi m$$

między liniami

Tak samo dla jakichkolwiek powierzchni



$$\oint \vec{F}_n d\vec{l} = \int \frac{\vec{m}}{r^2} \cdot \vec{n} dw = \int \frac{\vec{m}}{r^2} d\vec{l}' = \int \frac{m}{r'^2} dw = 4\pi m$$

$d\vec{l}' : d\vec{l} = r^2 : r'^2$

Linie sil: równie jak powierzchnia punkt jde przez -- powierzchnię

Jedli wych mas:

STL dane Wyjedźmy z nowej - styczna do powierzchni

Rozkładamy  $\vec{F}$  na kierunek  $\vec{F}_1, \vec{F}_2, \dots$  i kierunek normalny



$$4\pi m_1 = \oint \frac{\vec{m}}{r^2} d\vec{l}$$

$$4\pi m_2 = \oint \frac{\vec{m}}{r^2} d\vec{l}$$

$$4\pi m = \oint \vec{F}_n d\vec{l}$$

$$\int m_n d\vec{l} = \iiint \operatorname{div} \vec{v} dw$$

$$v = \nabla U$$

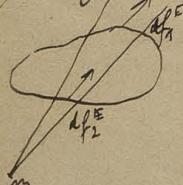
$$\int \frac{\partial U}{\partial n} d\vec{l} = \iiint \frac{\partial^2 U}{\partial n^2} dw$$

$$= 4\pi m$$

$$4\pi m = - \int \frac{\partial U}{\partial n} d\vec{l}$$

= - \iiint \frac{\partial^2 U}{\partial n^2} dw

Jedli je drah punkt rozdrogi zawsze:



$$\vec{F}_1 \cdot n_1 d\vec{l}_1 = \vec{F}_2 \cdot n_2 d\vec{l}_2$$

z jedli jest rozdrogi na wierzch to  $\vec{F}_1 \cdot n_1 d\vec{l}_1 = - \vec{F}_2 \cdot n_2 d\vec{l}_2$ 

$$\int \vec{F} d\vec{l} = 0 \quad \int \frac{\partial U}{\partial n} d\vec{l} = 0 \quad \text{Tak samo dla wierzch, kiedy mas}$$

wys. wychi  $\int \frac{\partial U}{\partial n} d\vec{l} = - 4\pi m$   $\checkmark$  mimo mas wierzchowych

$$\iiint G \frac{\partial H}{\partial x} dx dy dz$$

Friedrichs Green's princ!

13

particji d'ansatzu zwarto

3

$$\frac{\partial}{\partial x} \left( G \frac{\partial H}{\partial x} \right) = G \frac{\partial^2 H}{\partial x^2} + \frac{\partial G}{\partial x} \frac{\partial H}{\partial x}$$

$G, H$  funkje appka

$$\iiint G \frac{\partial^2 H}{\partial x^2} dx dy dz = \iint G \frac{\partial^2 H}{\partial x^2} dy dz - \iint \frac{\partial G}{\partial x} \frac{\partial H}{\partial x} dy dz$$

df (weak)

$$\iiint G \nabla^2 H dx dy dz = \iint G \left( \frac{\partial^2 H}{\partial x^2} \cos x + \frac{\partial^2 H}{\partial y^2} \cos y + \frac{\partial^2 H}{\partial z^2} \cos z \right) df - \iint \cdots$$

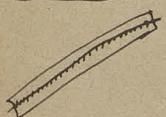
$\frac{\partial x}{\partial h}$

$$= \iint G \frac{\partial^2 H}{\partial n^2} df - \iint \cdots$$

$$\iiint G \nabla^2 H dx dy dz = \iint G \frac{\partial^2 H}{\partial n^2} df - \iint \left[ \frac{\partial^2 f}{\partial x^2} \frac{\partial^2 H}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} \frac{\partial^2 H}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} \frac{\partial^2 H}{\partial z^2} \right] dx dy dz$$

N.p.  $G = 1 \parallel H = \Psi$

$$\iiint \nabla^2 V dx dy dz = \iint \frac{\partial^2 V}{\partial n^2} df = - \sum 4 \pi m$$

← 

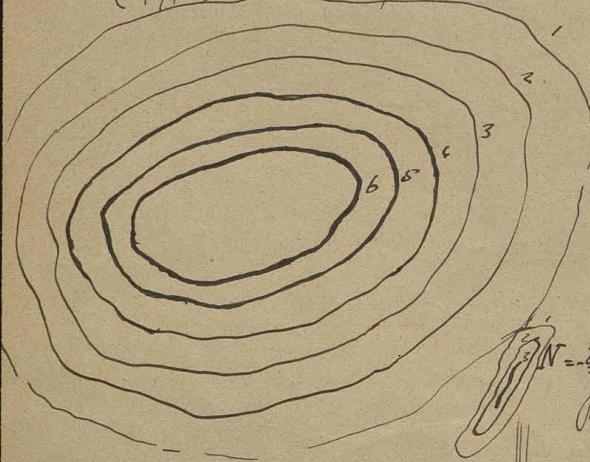
$$\iint \frac{\partial^2 V}{\partial n^2} df = \left[ \frac{\partial V}{\partial n} + \frac{\partial V}{\partial n'} \right] f + \dots = f.b$$

element jorimishni otzamyay pravka  
nurk. arki

←  $x \rightarrow \boxed{x} \rightarrow x+dx \quad dy dz dx + dx dz dy + dx dy dz = + 4 \pi \rho H dx dy dz$

$$\frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz = - 4 \pi \rho$$

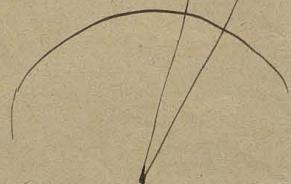
(p. 6)  
 Wyz dane sa masy i formy rozmieszczenia, z których określają orbitę  $V$   
 Współnione tej funkcji gromadzą informacje. Pole siłowe to jest gromadzące  
 $V(x, y, z) = \text{const}$  powierzchnie potencjalne (hiperboloidy)



zawiera informacje o ruchu wewnątrz  $V$   
 Bieżąca masa wytwarzająca pole grawitacyjne  $V$  ma taką samą  
 wartość jakkolwiek to niektóre parametry esto.

Wyz danej systemu znajdują się określone punkty, kierujące ruchem ją do nich  
 w związku z tymi określonymi punktami, na których ruch jest  
 ilość energii przechodzącej przez jądro powierzchniowo do tego punktu  
 Należy przyjąć jądro masy: powierzchnia  $\pi r^2$  ma energię w stanie

jednostkowej masy wewnątrz  
 moment prędkościowy do jądra jest równy  
 prędkości jądra do masy wewnętrznej i jest  
 spowodowany przez tą samą siłę grawitacji, jaką  
 jądro powoduje jądro + masa wewnętrzna



jednostkowej masy (4πr<sup>2</sup>) masy  
 to prędkość jądra powierzchniowo

$$\text{masy} \quad \frac{4\pi r^2}{4\pi r^2} = \frac{m}{r^2}$$

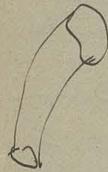
o jednostce  $\frac{m}{r^2}$  w s

to jest to samo i w ogólnym przypadku, wykazuje jądro złożone z dwóch

części.

Wyz danej masy do  $V$ ; masy wewnętrznej opisują punkt jądra masy jest zero.  
 Nie ma więc możliwości rozważania

Jużli għall-piex kien jidher minnha tħalli idu oporji kien u m'halli ramkun tgħiex to 10 15  
postejx istokku idu (ura idu) (Methħorre) (tube of force).



$$\text{żottorija na mis-Sensu:} \quad \tan jidu niha m'ha m'saq} \\ q F_u + q' F'_u = 0$$

$$F_u : F'_u \quad q F_u = q' F'_u$$

żotu ordop iekk jaft misaq idu, tħalli wiċċe u minn-hi kien u fuq orbie

Jużli wiċċe għarr-jidher pprekkij q' upprestħu  $F_u$  linj idu to użżejjew w-jekk  
iegħi pprekkij tiegħi istokku b'din dana għiex il-ġorr-dejeg u l-ġorr-dejeg =  $\frac{q F_u \cdot L}{2}$   
żotu misaqi stonzeri to jekk idher. I tkoll samu ar-Riġiż idher

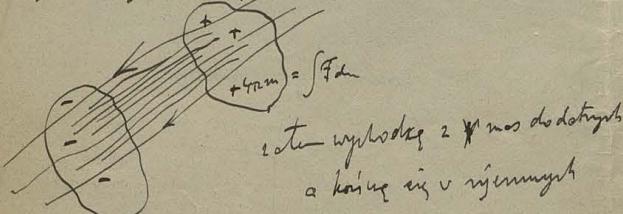
Għix tħalli linj pprestħu qiegħi minn-jekk. Iż-żorr uqqa' minn-  
 $= \int F_u \, df$

### Forza triddekkha Sensu

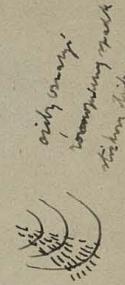
Jużli jidher s-salha u serrova jekk idher m'saq

to  $q F_u = q' F'_u - 4qmu$  wiċċe iddu u jidher strong wiċċi b'din linj u kien drid  
niżi u dridji strong wiċċi dan. (qarri k-tnejja minn-ikku minn-hi)

W-ġożei myjh kien idu minn-hi kien idher m'halli ramkun tgħiex -0  
Wiċċe wixxistha nseħħol u nekk i-kien u m'as (albo u m'as kien u m'as)



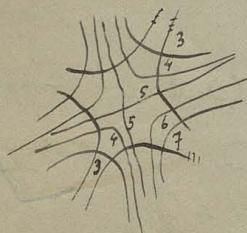
is tottekkija minnha  
jaġid samu minn-hi  
kien waqtaw minn-hi  
kien waqtaw minn-hi



16

et tgs most oynka in pthys in more nge' wghn now' gire tan johi se nay,  
bo johi nay. tw v pthys obhi wghthie  $F_n$  dethi also wghthie  
in  wife  $F_{nd} = 4 \text{ nm}$

More johi nctpic' minm. v pthys pththi also linies t.f. v johi  
kerukku nay. v inay min.



to study v johi kerukku + v drui -

line sity operad gnu.



$\theta$  by time by sandalito!  
de ar pththi  
opposite side to  $\theta$   
 $\theta = 60^\circ$  by gulu

wife johi n.p. pththi =  $\frac{\partial U}{\partial r}$  na pthys pththi zanting to w caty  
pustrem (by dae ~~stam~~) johi w nroku n zanting johi' nay  
Tak sans johi na pththi zanting v guthi nay = 0 to take v caty  
zanting pustrem = 0.

johi dene ~~the~~ <sup>the</sup> pththi pththi pththi  $\frac{\partial U}{\partial r}$  v wghthi pththi to  
v johi pththi pththi <sup>(microphoton)</sup> pththi mukong me moe hgi v kerukku steli  
to ~~the~~ <sup>the</sup> Rmowga steli v yga iky v obhi hell nay. moti'  $F_n < 0$

$$\text{wife } \frac{\partial U}{\partial r} > 0$$

Tymem nay  $\left( \frac{\partial U}{\partial r} + \frac{\partial U}{\partial p} + \frac{\partial U}{\partial n} \right) = 0 = \int \frac{\partial U}{\partial r} dr$  wife johi  $\frac{\partial U}{\partial r} > 0$  v pthys pththi  
v obhi dohuy johi tgs nay  
(v tgs may esle nay v tgs nay)

Gdby shthy amu' mto' nroku hgi v wghthi v nuk pustrem  
a tak sans nay graityna strathor steli v johi pththi

wife tgs to kerukku  
obhi  
dry mud steli turbul jum  
operashn up it excrete also  
operashn vah

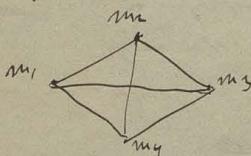
Si doted by the same tykho move o potencyah v jeho pukhie = potencyah 17  
na masy 1 tare si znejduje q.

11

Gdy ten tykhe masy m do sile = - m  $\frac{\partial U}{\partial s}$

a jekor <sup>potencyah</sup> ~~potencyah~~ = - m U Gdy uje masy m do sile sily  
masy m od dolu sily u  $\infty$ ; jekor <sup>dovles ilinnes</sup> ~~do masy m, m<sub>L</sub> & do sile sily~~, ~~do sile sily~~ ~~m<sub>L</sub>~~

potencyah = 0



Jekor masy masy one zolnotci:  $W =$

$$\text{punkt m, od dolu sily u } \infty : \frac{m_1 m_2}{r_{12}} + \frac{m_1 m_3}{r_{13}} + \frac{m_1 m_4}{r_{14}}$$

$$m_2 \sim \infty : \frac{m_2 m_3}{r_{23}} + \frac{m_2 m_4}{r_{24}}$$

$$m_3 \sim \infty : \frac{m_3 m_4}{r_{34}}$$

*Kombinace  
bez potencie*

Z tet potomny vysicini  $m_1 U_1 + m_2 U_2 + m_3 U_3 + m_4 U_4 =$

$$= \frac{m_1 m_2}{r_{12}} + \frac{m_1 m_3}{r_{13}} + \frac{m_1 m_4}{r_{14}} + \frac{m_2 m_3}{r_{23}} + \frac{m_2 m_4}{r_{24}} + \frac{m_3 m_4}{r_{34}} + \frac{m_1 m_2}{r_{13}} + \frac{m_1 m_4}{r_{14}} + \frac{m_2 m_3}{r_{24}}$$

$$= 2 W$$

*Kombinace s potenciem*

Zatem Area cethrate = Energia potencyah =  $\frac{1}{2} \sum m U$   
vyhodna

$$W = -\frac{1}{2} \int \int U \nabla^2 U dv$$

*zdvorsiv do  
parametru vektora  
ido myslit vektorem  
pri deli masy*

$$= -\frac{1}{8\pi} \int \int \frac{U}{r_{12}^2} df + \frac{1}{8\pi} \int \int \left[ \frac{(dU)}{r_{12}} + \frac{(dU)}{r_{13}} + \frac{(dU)}{r_{14}} \right] dv$$

*to kde pri deli masy  
takze zvetsene potencie  
je vektorem potencie*

$$W = \frac{1}{8\pi} \int F U df + \frac{1}{8\pi} \int \int \dots$$

*jekli zotra na posnej potencie  
U abo  $\frac{dU}{dr} = 0$  je jekli  
vzhodna pos to potencyah masy by isty  
(v pismenym puzdze = 0) jekli jen my*

18

Uzyskiwanie:

$$\lim_{r \rightarrow \infty} U_r = \int \rho dr$$

pomiarowy  $U = \frac{\int \rho dr}{R + (1-R)(r-R)}$



$$\lim_{R \rightarrow \infty} U_r = \lim_{R \rightarrow \infty} \frac{\int [R \dots (R+dr)] \rho dr}{R + (1-R)} = \frac{\int \rho dr}{R}$$

$$= \lim_{R \rightarrow \infty} \frac{\int \rho dr}{1 + \frac{1-R}{R}} = \int \rho dr = M$$

~~Jeżeli mamy tylko mierzone po dane, o której nie mówimy. To co z tego?~~

~~Takie dane daje  $\frac{dU}{dr}$  to powstaje do mierzonej, co daje tym zadanie p. II, jakim mówimy  
potrzeba określić?~~ Do mocy się zdecydowanie  $U = \int \rho dr$ : nie mamy wykonać tego oznaczenia, ale mamy ją zdecydowanie już zapisane.

Dobry mój radzić się myśleć: ~~jeżeli mamy ją zapisane, to mamy dobrze postawiony~~  
~~jeżeli mamy ją zapisane, to mamy dobrze postawiony~~

$$\nabla^2 \Phi = -4\pi\rho$$

w powyższej obrazku p20)

$$\frac{\partial^2 \Phi}{\partial r^2} + \frac{\partial^2 \Phi}{\partial z^2} = -4\pi\rho$$

w powyższej powiedzimy

w powyższej powiedzimy  
frankami

i na powyższej mówimy musi być dane  $U$  albo  $\frac{dU}{dr}$

jeżeli mamy mierzone, to jedyne jasne istotne drugie komponenit  $U$ , jedno z wymagać  
tych samych warunków to mówiąc my:

$$\nabla(\Phi - \Phi_0) = 0$$

$$\frac{\partial(\Phi - \Phi_0)}{\partial r} + \frac{\partial(\Phi - \Phi_0)}{\partial z} = 0$$

i na powyższej mówimy  $\frac{\partial(\Phi - \Phi_0)}{\partial r} = 0$  albo  $\frac{\partial(\Phi - \Phi_0)}{\partial z} = 0$

zatem  $(\Phi - \Phi_0) = C$  mówimy, to samo powiedzieć itd.

$U - U_0 = 0$  mówiąc dwaj zyski  
takie same

Zatem jeśli mówiąc istotnie funkcje radia "zgadza" to tylko jasne.

Dowolne są rozmieszczenia  $\rho$  i to w na powierzchni,  $U$  w jednym miejscu a  $\frac{dU}{dr}$  w innym  
albo także  $U$  same to jasne istotnie, jedyne  $\frac{dU}{dr}$  same to jasne nie mówimy tego.

ale to kiedyż mówiąc warunek jest możliwość tego mówimy jasne dobrze.

Przypomnian jawnie dość często twierdzenie

$$\int \varphi P \frac{d\varphi}{dr} dr = \int \varphi \frac{d\varphi}{dr} dr - \left[ \left( \frac{\partial \varphi}{\partial r} \right)^2 + \dots \right] dr$$

Jednakże wtedy  $P_{\varphi=0}$  i  $\varphi$  jest pochodna po  $r$  dla  $\frac{\partial r}{\partial \varphi} = 0$  to mówiąc  $\varphi = \text{const}$

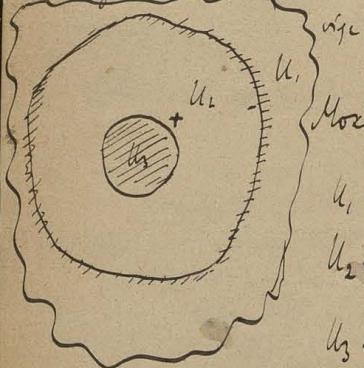
Ważność tego twierdzenia w ten sposób：

Jednakże dla  $\rho \neq 0$  i jednej masy wybranej całkowicie to mówiąc to to będzie  $U$  i nie  
potrafię wykazać jednego warunku na pochodnych

Jednakże jednak całkowitej masy wybranej całkowitej tyleż jeli i jeśli innym sposobem  
wykonując pochodną  $\varphi$  to kiedyż wybrany jest warunek dla  $\rho \neq 0$  to mówiąc  
to nie mówiąc aby to jest  $U$  dla  $\rho \neq 0$  mówiąc aby to jest warunek na warunki wybranej.

Intuicja mówiąc,  $\varphi$  musi być jawnie odwołane do warunków warunków na pochodnych.

Dzięki temu: 2 kule, środku  $\rho$ , na zewnątrz  $\sigma = -\frac{M}{4\pi A^2} = -\frac{a^3 \rho}{3A^2}$   
 $M = \frac{4\pi a^3 \rho}{3}$



Masywy obie pudełko skrócenie  $U$  o tym punkcie przypadek  
do tego na przykład jednego warunku

$$U_1 = 0$$

$$U_2 = M \left( \frac{1}{a} - \frac{1}{2a} \right)$$

$$U_3 = M \left( \frac{1}{2a} - \frac{1}{A} \right) - 2\pi \rho (a^2 - r^2)$$

ale jeli nie znajdziemy jakim sposobem funkcji  $\varphi$  która nadaje się warunkiem  $P_{\varphi=0} = -4\pi \rho$

To jasne nie ma masywy pośredni i to jest  $U$  my jesteśmy mimo funkcji,

bo do tego mamy jedynie jawnie miedzi jaka  $\varphi$  ma być na jednym warunku  
(To odwołane do tegoż całkowania my mówiliśmy o miedzi)

$$N.p. \quad \varphi_3 = U_3 + x_3$$

$$\varphi_2 = M \left( \frac{1}{2a} - \frac{1}{A} \right) + x_2$$

$$\varphi_1 = x_1$$

To nie działa i jest to jawnie kontrakt

$$\text{jeżeli } \varphi_0 = \varphi_2 = M \left( \frac{1}{2a} - \frac{1}{A} \right) + x_2 \text{ to } \varphi_1 = x_1$$

167 Tak jut miskonsumi nicle miskonsumi responz

ek jisti se potom vortici  $U$  (alto  $\frac{\partial U}{\partial x}$ ) so ravnost' posledni [vind] to sum to y  
je jut ornece

N.p. Jisti vortici je  $\varphi = 0$  na kde  $x=1$

To mydy mystremi miskonsumi tyto to jidlo  $\varphi = 0$  a priebe tenu vortici  
jisti na kde  $x=1$  a miskonsumi vortici dan n.p.  $\varphi = \frac{\partial U}{\partial x} \propto$   
to tyto jidlo  $\varphi = 0$  tenu vortici priebe st.

Hvora takie tak priebe je to miskonsumi vortici vortici

to ~~tyto~~ Intomuze fizyne jidlo to mystremi vortici miskonsumi

1). Granitaya  $\rho = 0$   $G = 0$  nech  $U =$

2). Elektro.  $\rho$ ,  $G$

3). Mag.

4). ~~Hydrodynamika~~ <sup>"</sup> cisay miskonsumi jisti priebe priebe

$\nabla \varphi = 0$  dan miskonsumi byt vortici ale posledni

Wtedy vize limit sily = limit priebe

n.p. jisti silu vortici to ten  
vtedy priebe miskonsumi  $\varphi = 0$   $\nabla \varphi = 0$

$\varphi = U$

Tedobe mi skrytu ~~sledovanie~~  $\nabla U = \nabla \varphi = \frac{\partial \varphi}{\partial x}$  Helmholtz

5). Cisdy stek elektroone

$$u = -\lambda \frac{\partial U}{\partial x} \quad \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = -\nabla^2 U = 0$$

$$v = -\lambda \frac{\partial U}{\partial y}$$

$$w = -\lambda \frac{\partial U}{\partial z}$$

## 6) W analogia tylu prawa dnia wyciąga

$$C \frac{dt}{dt} = -\kappa P^t$$

22  
13

Obersteilheit!  
Vorlesung mit dem von der Universität  
ab. Nur am Okt. 10. d. Jahr

Elastostatyka; tzn. siły tylu stanu niesymetrycznego  
 Hypothese  $\frac{+m_m}{r_i} + \frac{-m_m}{r_i}$ , diszeduna Coulomba; <sup>1785</sup> odnoszące się do elastostatyki  
 Coulomb; Cavendish; notowania nie są gotowe, tylko jest  
 wyraźny, o którym mówiący, kto i co  
 sprawdza.

Opis tego do historii napisy dodać: że el. o wartościach (konstantach) tak  
żeby nie miały żadnych związków z innymi o innymi wartościami, co natomiast tylu per to jest  
 możliwość i istnieje jasne izolatory które ją umożliwiają iż żadnych  
 sił nie ma między izolatorami ani między izolatorem i metalowymi częściami i krochów  
 sił, co do żeby stąd wynikało d. nie istnieje sytuacji. Mechanizm o wartościach  
 tak określonych, d. do nich były przypisane, albo raczej określonej sytuacji:  
 energie skup. + energ. mechaniczna (kinet. itp.) = stała, więc w zasadzie zachowane są  
 rozdzielne

Co do ~~szektryzyni~~ elektrostatyki:

W konstrukcji izolatorów tylu jest  $\frac{U}{r} = 0$   $U = \text{const}$   
 na powierzchni w konkretnych sytuacjach  $\frac{U}{r} = 0$ , tylu w normalnym warunku  $\frac{U}{r}$   
 (tam nie mówią o oddaleniu). Jednakże izolator (pozostałe)

W izolatorach to m. potencjały zasadniczo tylu m. potencjały by  $= 0$ , tylu mówią  
 m. drugie warunki, 2 poziomy izolacji jasno jasne m. siły natadowane, to t. m. sytuacji  
 m. zadanego natadowanego, więc wojciech ubogu edycji i w m.  $p=0$

23

Zatem w danym  $\nabla^2 U = 0$ 

&lt; tylko na powierzchniach kondensatorów:

$$\boxed{\frac{\partial U}{\partial n} + \frac{\partial U}{\partial n'} = -4\pi\sigma}$$

U podlega do funkcji  
wysokości przeniesienia  
wysokości przeniesienia  
"funkcji" i tym samym  
wysokości przeniesienia  
wysokości przeniesienia  
do góry -4πσ.

Zatem rozkład U całkowity na dany jął: dane 6 i  
dane wartości U na granicy powierzchni:  
"funkcji"

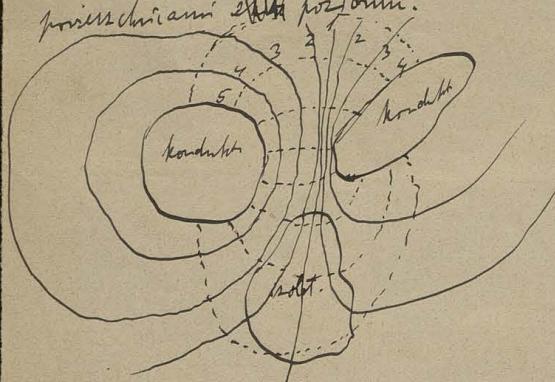
Wtedy

$$U = \int \frac{6 \, df}{\pi r^2} + \int \frac{\frac{\partial f}{\partial n} - \frac{\partial f}{\partial n'}}{r} \, dl$$

N.p. dla jąła

Zatem pole elektryczne wydaje się na całym obszarze i:

względzie  $\rho=0$ , tylko na powierzchniach kondensatorów może być 6  
wysokości przeniesienia wykroju z powierzchni kondensatorów; linię sig ne ma  
(albo  $r=\infty$ ). Ponieważ styczna skrótu musi być  $=0$ , zatem powierzchnie kondensatorów =  
powierzchniami ~~które~~ porównanie.



do wyjścia przeniesienia toków i pola, mające punkt  
wysokości przeniesienia, o którym mowa dalej, aby  $\nabla^2 U = 0$   
ale tym razem rozkładu zadanego na tyle powietrza  
zatem rozkładu nie potrafiemy wyznaczyć.

wysokości przeniesienia jedna i ta samą potrafieli  
jedynie dwa kondensatory się dotknąć to potrafią ich wyznaczyć się.

Na dany potencjał można dodać potencjały podlegające do tegoż jąła 2 wysokim eliktrycznym.

Ostatni znamy  $0$ , ~~to~~ one jest konstantą (współczynnik dalszy do wyznaczenia)

wysokim jest konstantą potencjału dany potencjały 2 znamy mające  $U=0$

$$2 \text{ typ matematyczny dla } 600 \text{ znamy, przewinie } \frac{\partial U}{\partial n} = \frac{600}{100} \cdot \frac{1}{100} = 0.02 \quad 6 = \frac{0.02}{4\pi} = -0.0016$$

zazwyczaj mniej potencjalny w powodzeniu

korzystne: pozytywne i negatywne = a czasem powodzenie zaktualizowane do nowej sytuacji wywołuje?

Zadanie: znaleźć rozbudowane i istotne podsumowanie.

Przygotowanie Verteilungsproblem Czy jest jasne jasne?

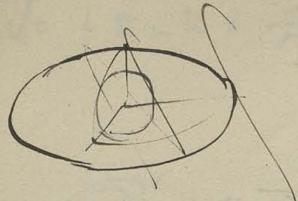
Aby móc zatrudnić dany zakład, jaką na nim zarząd, jaką potęgą i jakim wytrwałością jakaś istota może? To zatrudnia tylko, ile jednostek mała potęga i ile jednostek wiele =  $\frac{1}{\text{potęga}}$

[Pierwszy znak stawiany kwestią rozwiązywaną]

It is not clear what the original text was intended to say. The following is a reconstruction based on the visible ink and the context of the letter.

Dear Sir or Madam  
I am writing to you to express my thanks for your kind gift of books. I have received them and they are excellent. I particularly like the one on the history of the English language. It is very well written and informative. I have also received the book on the history of science, which is also very interesting. Thank you again for your kind gift.

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$$



~~eliptische~~

$$2\pi \int_{-\infty}^{\infty} d\varphi \frac{c^2}{A^2}$$

$$\cancel{\frac{c^2}{A^2}} \left( 1 - \frac{c^2}{a^2} \cos^2 \varphi \right)^{-1} + \frac{(c/a)^2}{A^2} \sin^2 \varphi$$

$$\frac{x^2}{a^2} \left( 1 - \frac{1}{a^2} \right) + \frac{y^2}{b^2} \left( 1 - \frac{1}{b^2} \right) = 1$$

$$= 2\pi \frac{c^2}{A^2} \frac{d\varphi}{\sqrt{c^2 - 2c^2 \cos^2 \varphi + (c^2 - a^2) \sin^2 \varphi + a^2}}$$

$$V_a = 2\pi \int_0^\infty \left( 1 - \frac{x^2}{a^2+s} - \frac{y^2}{b^2+s} \right) \frac{ds}{\sqrt{(1+\frac{x^2}{a^2+s})(1+\frac{y^2}{b^2+s})}} \quad || \quad a^2 = b^2(1+\varepsilon^2)$$

$\lambda = \rho(\varepsilon^2)$

$$\cancel{\frac{x^2}{a^2+s}} = \frac{x^2}{s}$$

$$= 2\pi \int_0^\infty 1 - \frac{x^2}{a^2+s+\lambda s} -$$

$$X = \int_0^\infty \frac{x \, ds}{(a^2+s)^{3/2} (b^2+s)^{1/2}} = \int_0^\infty \frac{s \, ds}{(b^2+s+\lambda s)^{3/2} (b^2+s)^{1/2}}$$

$$Y = \int_0^\infty \frac{y \, ds}{(a^2+s)^{1/2} (b^2+s)^{3/2}} = \frac{1}{(b^2+s)^{5/2}} + \frac{e^2}{(b^2+s)^{7/2}}$$

$$\int \frac{ds}{\sqrt{(1+\frac{x^2}{a^2+s})(1+\frac{y^2}{b^2+s})}} = \int \frac{2a^2 \sqrt{1+\frac{x^2}{a^2}}}{1+\frac{x^2}{b^2}} + \int \frac{\sqrt{1+\frac{y^2}{b^2}}}{(1+\frac{y^2}{a^2})^{1/2}} \, ds$$

$$\frac{\sqrt{1+\frac{x^2}{a^2}}}{1+\frac{x^2}{b^2}} + \frac{1+\frac{x^2}{b^2}}{\sqrt{1+\frac{x^2}{a^2}} (1+\frac{x^2}{b^2})} + \int \frac{y \, ds}{(1+\frac{x^2}{b^2})^{1/2} \sqrt{1+\frac{x^2}{a^2}}} + \int \frac{s \, ds}{a^2 (1+\frac{x^2}{b^2})^{1/2} \sqrt{1+\frac{x^2}{a^2}}}$$

$$a = b \quad \int \frac{x \, ds}{(a^2+s)^{5/2}} = \frac{x^2}{3} \frac{1}{(a^2+s)^{3/2}} \int = \frac{2x^2}{3a^2}$$

$$\int \frac{y}{(b^2+s)^{1/2} \sqrt{1+\frac{x^2}{b^2}}} = \frac{y}{(b^2+s)^{1/2}} \sqrt{1+\frac{x^2}{b^2}} = \frac{ye^2}{(b^2+s)^{5/2}} \left[ 1 - \frac{e^2}{2(b^2+s)} \right] \quad \left| = \frac{ye^3}{b^3} \left( \frac{2}{3} - \frac{1}{5} \cdot \frac{e^2}{b^2} \right) = \frac{ye^3}{b^3} \left( 1 - \frac{3}{10} \right) \right.$$

$$\int \frac{x^2}{(b^2+s)^{1/2} \sqrt{1+\frac{x^2}{b^2}}} = \int \frac{x^2}{(b^2+s)^{5/2}} \left[ 1 - \frac{e^2}{2(b^2+s)} \right] \quad \left| = \frac{x^2}{b^3} \left( \frac{2}{3} - \frac{3}{2} \cdot \frac{e^2}{5} \frac{1}{b^2} \right) \quad \left( 1 - \frac{9}{10} \right) \right.$$

$$\iiint \frac{abc}{A^3} \frac{dx dy dz}{\sqrt{\left[\frac{(x-a)^2}{A}\right]^2 + \left[\frac{(y-b)^2}{B}\right]^2 + \left[\frac{(z-c)^2}{C}\right]^2}}$$

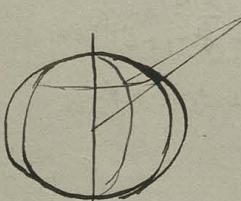
$$X = \frac{x-a}{A}$$

$$Y =$$

$$Z =$$

$$= \iiint abc \frac{dx dy dz}{\sqrt{(AX - ax)^2 + (CY - by)^2 + (CZ - cz)^2}}$$

Pot. sferisch wo punkt no verlängert



$$r =$$

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1$$

$$r^2 = \frac{1}{\frac{a^2 \varphi}{a^2 + b^2 \varphi} + \frac{b^2 \varphi}{a^2 + b^2 \varphi}} = \frac{1}{\frac{a^2}{a^2 + b^2 \varphi} (1 + \frac{b^2}{a^2})}$$

$$= \frac{a^2}{1 + \frac{b^2}{a^2} \sin^2 \varphi}$$

$$= a^2 (1 + \sin^2 \varphi)$$

$$\int_{\varphi=0}^{2\pi} \int_{\xi=0}^{2\pi} \frac{a^2 \sin^2 \varphi \cos \varphi d\varphi d\xi}{\sqrt{(x - a \sin \varphi \cos \xi)^2 + (y - a \sin \varphi \sin \xi)^2 + (a \cos \varphi)^2}} =$$

$$a^4 \int_0^{2\pi} \int_0^{2\pi} \frac{\sin^2 \varphi \cos \varphi d\varphi d\xi}{\sqrt{x^2 - 2ax \sin \varphi \cos \xi + a^2 \sin^2 \varphi + y^2 - 2ay \sin \varphi \sin \xi + a^2 \sin^2 \varphi}}$$

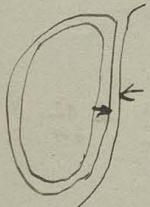
$$= a^4 \int_0^{2\pi} \int_0^{2\pi} \frac{\sin^2 \varphi \cos \varphi d\varphi d\xi}{\sqrt{x^2 - 2ax \sin \varphi \cos \xi + a^2 + y^2 - 2ay \sin \varphi \sin \xi}}$$

10 p. 17  
16

not pos. 6  $\Rightarrow$  assume  $\alpha$  perpendicular to  $\partial D$

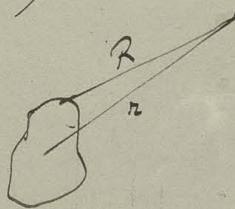
$$W = \frac{1}{2} \sum_m U = -\frac{1}{8\pi} \left[ \int_U \nabla U \cdot d\alpha + \int_U \frac{\partial U}{\partial n} d\sigma \right]$$

$$= \underbrace{\int_U \frac{\partial U}{\partial n} d\sigma}_{\text{orthogonal to } \partial D} + \int_U \frac{\partial U}{\partial n} d\sigma = \int \left( \frac{\partial U}{\partial n} + (\tilde{j})_r - (\tilde{j})_t \right) d\sigma$$



orthogonal to  $\partial D$

$$= \frac{1}{8\pi} \left[ \int \left( \frac{\partial U}{\partial n} \right)_r - \dots \right] d\sigma \quad \parallel \quad = 0 \quad \text{peripheri} \quad U \neq \frac{M}{n}$$



$$\lim_{n \rightarrow \infty} U = \frac{1}{8\pi} \int \frac{\rho d\omega}{R + (r-R)} = \frac{1}{8\pi} \int \frac{\rho d\omega}{R + \frac{R-r}{R}} \quad \frac{\partial U}{\partial n} \neq -\frac{M}{r} \quad d\sigma = d\omega r^2$$

$$= \frac{1}{R} \int \rho d\omega$$

$\left[ \begin{array}{l} \text{Jadi } \alpha \text{ pos. konstanty} \quad \text{K also } \frac{\partial U}{\partial n} = 0 \quad \text{da} \text{ wirkt } \rho \text{ auf } \alpha \text{ so } \text{ da} \text{ wo } \alpha \text{ auf } \partial D = 0 \\ \int_U \nabla U \cdot d\alpha = 0 = + \int_U \frac{\partial U}{\partial n} d\sigma - \int \left( \frac{\partial U}{\partial n} \right)_r - \dots - \dots - \dots \end{array} \right] \quad \text{aber } \Rightarrow \text{jadi } \uparrow$

gesetzigt sind: obige jadi ist  $\Rightarrow$   $\alpha$  pos.

- in der nachst. Zeit schreibt 1. mit ist dies verboten  
2. mit mir kann man hier nicht

$$V_i = \pi \rho \int_0^\infty \left( 1 - \frac{x^2}{a+x} - \frac{z^2}{b+z} - \frac{y^2}{c+y} \right) \frac{ds}{\sqrt{(1+\frac{x}{a}) (1+\frac{z}{b}) (1+\frac{y}{c})}}$$

$$V_a = \pi \rho \int_\lambda^\infty \frac{x}{a+x} + \frac{z}{b+z} + \frac{y}{c+y} ds = 1$$

$$\frac{\partial V_i}{\partial x} = -2\pi \rho \int_0^\infty \frac{x}{a+x} \frac{ds}{D}$$

$$\frac{\partial V_a}{\partial x} = -2\pi \rho \int_\lambda^\infty \frac{x}{a+x} \frac{ds}{D} - \pi \rho \underbrace{\left[ -\frac{x}{a+x} - \frac{z}{b+x} - \frac{y}{c+x} \right]}_{=0} \frac{2x}{D}$$

$$V_i = V_a \Big|_{\lambda=0}$$

$$\frac{\partial V_i}{\partial x} = \frac{\partial V_a}{\partial x} \Big|_{\lambda=0} \quad \left. \begin{array}{l} \text{Letzte Gleichung} \\ \hline \end{array} \right\}$$

$$\frac{\partial V_i}{\partial x} = -2\pi \rho \int_0^\infty \frac{x}{(a+x) D}$$

$$\tilde{V}_i = -2\pi \rho \int \frac{ds}{D} \left( \frac{x}{a+x} + \frac{1}{b+x} + \frac{1}{c+x} \right)$$

~~$$\frac{\partial}{\partial x} \frac{\partial D}{\partial s} = +\frac{1}{2} \frac{(1+\frac{x}{a})(1+\frac{x}{b}) + (1+\frac{x}{b})(1+\frac{x}{c}) + (1+\frac{x}{c})(1+\frac{x}{a})}{(x)(c)}$$~~

~~$$\tilde{V}_i = -4\pi \rho \int \frac{\partial D}{\partial s} = -4\pi \rho \frac{1}{D} \int_0^\infty \left( \frac{1}{a+x} + \frac{1}{b+x} + \frac{1}{c+x} \right)$$~~

~~$$\frac{\partial V_a}{\partial x} = -2\pi \rho \int_\lambda^\infty \frac{ds}{(a+x) D} + 2\pi \rho \int_\lambda^\infty \frac{x}{(a+x) D} \frac{\partial D}{\partial x}$$~~

~~$$\tilde{V}_a = -2\pi \rho \int_\lambda^\infty \frac{ds}{D} \left( \frac{1}{a+x} + \frac{1}{b+x} + \frac{1}{c+x} \right) + 2\pi \rho \left[ \frac{x}{a+x} \frac{\partial D}{\partial x} + \frac{z}{b+x} \frac{\partial D}{\partial z} + \frac{y}{c+x} \frac{\partial D}{\partial y} \right]$$~~

$\frac{2}{D} = 0$

$$\bar{V}_a = \pi \rho \int_0^\infty \left( 1 - \frac{x^2}{a^2+s} - \frac{y^2}{b^2+s} \right) \frac{ds}{(1+t_s) \sqrt{1+\frac{s}{a^2}}} \quad \text{17}$$

$$\frac{\partial V_a}{\partial x} = -2\pi\rho \int_0^\infty \frac{x}{a^2+s} \frac{ds}{D} \quad \text{no powierzchniowy} = -2\pi\rho \int_0^\infty \frac{x}{a^2+s} \frac{ds}{D}$$

$$D = \sqrt{(1 + \frac{1}{a^2})(1 + \frac{1}{b^2})(1 + \frac{1}{c^2})}$$

wymiastawiaj skumny o miedzim zlozieniu :  $b=c=\cancel{a}(1-\varepsilon)$

$$X = -2\pi\rho x \int_0^\infty \frac{ds}{(a^2+s)^{3/2}} \frac{a^3(1-\varepsilon)^2}{[a^2(1-\varepsilon)^2+s]} = -2\pi\rho x^2 \int_0^\infty \frac{ds}{(a^2+s)^{5/2}} \left[ 1 - \frac{2\varepsilon a^2}{a^2+s} \right] = \left[ \int_0^\infty \frac{ds}{(a^2+s)^{5/2}} + 2\varepsilon a^2 \int_0^\infty \frac{ds}{(a^2+s)^{7/2}} \right]$$

$$Y = -2\pi\rho y \int_0^\infty \frac{ds}{(a^2+s)^{5/2}} \frac{a^3(1-\varepsilon)^2}{[a^2(1-\varepsilon)^2+s]} = -2\pi\rho y^2 \int_0^\infty \frac{ds}{(a^2+s)^{7/2}} \left[ 1 - \frac{2\varepsilon a^2}{a^2+s} \right]^2 = \left[ \int_0^\infty \frac{ds}{(a^2+s)^{5/2}} + 4\varepsilon^2 a^2 \int_0^\infty \frac{ds}{(a^2+s)^{7/2}} \right]$$

$$\int_0^\infty \frac{ds}{(a^2+s)^{5/2}} = -\frac{2}{3} \left[ \frac{1}{(a^2+s)^{3/2}} \right] = -\frac{2}{3a^3} \quad \int_0^\infty \frac{ds}{(a^2+s)^{7/2}} = -\frac{2}{5a^5} \quad \int_0^\infty \frac{ds}{(a^2+s)^{3/2}} = -\frac{2}{a^3}$$

$$X = +2\pi\rho x \left[ \frac{2}{3} + \frac{4\varepsilon}{5} \right] = \frac{4\pi\rho}{3} x \left[ 1 + \frac{6\varepsilon}{5} \right]$$

$$Y = 2\pi\rho y \left[ \frac{2}{3} + \frac{8\varepsilon}{5} \right] = \frac{4\pi\rho}{3} y \left[ 1 + \frac{12\varepsilon}{5} \right]$$

$$V = \pi \rho \left\{ \int_0^\infty \frac{ds \cdot a^3}{(a^2+s)^{3/2}} \left( 1 + \frac{s}{a^2} \right) - \int_0^\infty \frac{x^2 a^3}{(a^2+s)^{5/2}} \left( 1 + \frac{s}{a^2} \right) - \int_0^\infty \frac{y^2 a^3}{(a^2+s)^{5/2}} \left( 1 + \frac{s}{a^2} \right) \right\}$$

$$= \pi \rho a^2 \left\{ \left( 2 + \frac{2\varepsilon}{3} \right) - \frac{x^2}{a^2} \left( \frac{2}{3} + \frac{2\varepsilon}{5} \right) - \frac{y^2}{a^2} \left( \frac{2}{3} + \frac{8\varepsilon}{5} \right) \right\}$$

$$\frac{x^2}{a^2} + \frac{y^2}{a^2(1-\varepsilon)^2} = 1$$

$$x^2 + y^2 (1+2\varepsilon) = a^2$$

$$g = 9.831 \left(1 - \frac{54}{191}\right)$$

12:

$$V = -\rho abc \int_0^\infty \left( \frac{x^2}{a^2+s} + \frac{y^2}{b^2+s} + \frac{z^2}{c^2+s} \right) \frac{ds}{D}$$

$$= -\rho (\alpha x^2 + \beta y^2 + \gamma z^2 - \chi)$$

$$\alpha = abc \int_0^\infty \frac{ds}{(a^2+s)D} \quad \beta = \quad \gamma = \quad \chi = \int_0^\infty \frac{ds}{D}$$

bosily a kierunku isty sign do parametru i mnoż. licznika.

$$R = V + \frac{\omega^2}{2} (x^2 + y^2) = \text{const}$$

$$x^2 \left[ \alpha - \frac{\omega^2}{2\pi\rho} \right] + y^2 \left[ \beta - \frac{\omega^2}{2\pi\rho} \right] + z^2 \gamma = \text{const}$$

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1$$

$$\left( \alpha - \frac{\omega^2}{2\pi\rho} \right) a^2 = \left( \beta - \frac{\omega^2}{2\pi\rho} \right) b^2 = \gamma c^2$$

wzór na symetry obrotowej  $\left( \alpha - \frac{\omega^2}{2\pi\rho} \right) a^2 = \gamma c^2$

I). jeśli  $a > c$

~~jeżeli~~

$$\alpha a^2 - \gamma c^2 = \frac{\omega^2}{2\pi\rho} a^2$$

$$\int_0^\infty \frac{ds}{D} \left( \frac{a^2}{a^2+s} - \frac{c^2}{c^2+s} \right) = \int_0^\infty \frac{ds}{D} \underbrace{\left( \frac{1}{1+\frac{c^2}{a^2}} - \frac{1}{1+\frac{s}{a^2}} \right)}_{\text{droższe}}$$

$$\begin{aligned} \alpha &= a^2 c \int_0^\infty \frac{ds}{(a^2+s)^{1/2} (c^2+s)} = \\ \beta &= a^2 c \int_0^\infty \frac{ds}{(a^2+s)^{1/2} (c^2+s)^{3/2}} = \\ &= a^2 c \int_0^\infty \frac{ds}{(a^2+s)^{1/2} (c^2+s)^{3/2}} \end{aligned}$$

poł. średnia średnia

II)  $c < a$  nieskończoność  $c = a(1-\epsilon)$

$$\frac{1}{3} \left[ a^2 \left( 1 + \frac{6\epsilon}{5} \right) - c^2 \left( 1 + \frac{2\epsilon}{5} \right) \right] = \frac{\omega^2 a^2}{2\pi\rho}$$

$$= a^2 \left[ \left( 1 + \frac{6\epsilon}{5} \right) - \left( 1 + \frac{2\epsilon}{5} \right) \right]$$

$$\frac{4}{5} a^2 \epsilon - \frac{4\epsilon \omega^2}{15 \pi \rho}$$

stąd A

$$J_P = \frac{4\pi\rho}{3} a \left[ 1 + \frac{6\varepsilon}{5} \right] = \frac{4\pi\rho}{3} a \left[ 1 - \frac{11\varepsilon}{5} \right]$$

$$J_A = \frac{4\pi\rho}{3} a \left[ 1 + \frac{12\varepsilon}{5} \right] = \frac{4\pi\rho}{3} a \left[ 1 - \frac{12\varepsilon}{5} \right]$$

$$J_P - J_A = \frac{4\pi\rho}{3} a \frac{\varepsilon}{5} = \frac{4\pi\rho}{3} a \frac{\omega^2 a}{5g} = \frac{a^2 \omega^2}{4}$$

$$J_P - J_A = \frac{a \omega^2}{4} + a \omega^2 = \frac{5}{4} a \omega^2 = J \varepsilon$$

$$\frac{J_P - J_A}{J} = \frac{5}{2} \frac{\omega^2}{g} - \varepsilon \quad \left. \begin{array}{l} \text{Cela montre que} \\ \text{le moment d'inertie est constant} \end{array} \right\} \text{Cela montre que}$$

$$\varepsilon = \frac{15}{16} \frac{\omega^2}{\pi\rho} = \frac{5}{4} \frac{\omega^2 a}{g}$$

$$J = \frac{4}{3} \pi \rho a$$

$$\frac{\omega^2 a}{g} = \frac{1}{209}$$

$$\varepsilon = \frac{1}{231} \quad \begin{array}{l} \text{pour la densité} \\ \text{égal à } 1 \end{array}$$

$$\text{et pour la hauteur } h = \frac{1}{297} \text{ m}$$

de Lami

$\frac{\omega}{\pi\rho}$	$\varepsilon$
0	0
0.1007	0.05
0.1868	0.127
0.2247	0.193
0.1551	0.09
0	0

$$(x-1)^2 = 0 \quad \text{soit} \quad x = 1 \quad \text{ou} \quad x = 2$$

$$\frac{\omega}{\pi\rho} = \underbrace{\left[ \left( \frac{x_1}{2} + 1 \right)^2 - \left( \frac{x_2}{2} + 1 \right)^2 \right]^{\frac{1}{2}}}_{\text{distance entre les deux points}}$$

$$\underbrace{\left[ \left( \frac{x_1}{2} + 1 \right) - \left( \frac{x_2}{2} + 1 \right) \right]}_{\text{distance entre les deux points}} =$$

zrąbem dalej it. se pojedynczo tworząc i utrzymując się poza tym poniżej punktem 18

24) jeśli wtedy np. mamy dla jednostki jednostki złożonej z dwóch jednostek E to mamy iż jeśli jedna bierze do 4n<sub>1</sub>, to druga ( $\epsilon$  wynosi co najmniej potem na  $E = E_1$ ) (odpowiednio o przeciwnie)

jeśli ciasto (kula) ma pot.  $E$ , to mówiąc nie zmieniając się mase  $\int \rho dV = M$

wtedy  $\frac{M}{E}$  nazywamy pojemnością jednostki (Capacitatem), z drugiej strony  $\frac{M}{E}$  jest określona (także pojemność jednostki).

Gdyby ~~nie~~ była u kuli żadnej energii, toby takie od nich robić (także pojemność jednostki).

Silę w masy masy bierze zatem  $E = m \cdot c^2 = \frac{mc^2}{a}$

N.p. Kula.

$$U_2 = \frac{4\pi \sigma a^2}{2}$$

$$\frac{\partial U_2}{\partial r} - \frac{\partial U_1}{\partial r} = -4\pi \sigma$$

$$U_1 = +4\pi \sigma a^2$$

$\Rightarrow$  Potencjał kuli = V

$$V = 4\pi \sigma a^2$$

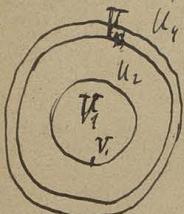
$$= aV$$

$\frac{M}{E} = a$  pojemność kuli = promień

czy kula jest pełna, czy przejmująca  
cały obieg

N.p. w masy d. kuli pojemność jednostki = 1 Farad = kula o promieniu  $a =$

Kula ośrodka potoku kuli jest



Silę masy bierze w środku i zewnętrznie

~~jeśli~~ jest V zawsze symetryczny względem osi z centralnej

$$U_0 = 4\pi \sigma_1^2 b_1 + 4\pi \sigma_2^2 b_2 + 4\pi \sigma_3^2 b_3 = m \cdot c^2 = V$$

$$\left[ U_2 = \frac{4\pi \sigma_1^2 b_1}{2} + 4\pi \sigma_2^2 b_2 + 4\pi \sigma_3^2 b_3 \right]$$

$$U_3 = \frac{4\pi \sigma_1^2 b_1 + 4\pi \sigma_2^2 b_2 + 4\pi \sigma_3^2 b_3}{2} = m \cdot c^2 = V_2$$

$$\left[ U_4 = \frac{4\pi (\sigma_1^2 b_1 + \sigma_2^2 b_2 + \sigma_3^2 b_3)}{2} \right]$$

Tylko możliwe jest  $\sigma_1^2 b_1 = -\sigma_2^2 b_2$ , wtedy  $U_3 = V_2 = 4\pi \sigma_3^2 b_3$

lignie  $U_4 = -U_2$  równie zgodnie z  $\frac{U_4}{U_2} = \frac{1}{2}$

$$U_1 = V_1 = V_2 + 4\pi \sigma_3^2 b_3 \left[ \frac{\sigma_1^2 - \sigma_2^2}{2} \right]$$

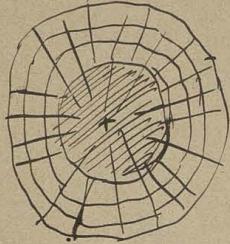
$$1 \text{ Volt} = \frac{1}{300} \text{ J} \\ 1 \text{ Farad} = 9.10^{11} \text{ m}^{-1} \\ 1 \text{ Coul} = 3 \cdot 10^9$$

Janusz ~~zad~~ o mechanice strumieni

20

Geometria przedstawianie

jeśli wiemy iż wzdłuż many wazy pionowej (w nieskończonym) to iloczynowa jest określony

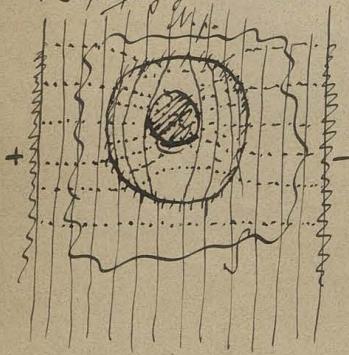


jeśli jednak nie wiemy ile ma opór stromy  $\rho = 16$  w przestrzeni

$S$ , to mogę się zastanowić jak działa gmina inne masy etc.

więc proszę o jakieś streszczenie?

Jak działa gmina  $\rho = \dots$ ?  
Superpowietrze



Prze superpowietrza tyle działa jak wszystko —

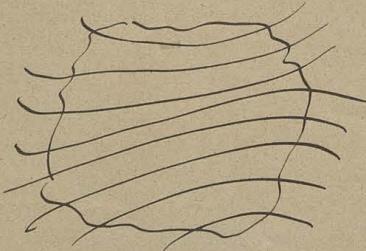
ale jeśli nie wiemy co się dzieje na powierzchni  $S$  się

zauważycie wtedy że dydyna działa właściwie pole pury to  
że podajemy gminie np. wartości na kąt A, aby wykazać  
osiągnięcie.

Gdyby np. spływać proponował: wroclawie w  $S$  dydin  $\rho = 620$

więc  $D^2U=0$  to zauważycie mniej tanie bić pole [przykładek z rachunków

przykrym



jeśli albo nie zauważycie żadnych ich ilości stoli na powierzchni powietrza.

N.p. jeżeli  $V_2 = 0$   ~~$\phi_3 = 0$~~  Punktka Lodzińska:

25

20

$$V_1 = 4\pi a_1 b_1 \frac{a_2 - a_1}{a_2}$$

$$\Phi_1 = 4\pi a_1^2 b_1$$

$$\frac{\Phi_1}{V_1} = \frac{a_1 a_2}{a_2 - a_1} = a_1 \cdot \frac{a_2}{a_2 - a_1}$$

więc wartość  $\frac{a_2}{a_2 - a_1}$  konieczna,

pojawnie

Jaki pojemnikowy ładunek ma zlokalizować:

$$\Phi_2 + \Phi_3 = 0 \quad \cancel{\text{zadanie}} \quad a_2^2 b_2 + a_3^2 b_3 = 0$$

Wówczas upodajmy do średnicy  $\Phi_1$ , jaka taka będzie  $V_1$   $V_2$ ?

~~$\Phi_2 = \frac{a_2}{a_2 - a_1} \Phi_1$~~ 

$$\Phi_1 = -\Phi_2 = \Phi_3$$

$$\text{więc } a_2^2 b_1 = -a_2^2 b_2 = a_3^2 b_3$$

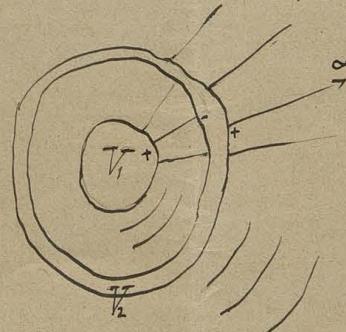
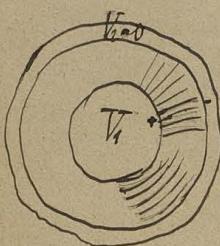
$$V_1 = 4\pi a_1 b_1 \left[ 1 - \frac{a_1}{a_2} + \frac{a_1}{a_3} \right]$$

pojawnie mały ładunek trafić:

$$V_2 = 4\pi a_1 b_1 \left( \frac{a_1}{a_3} \right)$$

$$\frac{\Phi_1}{V_1} = \frac{a_1}{1 - \frac{a_1}{a_2} + \frac{a_1}{a_3}} = a_1 \cdot \frac{a_2}{a_2 - a_1 + a_3}$$

zatem tyle bardziej mały ładunek



worm wówczas liczącym wykroju 2 + jch  
wówczas 4 - iżmów wykroju 2 + dwo

Poziomu pozytywu: niski poziomu jest konieczna klapa pusta  
 jaka  $a_2 - a_1 = \delta$  natomiast dla  $b_1 \propto \delta$ :  
 bieg.  $\infty$

$$\text{I). } V_1 = 4\pi b \frac{\delta}{b + \frac{\delta}{2}} \quad b = \frac{V_1}{4\pi} \delta \\ = 4\pi b \cdot \delta$$

$V_{20}$  //

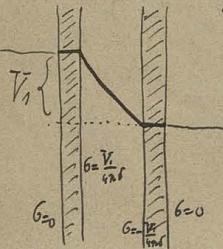
$$\text{II). } V_1 = 4\pi a_1 b_1 \left[ 1 - \frac{a_1}{a_1 + \delta} + \frac{a_1}{a_1 + \delta + d} \right] = 4\pi a_1 b_1$$

$$b_1 = \frac{V_1}{4\pi a_1} = 0 \text{ st.}$$

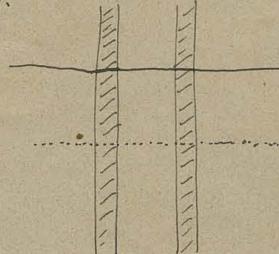
Wypływa z powyższych 2 równań że w tym dla warunków rektyfikacji zmiennego napięcia

wymaga się

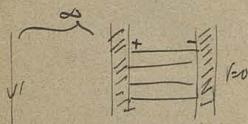
(I).



(II). wymaga się  $b_1 = -b_3$

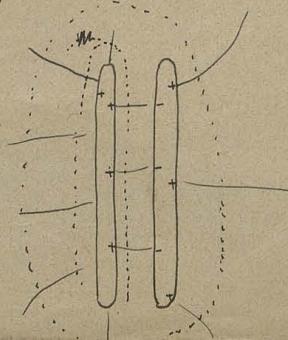
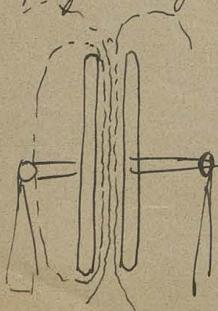


wysokociągowe niskociągowe  
 również na obu stronach  
 przedmiot  
 do tego przenieść



W przypadku gdy w warunkach warstwy Franklina; kondensator Kellensa

(I)

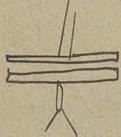


Jaki jest pojemnik?

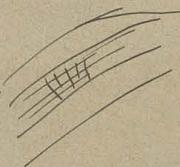
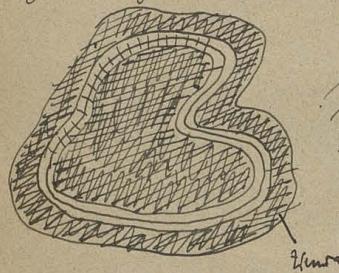
Właściwie się potencjał  $V_1$  do  $\varphi_1 = C V_1$

potem oddzielnie drugie równanie przez co C zaniknie i otrzymamy wtedy  $V'_1 = \frac{\varphi_1}{C} = \frac{C}{c} V_1$

Np. wiadomo np. jądro atomu ujemnych napięć (Volta)



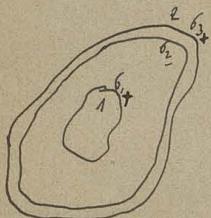
Definicja pojemnika:



$$C = -\frac{1}{4\pi} \frac{\partial U}{\partial V}$$
$$= -\frac{1}{4\pi} \frac{(U_2 - U_1)}{\epsilon_0}$$
$$\varphi_1 = \frac{FV}{4\pi\epsilon_0}$$

Opisując pojemnik  
1) rozważając jedno przekrój  
2) sumując po przekrojach

Skąd pojęcie pojemnika i definicja pojemnika:



2 = pow. pojemnika

Jakże 2 na pot.  $V_2$  to tzw. wewnętrzny potencjał  $V_2 = 0$

Jakże 1 na pot.  $V_1$  to tzw. zewnętrzny potencjał  $V_1 = 0$

$$\text{tzn } \iint \frac{\partial U}{\partial n} d\Gamma = \Sigma_{\text{wew}} = \varphi_1 = -\varphi_2 = \varphi_3$$

Gaussa law or using Green's function

wysokość której wiedzieć do mówiących aktów, występuje na wierzchu; jakże pot.  $V_2$  to zły mówiący

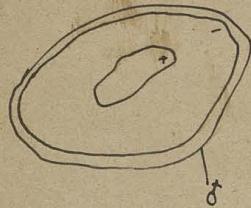
wysokość której wiedzieć do mówiących aktów, występuje na wierzchu; jakże pot.  $V_2$  to zły mówiący

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wysokość której wiedzieć do mówiących aktów, występuje na wierzchu; jakże pot.  $V_2$  to zły mówiący

$V_1 - V_2 : V_1 - V_2 = 0$  a stąd pojęcie pojemnika i skutku jego mówiących aktów

Gdyby tycie n.p. juzem zwyczajne maly.  $V_2 = 0$ :



to one as odrz. i woltka, zasady moga wykryć  
lo many i woltki, zasada elektr. otelecny pośredniczy  
zwizne stek, masy co woltka daje zwizne, wyl-  
mieszanie i zwizne napek woltka.

Wysokie odnosno, zasada zwizna masy pośredniczy zwizne stek, pośredniczy i zwizne  
(takie zwizne gazy)  $\#$  fizyka

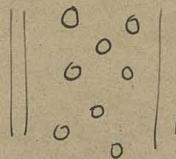
Zasada i odnosno stek zwizna ~~woltka~~ elektrycznego i pośredniczy to zwizne  
na zwizne pośredniczy woltka woltka woltka (Faraday's Law)

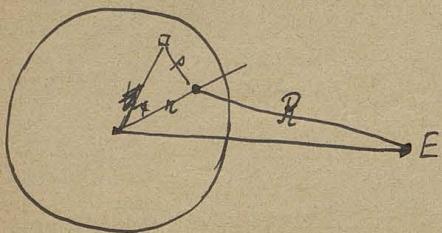
Pravo Newtona jedyne moze skorzystac to zwizne



jednosc zwizni stek pośredniczy masy ogolne kondensatora to  
pośredniczy zwid pośredniczy zwid i takie pojemnosc.

Dielektycza (Lamini - Monta)





$$V_i = U_i + \frac{E}{R}$$

$$U_i = \iint_{\text{loop}} \frac{6a^2 \sin \varphi \, d\varphi \, dy}{\sqrt{a^2 + r^2 - 2ar \cos \varphi}} \iint \frac{df \cdot 6}{s}$$

$$= \iint \frac{6a^2 \sin \varphi \, d\varphi \, dy}{\sqrt{a^2 + r^2 - 2ar \cos \varphi}}$$

my name  $\theta = f_a(\varphi, y)!$

$$= \iint 6a^2 \sin \varphi \, d\varphi \, dy \left[ 1 + \left( \frac{r}{a} \right)^2 - 2 \left( \frac{r}{a} \right) \cos \varphi \right]^{\frac{1}{2}} =$$

$$= a \left[ \underbrace{\iint_{\theta_0} 6 \sin \varphi \, d\varphi \, dy}_{\varphi_0} + \frac{r}{a} \underbrace{\iint_{\theta_1} \dots}_{\varphi_1} + \dots \right]$$

$$U_e = \iint \frac{df \cdot 6}{s} = \iint \frac{6a^2}{r} \sin \varphi \, d\varphi \, dy \left[ 1 + \left( \frac{r}{a} \right)^2 - 2 \left( \frac{r}{a} \right) \cos \varphi \right]^{\frac{1}{2}} =$$

$$= \frac{6a^2}{r} \left[ \iint 6 \sin \varphi \, d\varphi \, dy + \frac{r}{a} \iint \dots \right] = \frac{a^2}{r} \left[ \varphi_0 + \frac{r}{a} \varphi_1 + \dots \right]$$

$$\frac{E}{R} = \frac{E}{\sqrt{r^2 + a^2 - 2ra \cos \theta}} = \frac{E}{r} \left[ 1 + \left( \frac{r}{a} \right)^2 - \dots \right]^{\frac{1}{2}} = \frac{E}{r} \left[ 1 + \frac{r}{a} P_1 + \frac{r^2}{a^2} P_2 + \dots \right]$$

$$a \left[ \varphi_0 + \frac{r}{a} \varphi_1 + \frac{r^2}{a^2} \varphi_2 + \dots \right] + \cancel{\frac{r}{a} \varphi_0 + \frac{r^2}{a^2} \varphi_1 + \frac{r^3}{a^3} \varphi_2 + \dots} + \frac{E}{r} \left[ 1 + \frac{r}{a} P_1 + \dots \right] =$$

const =  $V$

~~200 = 200 - 200~~

$$a \varphi_0 + \frac{E}{r} = V$$

$$\varphi_1 + \frac{EP_1}{r^2} = 0$$

$$\frac{\varphi_2}{a} + \frac{EP_2}{r^3} = 0 \text{ etc.}$$

$$\left. \begin{array}{l} \cancel{a \varphi_0 + \frac{E}{r} = V} \\ \cancel{\varphi_1 + \frac{EP_1}{r^2} = 0} \\ \cancel{\frac{\varphi_2}{a} + \frac{EP_2}{r^3} = 0} \end{array} \right\} \frac{E}{r} \left[ 1 + \frac{r}{a} P_1 + \dots \right]$$

$$U_i = \sum P_n = V - \frac{E}{R}$$

$$U_e = \frac{a^2}{r} \varphi_0 + \frac{a^3}{r^2} \varphi_1 + \dots = \frac{a}{r} V - \left[ \frac{a}{r} \frac{E}{F} + \frac{a^2}{r^2} \frac{EP_1}{F^2} + \frac{a^5}{r^3} \frac{EP_2}{F^3} \right]$$

$$U_e = \frac{E}{R} + \frac{E_a}{r_p} \left[ 1 + \frac{\alpha^2}{r_p} P_1 + \frac{\alpha^4}{r_p^2} P_2 + \dots \right] = \frac{E}{R} - \frac{E_a}{r_p} \sqrt{1 + 2 \frac{\alpha^2}{r_p} \cos \theta + \frac{\alpha^4}{r_p^2}}$$

$$= \frac{E}{R} - E_a \sqrt{r_p^2 + \alpha^4 + 2\alpha^2 r_p \cos \theta}^{-\frac{1}{2}} + \frac{E}{R} \left[ \alpha^2 + r_p^2 - 2\alpha^2 r_p \cos \theta \right]^{\frac{1}{2}}$$

$$\frac{\partial U_e}{\partial r} = -\frac{E}{R^2} + \frac{E_a (\alpha^2 + \alpha^2 \cos \theta)}{\sqrt{r_p^2 + \alpha^4 + 2\alpha^2 r_p \cos \theta}^3} \Big|_{r=R} = -\frac{E}{R} + \frac{E \alpha^2 (1 + \cos \theta)}{\sqrt{\alpha^2 + \alpha^4 + 2\alpha^2 \cos \theta}^3}$$

$$-\frac{E (1 + \cos \theta)}{\sqrt{\alpha^2 + \alpha^4 + 2\alpha^2 \cos \theta}^3}$$

$$= -\frac{E}{R} + \frac{E \alpha^2}{\sqrt{(1 + \cos \theta)^3}} \pm \frac{E (1 + \cos \theta)}{\sqrt{(1 + \cos \theta)^3}} = -\frac{E}{R} + \frac{E (1 - \alpha^2)}{\sqrt{(1 + \cos \theta)^3}}$$

$$= \frac{1}{R} \left[ -V + \frac{E (1 - \alpha^2)}{R^3} \right]$$

Neglect  $V = 0$ :

$$G = -\frac{E(p^2 - \alpha^2)}{4\pi a} \frac{1}{R^3}$$

collocazione massima?

$$\int_0^{2\pi} G \sin \theta d\theta = -\frac{a}{2} E(p^2 - \alpha^2) \int \frac{\sin \theta d\theta}{\sqrt{1 + \alpha^2 - 2\alpha p \cos \theta}^3} = -\frac{a E(p^2 - \alpha^2)}{2\pi p} \sqrt{\frac{1}{1 + \alpha^2 - 2\alpha p \cos \theta}}$$

$$= +\frac{E(p^2 - \alpha^2)}{2\pi p} \left[ \frac{1}{\alpha + p} - \frac{1}{\alpha - p} \right] = -\cancel{\frac{E(p^2 - \alpha^2)}{2\pi p}} \frac{\alpha'}{\alpha}$$

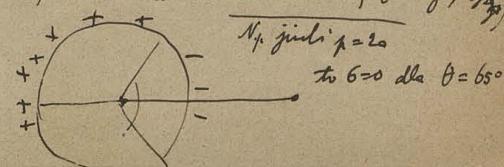
$$= \frac{E}{2\pi p} (1 - \alpha - (\alpha + p)) = -\frac{E\alpha}{p}$$

$$U_e = \frac{E}{R} - \frac{E_a}{R} \frac{1}{\sqrt{r_p^2 + \frac{E^2}{R^2} + 2\frac{E^2}{R^2} \cos \theta}}$$

$$H_i = \frac{E}{R} =$$

zadanie kula byla rozłożona do równie wiele +, równomiernie rozdzielonej (wysoko)

$$zadanie stacjonarne G = \frac{E}{4\pi R} \frac{E}{4\pi a} \left[ \frac{1}{p} - \frac{(p^2 - \alpha^2)}{R^3} \right]$$



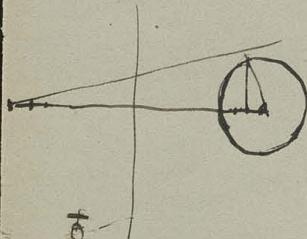
Rückweg, 2. Form  
ne formen wie

23

$$V_i = D \rho f t_2$$

$$\frac{K^2}{S^4} - \frac{K^2}{a^2 + z^2 + 1} = \frac{K^2}{(S^2 + 1)^2}$$

~~cancel~~



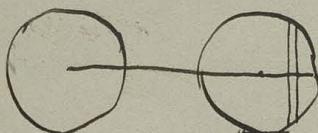
$$W = \frac{1}{2} \sum_m k$$

$$U = \frac{\varphi}{a} -$$

$$W_f \frac{Ea^3}{4\pi^2} \quad \text{z.B.}$$

$$\int_{r=0}^a \frac{r dr}{\sqrt{r^2 - r^2 - \frac{1}{4}a^2}}$$

Dreikantmomente!



$$W = \frac{1}{2} \int \frac{2\pi y^2 dx}{\sqrt{x^2 + y^2}} - \frac{1}{2} \int \frac{2\pi y^2 dr \sin \varphi d\varphi}{\sqrt{r^2 - x^2}}$$

$$\int_{x=a}^{a+\sqrt{a^2 - y^2}} \frac{2\pi y dy dx}{\sqrt{(a+x)^2 + y^2}} = \left[ \pi y^2 \sqrt{(a+x)^2 + y^2} \right]_{y=0}^{y=\sqrt{a^2 - x^2}} = \left[ \pi a^2 + 2ax - (a+x) \right] = \sqrt{2a} \left[ \sqrt{a+x} - (a+x) \right]$$

$$\sqrt{2a} \int \frac{2}{3} \sqrt{(a+x)^3} - ax - \frac{x^3}{2} \Big|_0^a + \frac{5}{3} \pi a^2$$

$$\sqrt{2a} \frac{2}{3} \left( \sqrt{8a^3} - 2a^2 \right) = \frac{8}{3} \pi a^2 - \frac{4a^3}{3} = \cancel{\frac{8}{3} \pi a^2} \quad \cancel{\frac{4a^3}{3}}$$



100

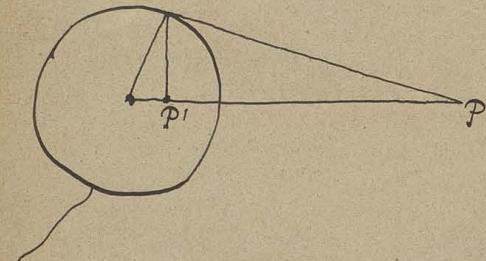
1000



$$\mathcal{U}_c = \frac{E}{[r^2 + p^2 - 2pr\cos\theta]^{\frac{1}{2}}} - \underbrace{\frac{E_a}{[r^2 + p^2 + 2pr\cos\theta]^{\frac{1}{2}}}}$$

$$= \frac{E_a}{p} \frac{1}{\sqrt{r^2 + \left(\frac{a^2}{p}\right)^2 - \frac{2a^2 r \cos\theta}}}$$

to calculate potential energy at any point in elliptical orbit  $\propto \frac{a^2}{p}$



at point  $P'$ , why just to other points  $P$ .

total potential energy within the same

for given elliptical orbit  $\propto E_{\text{tot}}$

$\therefore -\frac{E_a}{p} \propto P'$ , only more catastrophic point

$$P_0 = 1$$

$$P_1 = \cos\theta$$

$$P_2 = \frac{3}{2} (\cos\theta - \frac{1}{3})$$

$$P_3 = \frac{5}{2} (\cos 3\theta - \frac{3}{5} \cos\theta)$$

$$P_4 = \dots$$

greatest potential will be at

$$\frac{E}{r_1} - \frac{E_a}{p r_2} = \text{const}$$

$$\frac{1}{E_{\text{tot}}}$$

$$P_n(x) = \frac{1 \cdot 3 \cdot 5 \cdots (2n-1)}{n!} \left[ x^n - \frac{n(n-1)}{2(2n-1)} x^{n-2} + \frac{n(n-1)(n-2)(n-3)}{2 \cdot 4 \cdot (2n-1)(2n-3)} x^{n-4} - \dots \right]$$

$$(1 + x^2 - 2x\cos\theta)^{-\frac{1}{2}} = 1 - \frac{1}{2}x^2 + x\cos\theta - \frac{-\frac{1}{2} - \frac{3}{2} - \frac{5}{2}}{3} x^4 + \frac{3}{8}(x^4 - 4x^3\cos\theta + 4x^2\cos^2\theta) - \frac{5}{16}(\dots - \dots)$$

$$= 1 + x\cos\theta + x^2 \left( \frac{3}{2} \cos^2\theta - \frac{1}{2} \right) + x^3 \left( -\frac{5}{2} \cos^3\theta - \frac{3}{2} \cos\theta \right)$$

Gdy kolo warstwa pusta, prassi jest  $E$  w gorszach i dalej jest w  
wystawie.

Sile mody  $E$  a kolo



+E

$$F = \frac{E^2}{(2x)^2}$$

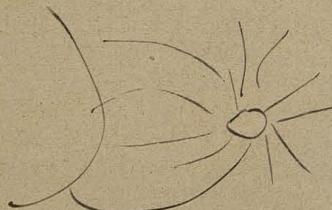
$$F = \frac{Ea}{r} \left[ \frac{1}{(r-\frac{a}{r})^2} - \frac{1}{r^2} \right] = \frac{Ea}{r} \left( \frac{r^2}{(r^2-a^2)^2} - \frac{1}{r^2} \right)$$

$$= \frac{Ea}{r} \frac{2r^2a^2-a^4}{r^2(r^2-a^2)^2} \neq \frac{2Ea^3}{r^7} = \frac{2Ea^3}{r^5}$$

$$W = \frac{1}{2} \sum_k U_k = \frac{1}{2} \frac{Ea}{r} \left( \frac{1}{r-\frac{a}{r}} - \frac{1}{r} \right) = \frac{1}{2} \frac{Ea}{r} \left( \frac{r}{r^2-a^2} - \frac{1}{r} \right) = \frac{1}{2} \frac{Ea}{r} \frac{a^2}{r(r^2-a^2)} = \frac{1}{2} \frac{Ea^3}{r^2(r^2-a^2)} \neq \frac{Ea^3}{2r^4}$$

$$- \frac{\partial W}{\partial r} = \frac{2Ea^2}{r^5} \quad \text{Rozum}$$

Ośmiu influencji



ośmiu stronnych punktów Green's!

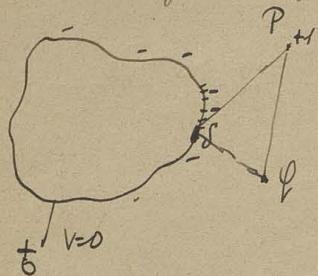
połykrużnicy jasności

W ośmiu kierunkach punktów Green's  
gdy r=nghm z punktu E

$$F_{\text{tot}} = \frac{a}{r^2}$$

reagująca struktura: kolo, kryształ, skrapla  
indukcyjna kolo, kondensator

Wia die gut presteden z. z. funkij. Greens



= potenzial el. struktur; rd. wert von  
induktfij. punkt?

$$U_i = 0 = \frac{1}{r_{p.s}} + \underbrace{\int \frac{6 \, dr}{\rho}}_{F_{p.s})} \text{ no parabol.}$$

$$\text{M. } F_{p.s} = \int \frac{6 \, ds}{\rho_{p.s}}$$

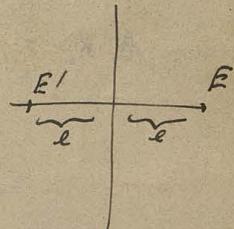
Mendy zuplun analogiam jeh myiny th. obachoveli induktyz jut yfym  
vong tungs punkte tekin alloryi induktyz punkt vong tungs na otoczeniy  
potencialu kubit; th. p'eknij wimy spust

Jedli p'omien kub:  $\lim a = \infty$ :

$$x = a + l$$

$$\lim \frac{-Ea}{l} = -E$$

$$\lim \frac{df}{dl} = \left( 0 - \frac{al}{l} \right) = \lim \frac{a^2 + al - al}{a + l} = l$$



$$U = f(x - h \cos \alpha, y - h \sin \alpha, z) - f(x, y, z)$$

$$= -h \left( \cos \alpha \frac{\partial f}{\partial x} + \sin \alpha \frac{\partial f}{\partial y} + 0 \frac{\partial f}{\partial z} \right) = -h \frac{\partial f}{\partial x}$$

$$f = \frac{1}{r} \quad \text{jedli h} = A,$$

punkt pozyjony

$$U = -A_1 \left[ \cos \alpha \frac{\partial (\frac{1}{r})}{\partial x} + \dots \right] = + \frac{A_1}{r_x^2} (\cos \alpha, \cos \beta, \cos \gamma, \sin \alpha, \sin \beta, \sin \gamma)$$

$$= A_1 \frac{\cos \alpha}{r_x^2}$$

$\lambda_{12}$   
 $\lambda_{11} + A_1$   
 $\lambda_{12}$   
 $-A_1$

$$\begin{aligned}
 U_2 &= \frac{A_1}{2} \left[ f_1\left(x - \frac{\lambda_{12}}{2} \omega_2, \dots\right) - f_1(x, \dots) \right] \\
 &= \frac{A_1}{2} \lambda_{12} \left[ \underbrace{\omega_2 \frac{\partial f_1}{\partial x} + \omega_1 \rho_2 \frac{\partial f_1}{\partial y}}_{\text{distr}} \dots \right] = \cancel{A_1 \frac{\partial f_1}{\partial x}} \cancel{\frac{\partial f_1}{\partial y}} = \frac{1}{2} \frac{\partial^2 f}{\partial x_1 \partial x_2} \\
 &= \frac{A_1}{2} \lambda_{12} \left[ \omega_2 \frac{\partial}{\partial x} \left( \frac{\omega_1 \varepsilon_1}{r^2} \right) + i \rho_2 \frac{\partial}{\partial y} \left( \frac{\omega_1 \varepsilon_1}{r^2} \right) + \dots \right] = \\
 &= \frac{A_1}{2} \lambda_{12} \left[ \omega_2 \frac{\partial}{\partial x} \left( \frac{\omega_1 \varepsilon_1 + i \rho_1 \omega_2 + 2 \omega_1 \varepsilon_2}{r^2} \right) + \dots \right] \\
 &= \frac{A_1}{2} \lambda_{12} \left[ \omega_2 \frac{\partial}{\partial x} \left( \frac{x \omega_1 + y \omega_2 + 2 \omega_1 \varepsilon_2}{r^3} \right) + \dots \right] \\
 &= -\frac{A_1}{2} \lambda_{12} \left[ \frac{\omega_1 \omega_2 + i \rho_1 \omega_2 + i \rho_2 \omega_1 + i \rho_1 \omega_2}{r^3} - \frac{3}{r^3} \frac{x \omega_1 + y \omega_2 + 2 \omega_1 \varepsilon_2}{r} \frac{x \omega_1 + y \omega_2 + 2 \omega_1 \varepsilon_2}{r^2} \right] \\
 &= \frac{A_1}{2} \lambda_{12} \left( \cos \frac{\vartheta}{r} - 3 \sin \varepsilon_1 \sin \varepsilon_2 \right)
 \end{aligned}$$

$$\lim A_1 h_n = \frac{A_1}{2} = \lim A_1 h_n \quad U_2 = \frac{1}{2} A_1 \frac{3 \sin \varepsilon_1 \sin \varepsilon_2 - \sin 2 \varepsilon_2}{r^3}$$

zwei  $(x - \frac{1}{3} \omega_2)$  -- zwei  $\sqrt{n}$  zwei  $\lim A_1 h_n \dots h_n = 1$

Geht ein:  $U_n = (-1)^n \frac{1}{1 \cdot 2 \cdot 3 \cdot \dots \cdot n!} \frac{\partial^n}{\partial h_1 \partial h_2 \dots \partial h_n} \left(\frac{1}{r}\right)$  zwei  $\frac{\partial}{\partial h_2} A_1 h_2 = 1$   
 $\lim A_1 h_n = 1$

$$= \frac{V_n}{r^{n+1}}$$

$V_n$  = fundamental harmonische  $n$ -teile

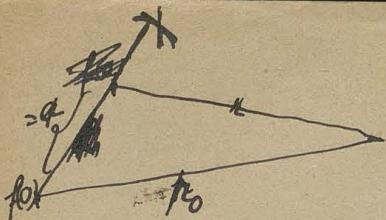
$V_n$  = fundamental harmonische  $n$ -teile

aber zwei wirst hier nur von negativer  $n$  trennen x ~~zwei~~  $\alpha_1 = \alpha_2 = -0$

$$\rho_1 = \dots = \frac{2}{2}$$

$$V_n = r^{n+1} \frac{(-1)^n}{n!} \frac{\partial^n}{\partial h_1 \partial h_2 \dots} = r^{n+1} \frac{(-1)^n}{n!} \left( \cancel{\frac{\partial}{\partial h_1} \cancel{\frac{\partial}{\partial h_2}} \dots} \right) \frac{\partial^n}{\partial x^n} = \frac{1}{n!} \frac{\partial^n}{\partial x^n}$$

$$r = \sqrt{\dots}$$



$$\frac{1}{\sqrt{a^2 + p^2 - 2ap \cos \theta}} = \frac{1}{r} = \frac{1}{r} \left[ 1 + \frac{a^2}{r^2} - \frac{2ap}{r^2} \cos \theta \right]^{-\frac{1}{2}}$$

$$= \frac{1}{r} f_c \left( \frac{a}{r} \right)$$

$$= \frac{1}{r} f_c(x)$$

$$\frac{1}{r} = \frac{1}{2!} \frac{\partial^2 f(x)}{\partial x^2} + \frac{1}{2!} \frac{\partial^2 f(x)}{\partial x^2}$$

$$= \frac{1}{r} \left[ 1 + \frac{a^2}{r^2} P_1 + \frac{a^4}{r^4} P_2 + \dots \right]$$

$$= \frac{1}{r} \left[ f(0) + \frac{1}{2} f'(0) \times \frac{2^2}{2!} f''(0) + \dots \right]$$

$$= \frac{1}{r} \left[ 1 + \frac{a^2}{r^2} \right]$$

$$\frac{1}{r} = f(x_0 - a)$$

$$x_0 = f(x_0) = \frac{V_n}{r^{n+1}} \text{ d}^n$$

$$\frac{1}{r} = \frac{1}{\sqrt{a^2 - 2ax_0 \cos \theta + x_0^2}} = \frac{1}{x_0} + \frac{1}{2!} \left( \frac{\partial(\ln)}{\partial x} \right)_0 + \frac{1}{2!} \left( \frac{\partial^2(\ln)}{\partial x^2} \right)_0 + \dots + \frac{1}{n!} \left( \frac{\partial^n(\ln)}{\partial x^n} \right)_0$$

$$= \frac{1}{x_0} \left[ 1 + \frac{a}{x_0} P_1 + \frac{a^2}{x_0^2} P_2 + \dots \right]$$

zaten w type gevallen  $P_n = V_n$  wic noem daarmjers  $P$  = zgnjch  
zgnjch of hghs  $V$  (stofw, zgnjch Economics)

tenste  $V$  dwig de ghnjchc zgnjch noemend:

$$\frac{1}{\sqrt{a^2 + p^2 - 2ap \cos \theta + r^2 \sin^2 \theta, n(4 - V_n)}} =$$

~~Totale~~ Tungs this U cymg zgnjch noemni  $VU = 0$

Al totale imm noemani:  $V_n r^n = U_n r^{2n+1}$

$$\frac{\partial}{\partial x} (U_n r^{2n+1}) = r^{2n+1} \frac{\partial U_n}{\partial x} + (2n+1) U_n r^{2n+1} \frac{x}{x}$$

$$\frac{\partial^2}{\partial x^2} ( ) = r^{2n+1} \frac{\partial^2 U_n}{\partial x^2} + 2(2n+1) \frac{\partial U_n}{\partial x} r^{2n+1} x + (2n+1) U_n [r^{2n+1} + (2n+1) r^{2n-3} x^2]$$

$$\nabla^2 U_n = r^{2n+1} \underbrace{\nabla^2 U_n + 2(2n+1) r^{2n-1} \left( \alpha \frac{\partial U_n}{\partial x} + \gamma \frac{\partial U_n}{\partial y} + 2 \frac{\partial^2 U_n}{\partial z^2} \right)}_{-U_{n+1}} + (2n+1) U_n 2(n+1) r^{2n-1}$$

$$= r^{2n+1} \nabla^2 U_n = 0$$

$$\frac{\partial}{\partial x} \left[ V_n r^{-n-1} \right] = -(n+1) r^{-n-2} \frac{\partial V_n}{\partial x}$$

$$\frac{\partial}{\partial y} \left[ V_n r^{-n-1} \right]$$

$$U_e = a^n V_n r^{-(n+1)}$$

$$U_i = V_n r^n \cdot a^{-(n+1)}$$

return to dynamic take same about  
- (n+1) job point ordinary  
 $\frac{1}{r} r^{n+2}$

$$G = \frac{1}{4\pi a^2} (2n+1) V_n$$

To take jolbyne molin wazenie

Tak samo jasne sume takich funkciij

$$U_e = \frac{1}{r} \left[ q_0 + \frac{q_1}{r} + \frac{q_2}{r^2} + \dots \right]$$

$$U_i = \frac{1}{a} \left[ 1 + \frac{2}{a} V_1 + \frac{2^2}{a^2} V_2 + \dots \right]$$

$$G = \frac{1}{4\pi a^2} \left[ 1 + 3 V_1 + 5 V_2 + \dots \right]$$

$$\text{Normuj } U_i + \text{Pot}_e = V_i \quad \text{z wazem oznaczenia } V \dots$$

$$\text{pot - tylo } V_e = U_e + \text{Pot}_e \quad i \quad G \quad \text{t.j. tak samo co tenu}$$

$$\text{spojeczeniem przyjaden } U_e = \frac{E}{R} \text{ niepotreblisciu.}$$

Indywidualne tylko kontrolnie w sprawdzanie funkciij  $V$  z  $\text{Pot}_e$

$$\iint \mathcal{P}_n^m ds = \frac{4\pi a^2}{2n+1} \quad . \quad \iint P_n P_m ds = 0$$

~~50~~

$$\mathcal{P}_n = \frac{1, 3, 5, 7 \dots (2n-1)}{n!} \left[ m^n - \frac{n(n-1)}{2(2n-1)} m^{n-2} + \frac{n(n-1)}{2, 4, (2n-1)(2n-3)} m^{n-4} \dots \right]$$

$$\frac{1}{\sqrt{1-2m\theta+m^2}} =$$

$$f(x) = a_0 P_0 + a_1 P_1 + \dots$$

$$a_n = \frac{2^{n+1}}{\pi} \int_{-1}^{+1} f(x) P_n dx$$

$$\int_{-1}^{+1} P_m P_n dx = 0 \quad \frac{2}{2n+1}$$

$$\nabla^2 U = 0 \quad \text{and} \quad \frac{\partial^2 U}{\partial r^2} + \frac{1}{\sin \theta} \frac{\partial (\sin \theta \frac{\partial U}{\partial \theta})}{\partial \theta} + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 U}{\partial \phi^2} = 0$$

$$U = a_0 P_0 + \frac{a_1}{r} P_1$$

$$= b_0 + \frac{b_0}{r} P_0 + \frac{b_1}{r^2} P_1 + \dots$$

$$U = \frac{1}{r} = \frac{1}{\sqrt{1-2rx+r^2}} \quad \frac{\partial U}{\partial x} = -\alpha$$

$$(1-x^2) \frac{d^2 P_m}{dx^2} - 2x \frac{d P_m}{dx} + m(m+1) P_m = 0$$

$$\underbrace{\frac{d}{dx} \left[ (1-x^2) \frac{d P_m}{dx} \right]}$$

$$\int m(m+1) P_m P_m dx = \int P_m \frac{d}{dx} \left[ \frac{d P_m}{dx} \right] dx =$$

$$= (1-x^2) P_m \frac{d P_m}{dx} - \int P_m \frac{d}{dx} \left[ (1-x^2) \frac{d P_m}{dx} \right] dx$$

$$[m(m+1) - m(m+1)] \int P_m P_m dx = (1-x^2) \left[ P_m \frac{d P_m}{dx} - P_m \frac{d P_m}{dx} \right]_{-1}^{+1} = 0$$

$$P_n(x) = \frac{1}{n!} \frac{d^n \left(\frac{x^n}{2^n}\right)}{dx^n} = \frac{1}{n!} \frac{d^n}{dx^n} \left[ \left( x + \frac{1}{2} \right)^n \right]$$

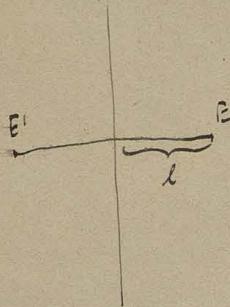
$$\omega \theta = \frac{x}{2} = \xi$$

$$P_n(\xi) = \frac{1}{2^n n!} \frac{d^n (\xi - 1)^n}{d\xi^n}$$

$$\frac{1}{n!} \frac{d^n}{dx^n} \left[ \left( x + \frac{1}{2} \right)^n \right]$$

$$\frac{1}{n!} \frac{d^n}{dx^n} \left[ \left( \frac{\xi}{2} + \frac{1}{2} \right)^n \right]$$

Czy przyjemni punktu E para kier. Taki jak gdyby EI dwa razy?



$$\bar{F} = -\frac{E l}{4 l^2}$$

$$W = \frac{1}{2} \sum_m u = \frac{1}{2} E \frac{EI}{2l} = -\frac{E^2}{4l}$$

$$F_x = -\frac{\partial W}{\partial x} = -\frac{E^2}{4l^2} \text{ strumet!}$$

Analiza

29

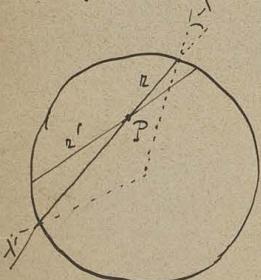
Aż dotąd poznaliśmy więc następujące metody:

- 1). Ze symetrii kuli, połowa odpowiedni wykresów jest oczywista
- 2). <sup>naj</sup> rozszerzający sposób jest przedstawianie równania  $V(x) = 0$  w postaciach i oznaczeniu
- 3). Kula i punkt rozwiniętej powierzchni funkcji kuli
- 4). Rozkład ~~po~~ na poszczególne części, rozwijając z danym ułożeniem

Teraz jeszcze kilka szczególnych metod:

Wykorzystanie jądrowanych albo przedstawień równaniowych

Spojrzać na wersję kuli:



$$\frac{6ds}{r^2}$$

$$\frac{6^{\pm}ds'}{r'^2}$$

$$\frac{6r^2dw}{r^2\sin\lambda}$$

$$\frac{6r^2dw}{r'^2\sin\lambda'}$$

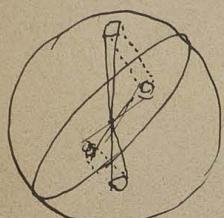
$$\lambda = \lambda'$$

wysokość pierścienia

$$wys. n/a = 0$$

[i mniej pokrocić w tym pojęciu jest to  
mniej  $\frac{1}{r^2}$  jedynie możliwe para typu rodzinny]

Na krzyk!

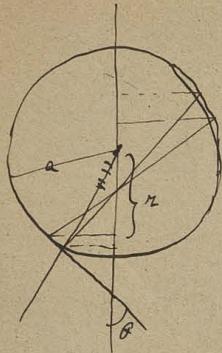


Takie iście przyjmuje następni sposób tego do  
obliczenia całek, i tym samym stawiać zauważoną

$$\frac{6ds}{r^2} = \frac{6ds}{r'^2}$$

$$\left( \frac{6ds}{r^2\sin\lambda} \right)^2 = \frac{6ds}{(r'\sin\lambda)^2}$$

wys. boków zatem wysokość  
jedli wys. tyle obliczając  
wynik na przypisany kątka

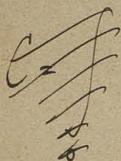


$$\sigma_1 ds_1 = 2s ds$$

$$\sigma_1 = \sigma \frac{ds}{ds_1} = \frac{2s}{\cos \theta}$$

$$\cos \theta = \sqrt{1 - \sin^2 \theta} = \sqrt{1 - \frac{r^2}{a^2}}$$

$$\sigma_1 = \frac{2s}{\sqrt{1 - \frac{r^2}{a^2}}} = \frac{E}{2\pi a^2 \sqrt{1 - \frac{r^2}{a^2}}}$$

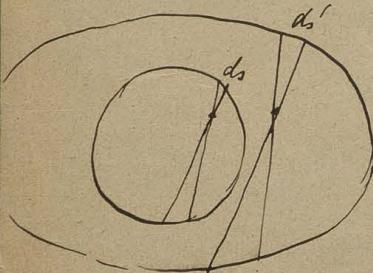


U poziomie stałego magnesium wiodące kreski

$$U = \int \frac{2\pi r dr \sigma_1}{a} = 2\pi \int \sigma_1 dr = \frac{E}{a} \int_0^a \frac{dr}{\sqrt{1 - \frac{r^2}{a^2}}} = \frac{E}{a} \arcsin \frac{r}{a} \Big|_0^a = \frac{E\pi}{2a}$$

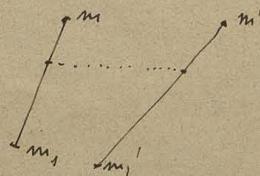
$$C = \frac{E}{U} = \frac{2a}{\pi} = \text{pojumność}$$

Rozszerzanie się tkaniny jadowitej kuli



Każda powierzchnia prosty

na każdej powierzchni wzrostu wylegu równowagowe  
powierzchnie



więc takie w nowej pozycji będą równowagi

Nördlings jordvärten:

$$\varphi = \sum \rho_n \left( \frac{z}{r} - \frac{z'}{r'} \right) = \sum \rho_n \lambda \frac{\partial \left( \frac{z}{r} \right)}{\partial x}$$

$$= \sum \alpha \, dr \frac{\partial \left( \frac{z}{r} \right)}{\partial x}$$

$$\varphi = \int \left( \alpha \frac{\partial z}{\partial x} + \rho \frac{\partial z}{\partial y} + f \frac{\partial z}{\partial z} \right) dr$$

$$= - \int \frac{\frac{\partial \alpha}{\partial x} + \frac{\partial \rho}{\partial y} + \frac{\partial f}{\partial z}}{r} dr + \int \frac{(\alpha_{mn}nx + \rho_{mn}ny + f_{mn}nz)}{r} df$$

$$\alpha = \varepsilon \frac{\partial u}{\partial x} = \int \varepsilon \frac{\nabla u}{r} dr + \int \varepsilon \frac{\partial u}{\partial r} dr$$

$\Sigma$

~~$\int \varepsilon \frac{\partial u}{\partial x} dr$~~

"snell"

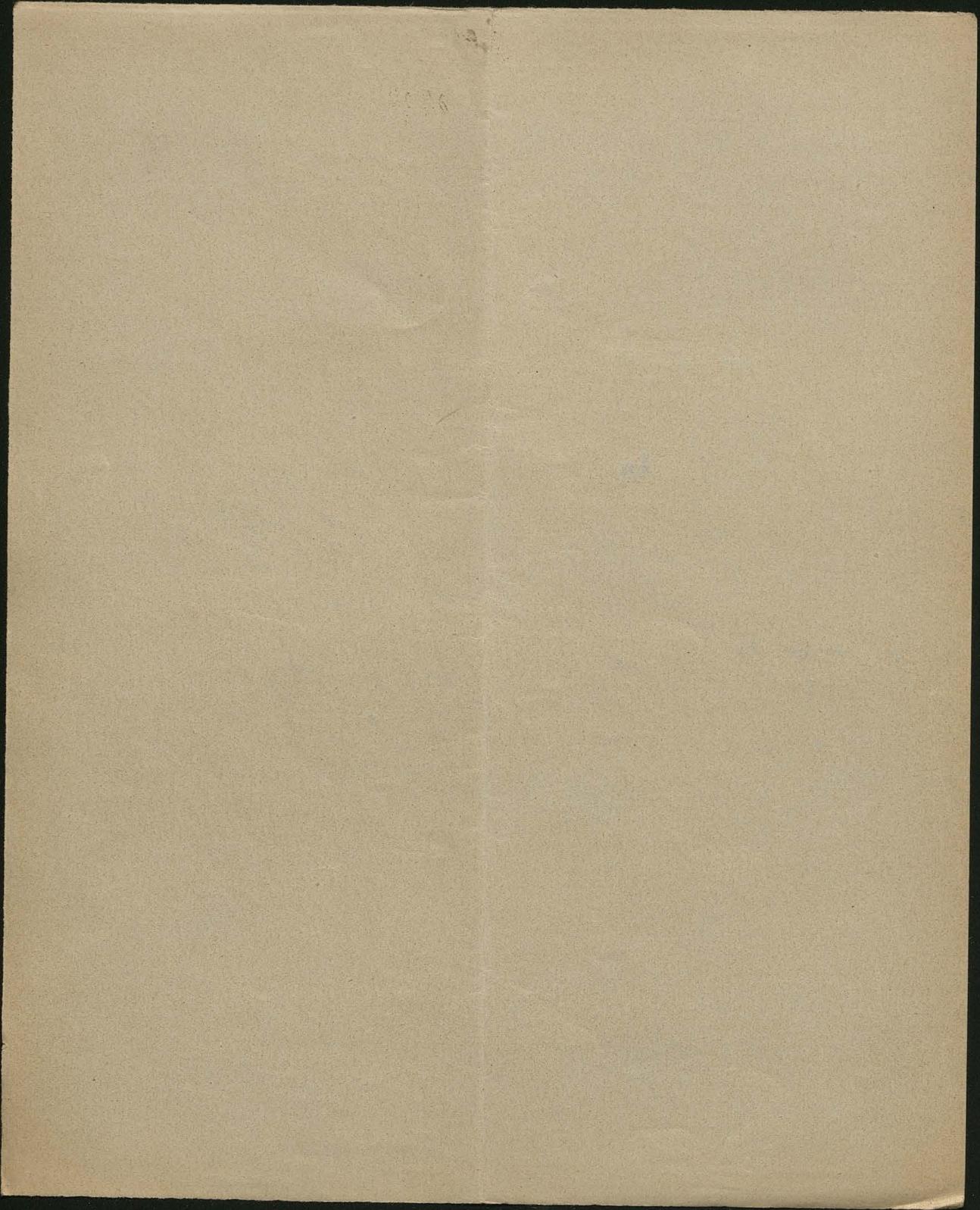
~~$\int \varepsilon \frac{\partial u}{\partial y} dr$~~

~~$4\pi u = \int \frac{\nabla u}{r} dr + \int \left( \frac{\partial u}{\partial r} + \frac{u}{r} \right) dr$~~

$u_{xc}$

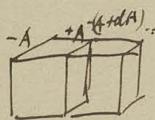
$\frac{\partial \varphi}{\partial x} = 4\pi \varepsilon \frac{\partial u}{\partial x}$

A.d. vissna to res i galaxien



$$\begin{aligned} A_{dw} &= \sum n \lambda_x = \sum n \lambda_w x \\ P_{dw} &= \sum n \lambda_w y \\ C_{dw} &= \end{aligned}$$

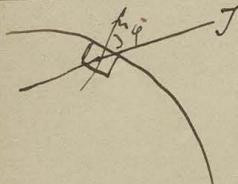
$$J_{dw} = \sum n \lambda$$



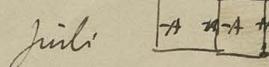
$A dx dy dz$  gerekken moet te zijn voor de hoek  $A dy dz$

waarom niet:  $-[A + \frac{\partial A}{\partial x} dx] dy dz + A dy dz = -\frac{\partial A}{\partial x} dx dy dz = P_{dw}$

$$P = -\left(\frac{\partial A}{\partial x} + \frac{\partial P}{\partial y} + \frac{\partial C}{\partial z}\right)$$



$$J_{wy} = A_{max} \theta_{wy} + C_{wy}$$



juli moment per periode v berekenen x

$$A \text{ tot max is } b = A$$

juli periodes van een punt polygone

$b = \text{afstand van kijkt naar oog}$

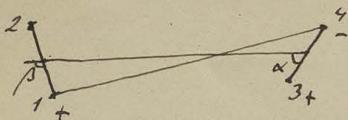
$$= J_{wy} = A_{max}$$

39  
vlieg in polje  $\perp$  do X o zilf  
F ste moment tyd  
 $F A_{dw}$

juli pole na staande X/2  
to voorlangs moment

$$A_{dw} \cdot Y - P_{dw} \cdot X$$

st.



$$W = \frac{1}{2} (m_1 u_1 + m_2 u_2 + m_3 u_3 + m_4 u_4)$$

$$= C + \frac{1}{2} \cancel{\int \int}$$

$$+ \cancel{\frac{1}{4} m_1 m_3} \left[ \frac{1}{r_{13}} + \frac{1}{r_{14}} - \frac{1}{r_{23}} + \frac{1}{r_{24}} \right]$$

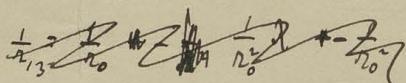
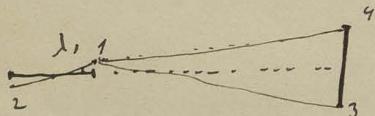
~~1/2 r<sub>13</sub> r<sub>14</sub>~~

$$\frac{1}{2} = \frac{1}{r_0} + \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy + \frac{1}{2} \left[ \frac{\partial^2 u}{\partial x^2} dx^2 + \frac{\partial^2 u}{\partial y^2} dy^2 + \frac{\partial^2 u}{\partial x \partial y} dx dy \right] + -$$



$$r_{13} = \sqrt{(x_1 - x_3)^2 + (y_1 - y_3)^2}$$

$$\frac{\partial u}{\partial x} = \frac{y_1 - y_3}{2R} =$$



$$\left[ (x_1 - x_3)^2 + (y_1 - y_3)^2 \right]^{\frac{1}{2}} = \cancel{\frac{1}{2}} \left[ \cancel{\frac{1}{2}} (R + \lambda_2 \sin \alpha - \lambda_1 \cos \alpha)^2 + (\lambda_2 \sin \alpha - \lambda_1 \cos \alpha)^2 \right]^{\frac{1}{2}}$$

$$= R^{\frac{1}{2}} \left[ 1 + 2 \frac{\lambda_2 \sin \alpha}{R} - 2$$

$$\sqrt{(R - \lambda_1 \cos \alpha)^2 + (\lambda_2 - \lambda_1 \cos \alpha)^2} = R \sqrt{1 - \frac{2 \lambda_1 \cos \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 - 2 \lambda_1 \lambda_2 \cos \alpha}{R^2}}$$

$$\frac{1}{r_{13}} = \frac{1}{R} \left[ 1 - \frac{\lambda_1 \cos \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 - 2 \lambda_1 \lambda_2 \cos \alpha}{2 R^2} + \frac{3}{2} \frac{\lambda_1^2 \cos^2 \alpha}{R^2} - - \right] +$$

$$\frac{1}{r_{23}} = \frac{1}{R} \left[ 1 + \frac{\lambda_1 \cos \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 + 2 \lambda_1 \lambda_2 \cos \alpha}{2 R^2} + \frac{3}{2} \frac{\lambda_1^2 \cos^2 \alpha}{R^2} - - \right] -$$

$$\frac{1}{r_{14}} = \frac{1}{R} \left[ 1 - \frac{\lambda_1 \cos \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 + 2 \lambda_1 \lambda_2 \cos \alpha}{2 R^2} + \frac{3}{2} \frac{\lambda_1 \cos \alpha}{R^2} - - \right] -$$

$$\frac{1}{r_{24}} = \frac{1}{R} \left[ 1 + \frac{\lambda_1 \cos \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 - 2 \lambda_1 \lambda_2 \cos \alpha}{2 R^2} + - \right] +$$

$$\frac{1}{\tau_{ij}} = \frac{1}{\tau_{11}} + \frac{1}{\tau_{22}} + \frac{1}{\tau_{33}} = \\ = \frac{1}{R} \left[ -\frac{4\lambda_1 \lambda_2 \alpha^2}{R^2} \dots \right] \mu_1 \mu_3$$

32

$$2\lambda_1 \mu_1 = M_1 \\ 2\lambda_2 \mu_2 = M_2$$

$$W = -M_1 M_2 \frac{\alpha^2 \omega}{R^3}$$

$$\frac{\partial W}{\partial \alpha} = - \frac{M_1 M_2}{R^3} \cancel{\omega}$$



~~$$\mu_1 \lambda_2 \omega \varepsilon = M^H \omega \varepsilon = -K \frac{\partial \varepsilon}{\partial r}$$~~

$$\frac{\partial \varepsilon}{\partial r} = - \frac{MH}{R} \varepsilon$$

$$\varepsilon = \varepsilon_0 \sin \alpha r t$$

$$\alpha^2 = \frac{MH}{K}$$

$$T = 2\pi \sqrt{\frac{K}{MH}}$$

$$T' = 2\pi \sqrt{\frac{K+K}{MH}} \quad \left. \right\} \text{2 vays MH moins gyroscopie}$$

$$\frac{1}{R} \left[ 1 + \frac{\lambda_2 \omega \beta - \lambda_1 \omega \alpha}{R} + \frac{\lambda_1^2 + \lambda_2^2 - \lambda_1 \lambda_2 \omega(\alpha - \beta)}{R^2} \right]$$

$$1 = \frac{1}{2} \frac{\lambda_2 \omega \beta - \lambda_1 \omega \alpha}{R} + \frac{\frac{\lambda_1^2}{4} + \frac{\lambda_2^2}{4} - \frac{\lambda_1 \lambda_2}{2} \omega(\alpha - \beta)}{2R^2} + \frac{\frac{3}{4} (\lambda_2 \omega \beta - \lambda_1 \omega \alpha)^2}{R^4}$$

$$- \left[ 1 - \frac{1}{2} \frac{\lambda_2 \omega \beta + \lambda_1 \omega \alpha}{R} - \frac{\frac{\lambda_1^2}{4} + \frac{\lambda_2^2}{4} - \frac{\lambda_1 \lambda_2}{2} \omega}{2R^2} \right]$$

$\approx (-\alpha + \beta)$

$$D = \frac{MM'}{R^3} \left[ \frac{n(\alpha - \beta)}{2} - \frac{3n\alpha \omega \beta}{2} \right] + \frac{L}{R^5}$$

$$\alpha = \frac{n}{2} + \varepsilon$$

$$n = n - \varepsilon$$

$$n = \frac{3n}{2} - \beta$$

$$\mu_n = \frac{n}{2} - \alpha$$

$$n - \beta \rightarrow$$

$$\cancel{\alpha = 0/n}$$

$$D = \frac{MM'}{R^3} n \beta + \frac{L}{R^5} = \mu \lambda \cdot H \omega \beta$$

$$Tg^2 = ctg \beta = \frac{M'}{H R^3}$$

$$\beta = n - \varepsilon \quad \alpha = \frac{n}{2}$$

$$D = \frac{MM'}{R^3} [ \cancel{n} - \omega \varepsilon + 3 \omega \varepsilon ] = \frac{2MM' \omega \varepsilon}{R^3} = \frac{M H n \varepsilon}{R^3}$$

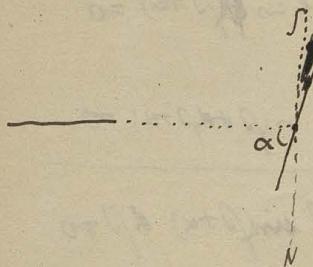
$$Tg^2 = \frac{2M'}{H R^3}$$

Strij do potrindensia mera  $\frac{1}{R}$ ; drukdienis sterk  $\frac{M}{H}$

korren z ojny struktury  $M/H$  dgi  $H/M$

$$[\sin(\beta-\alpha) + 3 \sin \alpha \cos \beta] \frac{MM'}{R^3} + \frac{L}{R^5} = 0$$

33



$$\beta = 0$$

$$2 \sin \alpha \frac{MM'}{R^3} = MH \sin \alpha$$

$$\tau_{\Sigma} = \tau_{\Sigma} = \frac{2M'}{HR^3}$$

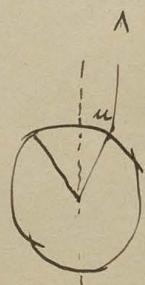
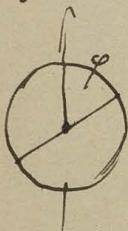


$$\rho = \frac{\pi}{2} \parallel \alpha = \varepsilon$$

$$\text{und } \frac{MM'}{R^3} = MH \sim \varepsilon$$

$$\tau_{\Sigma} = \frac{M'}{HR^3}$$

Reaktionen



~~Wirkung~~

$$D(\varphi - u) = HM \sin u$$

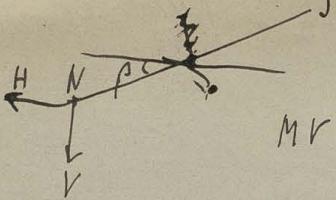
~~Dosis~~

~~(H+ΔH)~~

$$D(\varphi + \cancel{H} - u - du) = \cancel{HM} \sin(u + du - \Delta d)$$

$$D(\varphi - u) - D(u) = dH \cdot M \cdot \sin u + HM \cos u (du - \Delta d)$$

$$\frac{-du}{\varphi - u} = \frac{dt}{H} + \frac{\cos u}{\sin u} (\Delta d)$$



Waya Lloyd

$$M V \sin \beta - M H \cos \beta + P \sin(\beta + \alpha) = 0$$

$$M(V + dV) \sin(\beta + d\beta) - M(H + dH) \cos(\beta + d\beta) + PL \sin(\beta + \alpha) d\beta = 0$$

$$\begin{aligned} M dV \sin \beta &= \cancel{M H \sin \beta} - \cancel{M dH \cos \beta} + PL \sin(\beta + \alpha) d\beta = 0 \\ &\quad + M H d\beta \cancel{\sin \beta} \end{aligned}$$

Jadi  $\beta = 0$ :

$$MV + PL \sin \beta = 0$$

$$M \Delta V + (MH + PL \sin \beta) \Delta \beta = 0$$

$$\Delta V = - \Delta \beta \left[ MH - MV \frac{\sin(\beta + \alpha)}{\sin \beta \cos \alpha} \right]$$

$$\frac{M}{M_i} = \frac{V - H}{V + H} \tan i$$

$$\Delta V = \Delta \beta \cdot V \left[ \tan(\beta + \alpha) - \tan i \right]$$

34

POLSKIE  
TOWARZYSTWO PRZYRODNIKÓW  
IM. KOPERNIKA.



*Lwów dnia* .....

(-+)

$$\Delta \varphi = e^{\Delta x} \frac{\partial f}{\partial x} = \text{---}$$

$$e^{\left(\Delta x \frac{\partial}{\partial x} + \Delta y \frac{\partial}{\partial y} + \Delta z \frac{\partial}{\partial z}\right) \frac{1}{2}}$$

$$\rho = \sum \quad \varphi = \int \left( f \frac{\partial \psi}{\partial x} + g \dots + h \right) dx$$

~~$\frac{\partial \psi}{\partial x} = \frac{\partial \psi}{\partial x} + \frac{\partial \psi}{\partial y} + \frac{\partial \psi}{\partial z}$~~

$$\rho = \frac{\partial \beta}{\partial x} + \frac{\partial \gamma}{\partial y} + \frac{\partial \kappa}{\partial z}$$

$$f = \varepsilon X = \cancel{\frac{\partial}{\partial x} (\alpha + \beta y)} = \varepsilon \frac{\partial U}{\partial x}$$

$$g =$$

$$h =$$

$$\rho, V = \varepsilon (\nabla U)^*$$

$$-\nabla p = -\nabla \varepsilon \nabla U = \nabla \varepsilon U \quad \delta_p = \varepsilon \frac{\partial U}{\partial n} = \cancel{\varepsilon \left( \frac{\partial U}{\partial n} + \frac{\partial U}{\partial x} \right)}$$

$$\delta_p = -\frac{1}{m} \frac{\partial U}{\partial n} = -\frac{1}{m} \left( \frac{\partial U}{\partial n} + \varepsilon \frac{\partial V}{\partial n} \right)$$

$$\frac{\partial V}{\partial n} = -\nabla \varepsilon \frac{\partial V}{\partial n} + \frac{\partial U}{\partial n}$$

$$f = -\varepsilon \frac{\partial V}{\partial x}$$

~~$\varepsilon \nabla V + \nabla (\varepsilon U) = \rho \vec{v}$~~

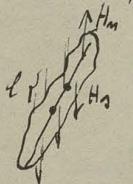
\*<sup>\*)</sup> Ce que nous avons trouvé n'est pas la distance moyenne, mais la racine  
du carré moyen de la distance. D'après les formules ( ) et ( ) de mon mémoire  
précédent (Bullet. Crac. 19) il faudrait la multiplier

Dawnych typu magnetyzmu Coulomb-Poisson przekształcione z delta

elementarny magnes; sygnały prop do  $H, V_i$

$$A = J_{\text{tot}} \quad V = J_{\text{tot}}$$

zadni reaktywny  $A = n = \sum s_i H$



wyszczególniony moment magnetyczny

$$\xi = \frac{\sum n x}{\sum n} \quad \gamma = \beta =$$

$$\xi' = \frac{\sum s x}{\sum s}$$

$M_m$  os magnetyzmu, bigamy

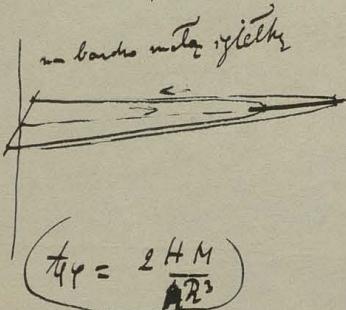
$$M = l \sum n = l \sum s = l \sum m ; m = \text{albo}$$

$$-H \underbrace{l \sum m}_{M} \sin \varphi = K \frac{d \varphi}{dt}$$

$$\tau = 2\pi \sqrt{\frac{K}{HM}}$$

zamianę w  $K$  pula do dawania ~~do dawania~~  
wykonanie może otrzymać  $HM$

trzy złożone prądy,  $H, M$ , trzeba jimm iść w kierunku

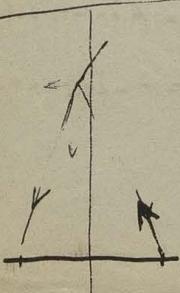


~~H sin phi~~

$$H_m \sin \varphi = m \cos \varphi \cdot \left( \frac{r_1}{R^2} - \frac{1}{r_2} \right)$$

$$= m \cos \varphi \frac{2 \pi l}{R^3} = 2 m \frac{M \cos \varphi}{R^3}$$

"II Hengelby" Gauss



$$H_m \sin \varphi = m \cos \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$\frac{1}{R^2 + \left( \frac{l}{2} - \delta \sin \varphi \right)^2} - \frac{1}{R^2 + \left( \frac{l}{2} + \delta \sin \varphi \right)^2} = \frac{1}{R^2}$$

$$U = nHy + \frac{nN}{\sqrt{y^2 + (x - \frac{\ell}{2})^2}} - \frac{nN}{\sqrt{y^2 + (x + \frac{\ell}{2})^2}}$$

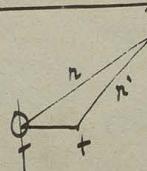
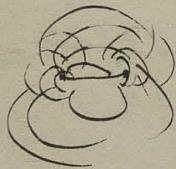
$$\left. \frac{\partial U}{\partial y} \right|_{y=R, x=0} = nH$$

$$\left. \frac{\partial U}{\partial x} \right|_{y=R, x=0} = \frac{nN}{R^3} \left\{ \frac{x - \frac{\ell}{2}}{\sqrt{y^2 + (x - \frac{\ell}{2})^2}} - \frac{x + \frac{\ell}{2}}{\sqrt{y^2 + (x + \frac{\ell}{2})^2}} \right\} = nN \frac{\ell}{R^3} = n \frac{M}{R^3}$$

$$\nabla \phi = \frac{M}{R^3}$$

da oba vrekenen tot de magnetische, totale momenten  $\frac{\alpha}{R^5}$

$$U_n = \frac{n}{r}$$



$$dM = \frac{n}{r} + \frac{I}{2\pi r} = n \left( \frac{1}{r} - \frac{1}{2\pi r} \right) = \frac{n}{r} \cos \theta = -\frac{n\alpha}{r^2}$$

$$U = - \sum \frac{n}{r} \cos \theta = -$$

wie juist many worked n te maken dat  $n = I/r$   $nL = I$

$$U = \int \frac{I \cos \theta dr}{r^2}$$

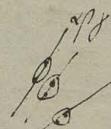
Result magnetisch =  $\Sigma$

Moment momenten  $\omega$ :

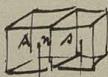
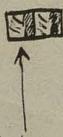
$$Ad\omega = nL \sin \alpha$$

$$Bd\omega = nL \cos \beta$$

$$Cd\omega = nL \cos \gamma$$

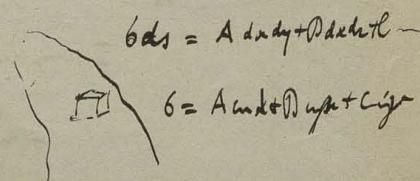


$$J = A_m \omega + B_{up} \omega + C_{up} \omega$$



$$\rho = \left( \frac{\partial A}{\partial x} + \frac{\partial B}{\partial y} + \frac{\partial C}{\partial z} \right)$$

$$Adxdydz = R dydz dx$$



$$d\omega = Adxdy + Bdxdz + Cdxdy$$

$$W = \frac{1}{2} (U_1 U_1 + U_2 U_2) = \frac{1}{2} q (U_2 - U_1)$$

$$U_2 - U_1 = x \frac{\partial U_1}{\partial x} + (a-x) \frac{K_1}{K_2} \frac{\partial U_1}{\partial x} = 4 \pi \epsilon \left[ \frac{x}{K_1} + \frac{a-x}{K_2} \right]$$

$$W = \frac{1}{2} 2 \pi \epsilon^2 \left[ \frac{x}{K_1} + \frac{a-x}{K_2} \right]$$

$$\frac{\partial W}{\partial x} = 2 \pi \epsilon^2 \left[ \frac{1}{K_1} - \frac{1}{K_2} \right] = \text{constant}$$

~~$\mu(\frac{1}{x} - \frac{1}{a-x}) = \mu \text{ und } \frac{d(\frac{1}{x})}{dx} = -\frac{1}{x^2}$~~   $\varphi$   
  
 $\sum \mu \lambda \cdot \frac{d(\frac{1}{x})}{dx}$        $\underbrace{\sum \mu \lambda}_{\text{elementary systems = moment elements.}} \quad = \oint d\varphi$

Wegen der positiven  $\varphi = \int \left[ \oint \frac{\partial \mu}{\partial x} + \oint \frac{\partial (\frac{1}{x})}{\partial x} + \oint \frac{\partial \lambda}{\partial x} \right] dx$   
 & durch polarezgi

$$f = \epsilon X = -\epsilon \left[ \frac{\partial V}{\partial x} - \frac{\partial \varphi}{\partial x} \right] = -\epsilon \frac{\partial U}{\partial x}$$

$$\begin{matrix} g \\ h \end{matrix} =$$

$$\varphi = -\epsilon \int \left[ \frac{\partial U}{\partial x} \frac{\partial \mu}{\partial x} + \dots \right] dx = \epsilon \int \frac{\partial^2 U}{\partial x^2} dx - \epsilon \int \frac{\partial U}{\partial x} \frac{\partial \mu}{\partial x} dx$$

(we consider only  
radial  
discrete, viz  
parabolic profile)

$$\varphi = 4 \pi \epsilon U \stackrel{\text{const}}{=} V - U$$

~~$U = \frac{V}{T + \text{const}}$~~

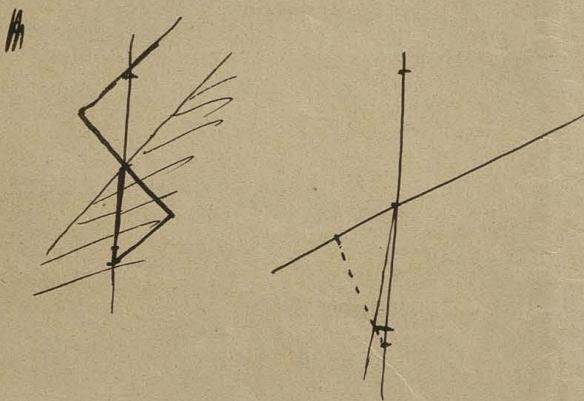
$$\frac{\partial \varphi}{\partial x} = 4 \pi \epsilon \frac{\partial U}{\partial x}$$

$$\frac{\partial K}{\partial x} = (1 + \epsilon_{n\Sigma}) \quad \frac{\partial u}{\partial x} = K \frac{\partial u}{\partial x}$$

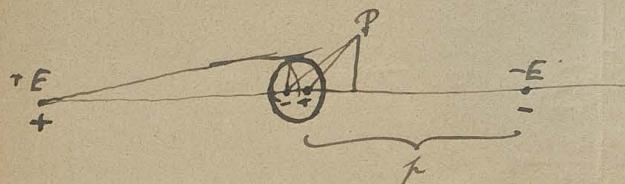
$$\frac{\partial V}{\partial y} = \quad K \frac{\partial u}{\partial y} \quad \text{at.}$$

$$\frac{\partial V}{\partial z} = \quad K \frac{\partial u}{\partial z}$$

$$\nabla^2 V = -\epsilon_{n\Sigma} \rho = K \nabla^2 u \quad \nabla^2 u = -\epsilon_{n\Sigma} (\rho + \rho')$$



Co polega na kuli przenoszącej energię z i o pół jednostkami? 38



Sytomi elektryczny pochodzący z masy i o

Jak daje się mu kula przeno.

$$\text{pot.} = \frac{E}{1+x} - \frac{E}{1-x} = \frac{E}{f} \left[ 1 - \frac{x}{f} - \left( 1 + \frac{x}{f} \right) \right] \\ = - \frac{2Ex}{f^2}$$

$$SIT_0 = \frac{2E}{f^2} = A$$

$$U_e = V_e + \varphi_e$$

$$\varphi_e = \frac{EA}{f} \left[ \cancel{\frac{1}{1+x}} - \cancel{\frac{1}{1-x}} \right] - \lambda \frac{\partial \psi}{\partial x} \\ = + \frac{2EA}{f} \frac{a^2}{f} \frac{x}{r^3} \\ = A \frac{a^3 x}{r^3}$$

$$= A \frac{a^3}{r^2} \cos \varphi$$

$$G = - \frac{1}{4\pi} \frac{\partial \varphi_e}{\partial r} = + \frac{3a^3 x}{4\pi r^5} \Big|_{r=a} = \frac{3}{4\pi} \cos \varphi$$

Wzorami są te rezultaty mówiące styczne wstęp z tamtego rozdziału  
stwierdzając  $K=0$

Dowodzić należy te same wzórki:  $\nabla U = 0$

$$\frac{\partial U_e}{\partial r} = 0$$

Znacząc kąt nachylenia:  $\varphi$  w tymże wypadku mówiąc o stonku  $\frac{K-1}{K+2}$   
to jest wypis ją obliczanie

Wyznaczyć w takich kiel w jednostki objętościowe zapisanej na daleku.

$$\text{To: } n \frac{a^3}{r^2} w\varphi = \frac{K-1}{K+2} \frac{A^3}{r^2} w\varphi$$

$$n \frac{a^3}{r^2} = \frac{K-1}{K+2} = h$$

$$N_p \text{ porostu} \quad K = 1.000590$$

$$h = 0.000197 = 1.97 \cdot 10^{-4}$$

$$\begin{cases} \lambda = \frac{3\pi}{Nmc} \\ c^2 = \frac{3\pi}{Nm} \end{cases}$$

$$\frac{1}{\lambda} = \frac{4\pi b^2}{3} N = \frac{\frac{4\pi b^3}{3} \cdot N}{6} = \frac{8h}{6}$$

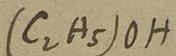
$$b = \theta h \lambda$$

$$\lambda = 95 \cdot 10^{-7} \text{ cm}$$

$$= 8.95 \cdot 10^{-11} = 760 \cdot 10^{-11}$$

$$= 0.76 \cdot 10^{-8} \text{ cm}$$

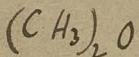
$$\text{Dewar } C_6H_6 : K = 2.2$$



25

$$h \text{ droższa miedziane} = \frac{w_2}{3}$$

$$\sqrt{K} = 7$$



4.5



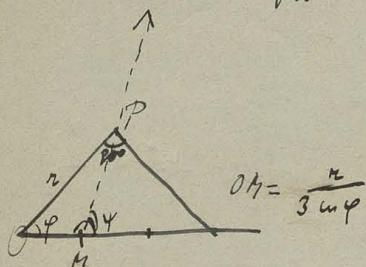
80

$$U = \frac{M}{r^2} \sin\varphi = \frac{Mx}{\sqrt{x^2 + r^2}^3}$$

$$X = \frac{M}{r^3} (3 \sin^2 \varphi - 1) \quad \left. \right\} F = M_p \frac{MP}{r^3 OM}^{39}$$

$$V = \frac{M}{r^3} (3 \cos^2 \varphi)$$

$$F = \frac{\mu M}{r^3} [9 \sin^2 \varphi - 6 \cos^2 \varphi + 1] = \frac{\mu M}{r^3} [3 \sin^2 \varphi + 1]$$



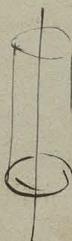
$$\therefore r = \sin(\varphi + \phi) : \frac{2}{3 \sin \varphi}$$

$$\begin{aligned} MP &= \sqrt{r^2 - \frac{r^2}{3 \sin^2 \varphi}} = \frac{2r}{\sqrt{3 \sin^2 \varphi}} \\ &= \cancel{r} \sqrt{3 \sin^2 \varphi - 1} \\ &= OM. \cancel{\sqrt{3 \sin^2 \varphi - 1}} \end{aligned}$$

$$\frac{\sin \varphi}{3 \sin \varphi} = -\sin \varphi \cos \varphi + \cos \varphi \sin \varphi$$

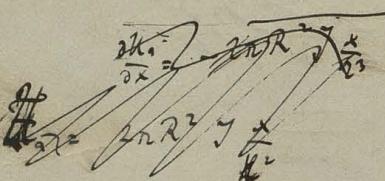
$$\sin \varphi (1 - 3 \cos^2 \varphi) = -3 \cos \varphi \sin \varphi$$

$$\tan \varphi = -\frac{3 \cos \varphi \sin \varphi}{1 - 3 \cos^2 \varphi} = \frac{3 \cos \varphi \sin \varphi}{3 \sin^2 \varphi - 1} = \frac{V}{X}$$



$$-\pi R_p^2 \dot{\varphi} = 2\pi R_p \dot{h} \cdot F$$

$$F = \frac{2\pi R_p \dot{h}}{r}$$



$$2\pi r F = -2\pi r \dot{h} \rho$$

$$\dot{F} = 2\pi r \frac{\rho}{t}$$

$$\dot{F} = \cancel{2\pi r} \cancel{\frac{\rho}{t}}$$

$$U = \cancel{2\pi r^2} \rho$$

$$\dot{U} = 2\pi r \cancel{\rho} x$$

$$U = 2\pi R_p^2 \rho r$$

$$U_r = 2\pi R_p^2 \frac{J_x}{r^2}$$

$$H = \frac{2\pi a^2}{r} \sin \theta \cdot \omega$$

$$\left. \begin{array}{l} U_1 = \frac{4\pi}{3} \left( A^2 - a^2 \right) \\ U_2 = \frac{4\pi}{3} \left( \frac{3}{2} A^2 - \frac{a^2}{2} - \frac{a^3}{r} \right) \\ U_3 = 2\pi a^2 \end{array} \right| \quad \left. \begin{array}{l} U_1 = cx - \frac{4\pi}{3} (A^2 - a^2) \frac{J_{\text{cos}\theta}}{r^2} = \cos \left[ cr - \frac{4\pi}{3} (A^2 - a^2) \frac{J}{r^2} \right] \\ U_2 = cx + \frac{4\pi}{3} \left( - J_{\text{sin}\theta} + \frac{a^2 J_{\text{cos}\theta}}{r^2} \right) = \cos \left[ cr - J \frac{4\pi}{3} r + \frac{4\pi a^2}{3} \frac{J_{\text{cos}\theta}}{r^2} \right] \\ U_3 = cx \end{array} \right.$$

$$c \cos \theta + \frac{8\pi}{3} (A^2 - a^2) \frac{J_{\text{sin}\theta}}{A^2} = \mu \left[ c \cos \theta - \frac{4\pi}{3} J \cos \theta - \frac{8\pi}{3} a^2 \frac{J_{\text{sin}\theta}}{A^2} \right]$$

$$\frac{4\pi}{3} \left[ 2 \left( 1 - \frac{a^2}{A^2} \right) + \mu \left( 1 + \frac{2a^2}{A^2} \right) \right] J = (n-1)c \\ = 4\pi K c$$

$$\mu \left[ \cos \theta - \frac{4\pi}{3} J \cos \theta \right] = c \cos \theta \quad \mu \left[ 1 - \frac{4\pi}{3} \frac{J \cos \theta}{c} \right] \\ \mu J = \frac{(n-1)c}{4\pi \mu} = \frac{Kc}{1+4\pi \mu}$$

$$m \left[ - \frac{1}{2} \left( \frac{re}{ne} \right)^2 \right] \times \int \frac{re}{I} =$$

$$m n \frac{re}{ne} \int \frac{re}{I} = 5 \times 19 \int \frac{re}{I} = 103$$

$$\varphi = \iiint \left[ \alpha \frac{\partial(\frac{f}{n})}{\partial x} + \beta \frac{\partial(\frac{f}{n})}{\partial y} + \gamma \frac{\partial(\frac{f}{n})}{\partial z} \right] dx dy dz = \iint \frac{\alpha \omega_{xx} + \beta \omega_{yy} + \gamma \omega_{zz}}{n} dS$$

$$- \iiint \frac{\left( \frac{\partial \alpha}{\partial x} + \frac{\partial \beta}{\partial y} + \frac{\partial \gamma}{\partial z} \right)}{n} dV$$

$$\varphi = \iint \frac{6_u}{n} dS + \iiint \frac{\rho_f}{n} dV$$

or same Indukcji:

$$\begin{aligned} \alpha &= -k \frac{\partial U}{\partial x} \\ (\text{II}): \quad \beta &= -k \frac{\partial U}{\partial y} \\ \gamma &= -k \frac{\partial U}{\partial z} \end{aligned}$$

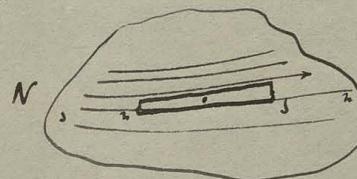
Znaki K. feld:

$$\Psi = \int k \frac{\partial U}{\partial x} + k \frac{\partial U}{\partial y} + k \frac{\partial U}{\partial z} dV$$

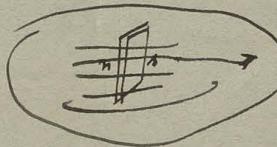
$$\begin{aligned} \rho_f &= - \left( \frac{\partial \alpha}{\partial x} + \frac{\partial \beta}{\partial y} + \frac{\partial \gamma}{\partial z} \right) \\ (\text{III}): \quad \rho_f &= - \left( \frac{\partial}{\partial x} \left( k \frac{\partial U}{\partial x} \right) + \frac{\partial}{\partial y} \left( k \frac{\partial U}{\partial y} \right) + \frac{\partial}{\partial z} \left( k \frac{\partial U}{\partial z} \right) \right) = - \operatorname{div}(k \vec{U}) \end{aligned}$$

(I).

Jak mamy tu moga być konkretnie wtedy?



$S$  ~~area~~  $R + D\varphi$   
w przekroju również  $\int \frac{6_u}{n} dS$   
zauważ, że tam dla y jedynej w ilościach dwoch jest  $\int$



w przekroju również  
 $\int 6_u \frac{dS}{n}$

$$\sqrt{\alpha^2 + \beta^2 + \gamma^2} = J = k \vec{U}$$

$$\begin{aligned} \Rightarrow 2\pi b &\rightarrow 2\pi b \quad L = \vec{U} + 4\pi b (6) \end{aligned}$$

$$\begin{aligned} L &= \vec{U} + 4\pi J \\ &= (1 + 4\pi k) \vec{U} \\ L &= \mu \vec{U} \end{aligned}$$

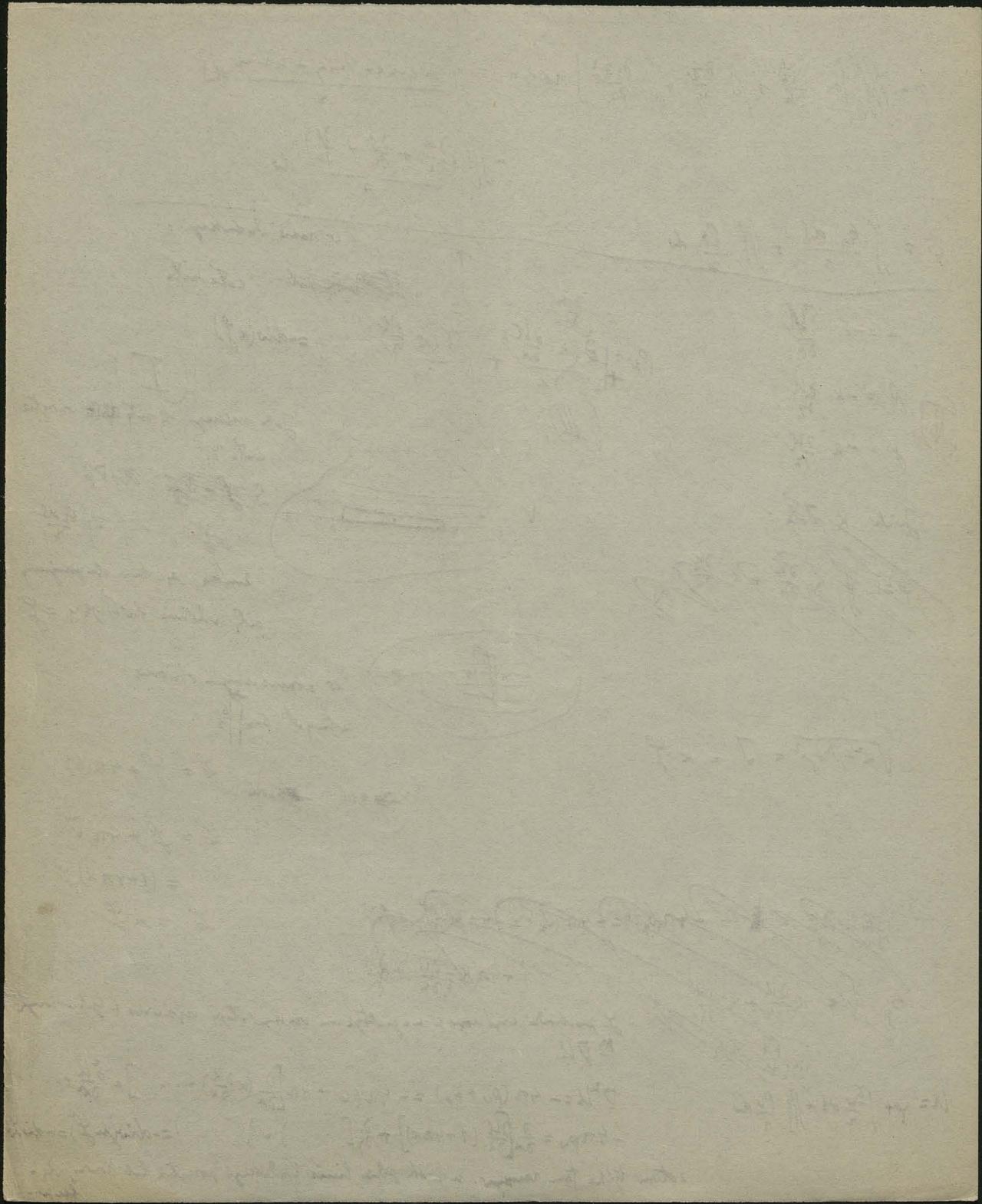
$$\begin{aligned} \frac{\partial \alpha}{\partial x} + \frac{\partial \beta}{\partial y} &= -4\pi (b + \frac{1}{2}) - 4\pi (\frac{1}{2} b) \operatorname{div}(\vec{U}) + \operatorname{div}(\vec{U}') \\ 6_u + \frac{\partial U}{\partial x} &= k \frac{\partial U}{\partial x} + k \frac{\partial U}{\partial y} \end{aligned}$$

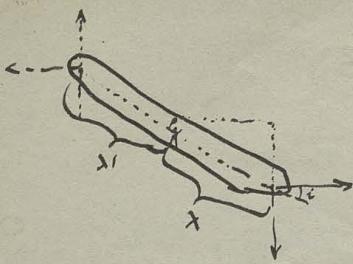
L podaje znaków i negatywnego momentu mimożew i tak powinno być prawidłowe  
 $\approx D\vec{U}$

$$U = \varphi + \int \frac{6_u}{n} dS + \iiint \frac{\rho_f}{n} dV$$

$$\begin{aligned} \nabla^2 U &= -4\pi (\rho_u + \rho_f) = -4\pi \rho_u - 4\pi \left[ \frac{\partial}{\partial x} (k \frac{\partial U}{\partial x}) + \dots \right] = \frac{\partial^2 U}{\partial x^2} + \dots \\ -4\pi \rho_u &= \frac{\partial}{\partial x} \left[ \frac{\partial U}{\partial x} (1 + 4\pi k) \right] + \frac{\partial}{\partial y} [\dots] + \frac{\partial}{\partial z} [\dots] = -\operatorname{div}(k \vec{U}) = -\operatorname{div}(k \vec{L}) \end{aligned}$$

zatem tylko tam rany, myśląc odręcznie indeksy poniekąd lepiej zrozumieć.





$$V_n \lambda_{ni} + V_s \lambda'_{ni} - H_n \lambda''_{ni} - H_s \lambda'''_{ni} + p \delta_{ni} = 0$$

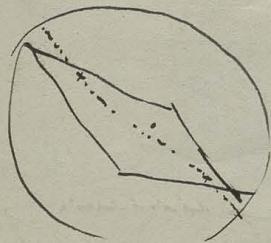
$$M(V_{ni} - H_{ni}) = -p \delta_{ni}$$

$$\tau_{ii}^1 = \frac{H}{V} + p \frac{\delta_{ni}}{M V_{ni}}$$

$$\tau_{ii2}^1 = \frac{H}{V} + p \frac{\sqrt{m(\varepsilon + \eta)}}{M V_{ni}}$$

$$HV = \frac{1}{2} (\tau_{ii}^1 + \tau_{ii2}^1)$$

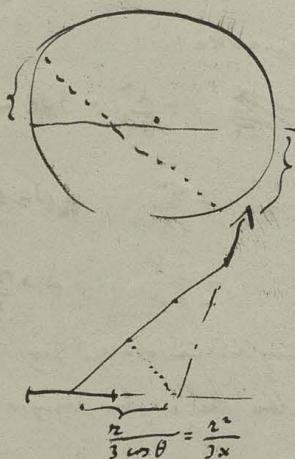
$$\begin{aligned} & (180^\circ \text{ Länge}) \\ & \delta = 9.1 \\ & i = 63.6 \\ & M = 0.107 \end{aligned}$$



Wegen  
durch 0.180°



Mindestens  
zweimal



mindestens  
zwei auf der  
Wegstrecke

Weg von  
Punkt A

$$U = n\left(\frac{x}{r_0} - \frac{\lambda}{2}\right) = n\left[\frac{1}{r_0} + \frac{\lambda}{2} \frac{\partial}{\partial x}\left(\frac{x}{r_0}\right) + \frac{\lambda^2}{2} \frac{\partial^2}{\partial x^2}\left(\frac{x}{r_0}\right) + \frac{\lambda^3}{3!} \frac{\partial^3}{\partial x^3}\left(\frac{x}{r_0}\right)\right] - \left(\frac{x}{r_0} - \frac{\lambda}{2}\right) \dots +$$

$$= n\lambda \frac{\partial}{\partial x}\left(\frac{x}{r_0}\right) + \frac{n\lambda^3}{24} \frac{\partial^3}{\partial x^3}\left(\frac{x}{r_0}\right) = M\left[\frac{x}{r_0^3} + \frac{\lambda^2}{24} \left(-\frac{9x}{r_0^5} + \frac{(5x)^3}{r_0^7}\right)\right]$$

$$\frac{x}{r_0^3} - \frac{3x^3}{r_0^5}$$

$$-\frac{3x}{r_0^5} - \frac{6x}{r_0^7} + \frac{15x^3}{r_0^7}$$

(1) plausibel machen:

$$U = M \frac{\sin \theta}{r_0^2}$$

$$\left. \begin{aligned} X &= \frac{1}{r_0^3} (1 - 3 \sin^2 \theta) \\ Y &= -\frac{3 \sin \theta \cos \theta}{r_0^5} \end{aligned} \right\} F = \frac{1}{r_0^2} \sqrt{1 - 6 \sin^2 \theta + 9 \sin^4 \theta}$$

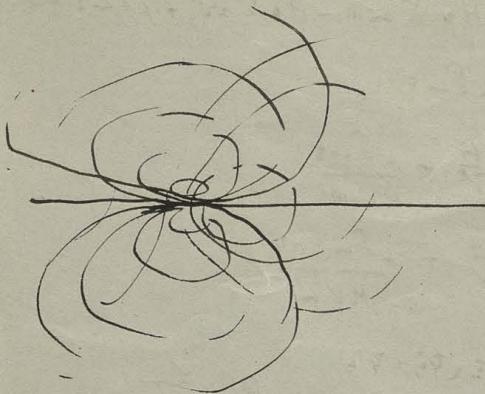
die dann x gegen alle  
 $\theta > 0$

minim alle  $\theta = \frac{\pi}{2}$

Plausibel = 1:2!

$$\begin{aligned} \text{Koeffiz. } \frac{Y}{X} &= -\frac{3 \sin \theta \cos \theta}{1 - 3 \sin^2 \theta} = \frac{y}{x} = \frac{(x - \sqrt{1 - x^2})^2}{3x^2} \\ \text{Koeffiz. } \frac{3xy}{3x^2 - x^2 - y^2} &= \frac{-3xy}{4x^2 - 3x^2 - y^2} = \end{aligned}$$

skewi mörk nivåer H?



$$2m \frac{M}{r^3} \sin\varphi = nH \sin\varphi$$

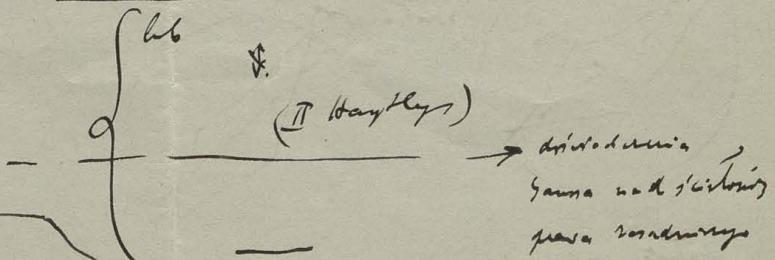
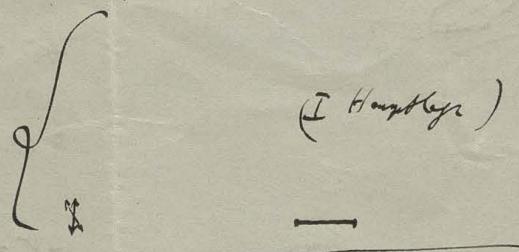
$$\frac{d\varphi}{dt} = \frac{M}{H} \frac{2}{r^2}$$

eller till ochs dyn!

o först uppdelning

$$T = 2\pi \sqrt{\frac{K}{mH}}$$

$$\tilde{T}_1 = 2\pi \sqrt{\frac{K}{m(H \pm \frac{2M}{r^3})}}$$



$$\left(\frac{2\pi}{\tilde{T}_1}\right)^2 - \left(\frac{2\pi}{T}\right)^2 = \frac{2Hm}{K^2}$$

$$\frac{\frac{4}{\tilde{T}_1^2} - \frac{4}{T^2}}{\frac{1}{\tilde{T}_1^2}} = \frac{2M}{H^2 r^3}$$

komma:

$$\cancel{H^2} + \frac{\lambda^2}{8r^2} (-3\cancel{H^2} + 5m^2)$$

$$= 1 + \frac{\lambda^2}{4r^2} \quad K(t) = 0$$

$$1 - \frac{3\lambda^2}{8r^2} \quad \theta = \frac{\pi}{2}$$

eller alla problemet skryt sig  
bort & eller till ovan projekter  
kan var i funnits där i viss  
 $\frac{3}{2}$

Mer tekniskt skryt sig!

riktning!

$$\text{Gelenk polyg} \quad U = \frac{m}{2^{k+1}}$$

42

$$U = m \left( \frac{1}{2^{k+1}} - \frac{1}{2^{k+1}} \right) = m \lambda \frac{\partial}{\partial x} \left( \frac{1}{2^{k+1}} \right) = -m \lambda (1-1) \frac{x}{2^{k+1}}$$

$$\frac{\partial U}{\partial x} = -m (1-1) \left( \frac{1}{2^{k+1}} - \frac{(x+k)}{2^{k+3}} \right)$$

$$\frac{\delta U}{\delta} = +m \frac{\lambda (1-k)x}{2^{k+3}}$$

~~$\theta = 0 \quad X = M(\lambda-1) \frac{x}{2^{k+1}}$~~

~~$\theta = \frac{\pi}{2} \quad X = M(\lambda-1)$~~

wie stromt  $\frac{I_0}{I_{\frac{\pi}{2}}} = \mu$

~~$\frac{I_0}{I_{\frac{\pi}{2}}} = \mu$~~

~~$\frac{I_0}{I_{\frac{\pi}{2}}} = \mu$~~

Orientierung des Polygons:

moment statisch stabil

durch Polarisat.:

Sieg Polyzon

$$-m_2 m_1 \lambda_1 \left( \frac{2}{2^3} - \frac{2}{2^3} \right) = -6 \frac{m_1 m_2}{2^5}$$

~~$m_1$~~

~~$m_2$~~

$$X = -6 \frac{m_1 m_2}{2^5} \text{ gegen X}$$

$$Y = 0$$

X nicht mehr erhalten symmetrisch  
durch V

$$m_2 m_1 \left( \frac{3 \frac{x_4 y}{2^5}}{2^5} - \frac{3 \frac{x_4 y}{2^5}}{2^5} \right) = \frac{3 m_1 m_2}{2^5}$$

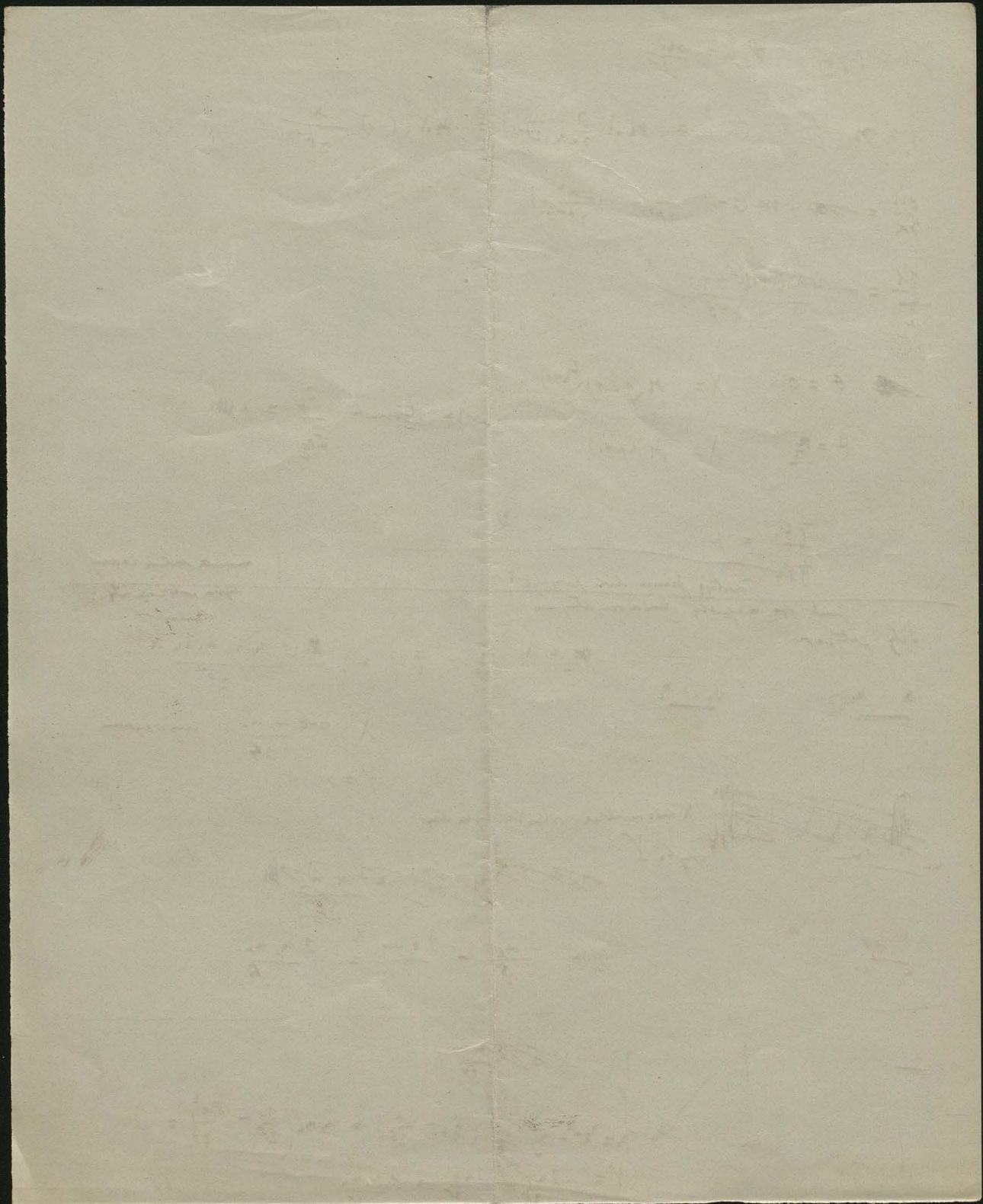
~~$m_1$~~

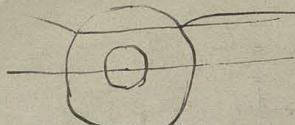
~~$m_2$~~

~~$\frac{3 \frac{x_4 y}{2^5}}{2^5}$~~

~~$x = m_2 \lambda_2 \frac{3}{2^5} \frac{m_1}{2^5} \left( \frac{1}{2^3} - \frac{3 \frac{x_4}{2^5}}{2^5} \right) = m_1 m_2 \left( \frac{3y}{2^8} - \frac{15 \frac{x_4^2}{2^8}}{2^8} \right) = 0$~~

$$Y = \frac{3 \frac{x_4 y}{2^5}}{2^5} - \frac{3 \frac{x_4 y'}{2^5}}{2^5} = \frac{3 m_1 m_2}{2^5}$$



~~Diagram~~

$$\mathcal{U}_1 = \frac{4\pi}{3} \frac{(A^3 - a^3)}{r^2}$$

$$\mathcal{U}_2 = \frac{4\pi}{3} \left( 3A^2 - r^2 - \frac{2a^2}{r} \right)$$

$$\mathcal{U}_3 = 2\pi a^2$$

$$-\frac{4\pi}{3} \frac{(A^3 - a^3) J \ln r}{r^2} + c_1 x = V_1$$

$$\frac{4\pi}{3} \left( -4 J \ln r + \frac{2a^3 J \ln r}{r^2} \right) + c_2 x = V_2$$

()

$$+ c_3 x = V_3$$

$$\frac{4}{3} - 2 = -\frac{2\pi}{3}$$

$$\frac{\partial V_1}{\partial r} = \frac{8\pi}{3} \frac{(A^2 - a^2)}{A^3} \frac{J \ln r}{r} + c_1 \cancel{J \ln r}$$

$$\frac{\partial V_2}{\partial r} = -\frac{8\pi}{3} a^3 \frac{J \ln r}{A^3} + \left( c - \frac{16\pi}{3} J \right) \cancel{J \ln r}$$

$$\frac{\partial V_3}{\partial r} = c \cancel{J \ln r}$$

$$\frac{8\pi}{3} \frac{A^3 - a^3}{A^3} J + c = \mu \left[ \frac{8\pi}{3} \frac{a^2}{A^3} J + \left( c - \frac{16\pi}{3} J \right) \right]$$

$$\frac{8\pi}{3} J + c = \mu c - \frac{16\pi}{3} \mu$$

$$c = \cancel{\frac{8\pi}{3} J (1 + 2\mu)}_{\mu=1}$$

$$\cancel{\left( \frac{8\pi}{3} J + c \right)} = c$$

$$\frac{8\pi}{3} \frac{3A^2 - a^2}{A^3} J = c \cancel{J \ln r (1)}$$

$$\cancel{\frac{8\pi}{3} \left( A^3 - a^3 \right) J + \mu \left( \frac{3}{2} A^2 - \frac{a^2}{2} \right) J} = c \cancel{J \ln r (1)}$$

$$= \frac{8\pi}{3} J \left( 3 + \frac{8\pi}{3} \mu \right) =$$

$$\mu \left[ -\frac{8\pi}{3} J \cancel{J \ln r} + c \cancel{J \ln r} \right] = c \cancel{J \ln r}$$

$$J = \frac{\frac{\kappa c}{2}}{1 + \frac{8\pi}{3} \kappa}$$

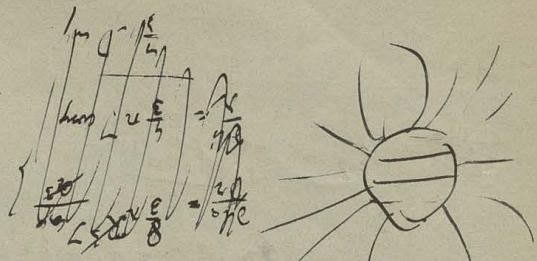
$$J = \frac{c (1 - \mu)}{-8\pi \mu} = \frac{\cancel{\frac{\kappa c}{2}} \cancel{c}}{-\mu}$$

$$\text{मात्रा } \frac{v}{\alpha^2} \text{ की } = \int A \cdot dA + \dots = \int A \cdot dA + \dots$$

$$= \left[ A \cdot \frac{v}{\alpha^2} + \dots \right] =$$

$$= \int A \cos \theta + \dots dA$$

$$= \int \frac{v}{\alpha^2} \cos \theta \cdot dA$$



$$A = \frac{4\pi}{3} r^3$$

$$A = \frac{4}{3} \pi r^3$$

$$\frac{dA}{d\theta}$$

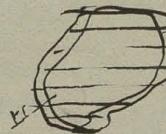


$$dA =$$

$$\frac{\delta}{\sin \theta} d\theta$$

$$\frac{\delta}{\sin \theta} d\theta = \frac{dA}{d\theta}$$

$$\delta =$$



$$dA = \delta \sin \theta$$

3. अधिक परिवर्तन

मात्रा का संबंध

$$K = f(\theta)$$

$$A = K \frac{\partial E}{\partial \theta} \quad \theta = K \frac{\partial E}{\partial \theta} \quad C = K \frac{\partial E}{\partial \theta}$$



4. मात्रा संवर्तन : इसी विधि से  $\Gamma$  प्राप्त होता है।

$$C, \delta = C'$$

जब इसका विलयन 0 हो



5. मात्रा संवर्तन का अर्थ

वह विधि जिसके द्वारा एक गोले की मात्रा निकाली जाती है।

$$U_1 = A_0 + \left[ -A + A \frac{(K-1)}{K+2} \right] r \omega y = A_0 - A \frac{3}{K+2} r \omega y$$

$$U_2 = A_0 + \left[ -A + \frac{A(K-1) r^3}{K+2} \right] r \omega y = A_0 - A \left[ 1 - \frac{K-1}{K+2} \frac{r^3}{2^3} \right] r \omega y$$

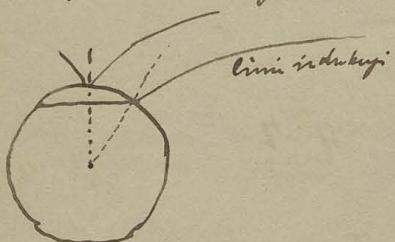
$$\frac{\partial U_1}{\partial z} = -A \frac{3}{K+2} r \omega y$$

$$-\frac{\partial U_2}{\partial z} = -\left(1 + 2 \frac{K-1}{K+2}\right) r \omega y - \cancel{N \frac{\partial A}{\partial z}} = \cancel{N \frac{\partial A}{\partial z}} + \underbrace{\frac{3}{K+2} K r \omega y}$$

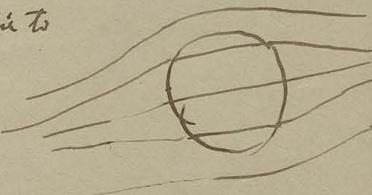
$$K \frac{3}{K+2} + \cancel{1 + 2 \frac{K-1}{K+2}} = 0$$

Wys. wiatru spłonie

Ponieważ  $U_1$  zależy tylko od  $x$ , to linią zatrzymania wiatru aż do końca, tzn. zatrzymywania;  $K_1 > K_2$  oznacza



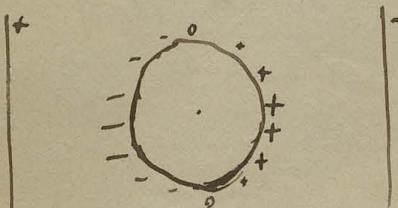
zatrzymuje wiatr



$\rho u^2 / 2 = 0$

$$2 \text{ "na powierzchni? " } \frac{\partial u}{\partial n} = \cancel{\frac{\partial U_1}{\partial n}} + \cancel{\frac{\partial U_2}{\partial n}}$$

$$= + (K-1) \frac{3A}{K+2} r \omega y = + 3 \frac{K-1}{K+2} A r \omega y$$



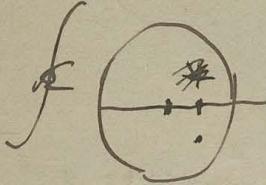
|| Flot leżący na wiatr

$$\sum -\frac{\partial U_1}{\partial x} = A \frac{3}{K+2} \cdot a^2$$

$$\sum -\frac{\partial V_1}{\partial x} = K \frac{3A}{K+2} \cdot a^2$$

$$\int \frac{x}{r^3} dr = \int r \cos \varphi \cdot 2\pi \sin \varphi dr$$

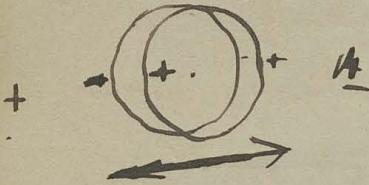
$$= 2\pi \left[ \frac{\sin^2 \varphi}{2} \right]_0^\pi$$

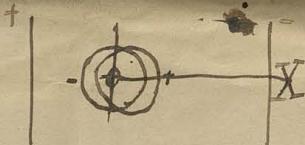


~~$$V_i = 2\pi \mu_0 \left( a^2 - \frac{x^2}{3} \right)$$~~

~~$$2\pi c a^2 - \frac{2\pi M}{3} (x + \delta)^2 - 2\pi c a^2 + \frac{2\pi c x^2}{3}$$~~

$$= \frac{4\pi M x \delta}{3} = \frac{4}{3} \pi c x$$





Lwów dnia

$$\rho_a = C \int \frac{d\varphi}{dx} dx = C \frac{\partial}{\partial x} \left( \int \frac{dx}{r} \right) + C \frac{\frac{4}{3} \pi a^3}{r^2} \cos \varphi = + \frac{4}{3} \pi a^3 c \frac{x}{r^3}$$

$$y_i = \int \frac{x}{r^2} dx = \frac{4}{3} \pi c x$$

Naturalne położenie wiodące do wykresu złożonego z dwóch części



$$V = -Ax + A_0$$

$$\text{Odejmując term. } \frac{\partial V}{\partial x} = \cancel{B} = \cancel{A}x - \cancel{A}$$

$$= A_0 + \left( A + \frac{4}{3} \pi c \right) r \cos \varphi$$

$$\begin{aligned} P^2 U &= P^2 V + P^2 Y \\ &\quad \left. \begin{array}{c} " \\ 0 \\ " \\ 0 \end{array} \right\} \text{wariant} \end{aligned} \quad \left\{ \begin{array}{l} U_1 = A_0 + Ax + \frac{4}{3} \pi c x \\ U_2 = A_0 - Ax + \frac{4}{3} \pi a^3 c \frac{x}{r^3} \\ \quad = A_0 + \left( A + \frac{4}{3} \pi a^3 c \right) r \cos \varphi \end{array} \right.$$

$$K, \frac{\partial U_1}{\partial x} + \frac{\partial U_2}{\partial x} = 0$$

$$U_1 = U_2 \Big|_{x=a}$$

$$K \left[ A + \frac{4}{3} \pi c \right] \cos \varphi + \left[ A + \frac{4}{3} \pi a^3 c \right] \cos \varphi \Big|_{x=a} + \frac{8}{3} \pi a^3 c \frac{x}{r^3} \cos \varphi \Big|_{x=a} = 0$$

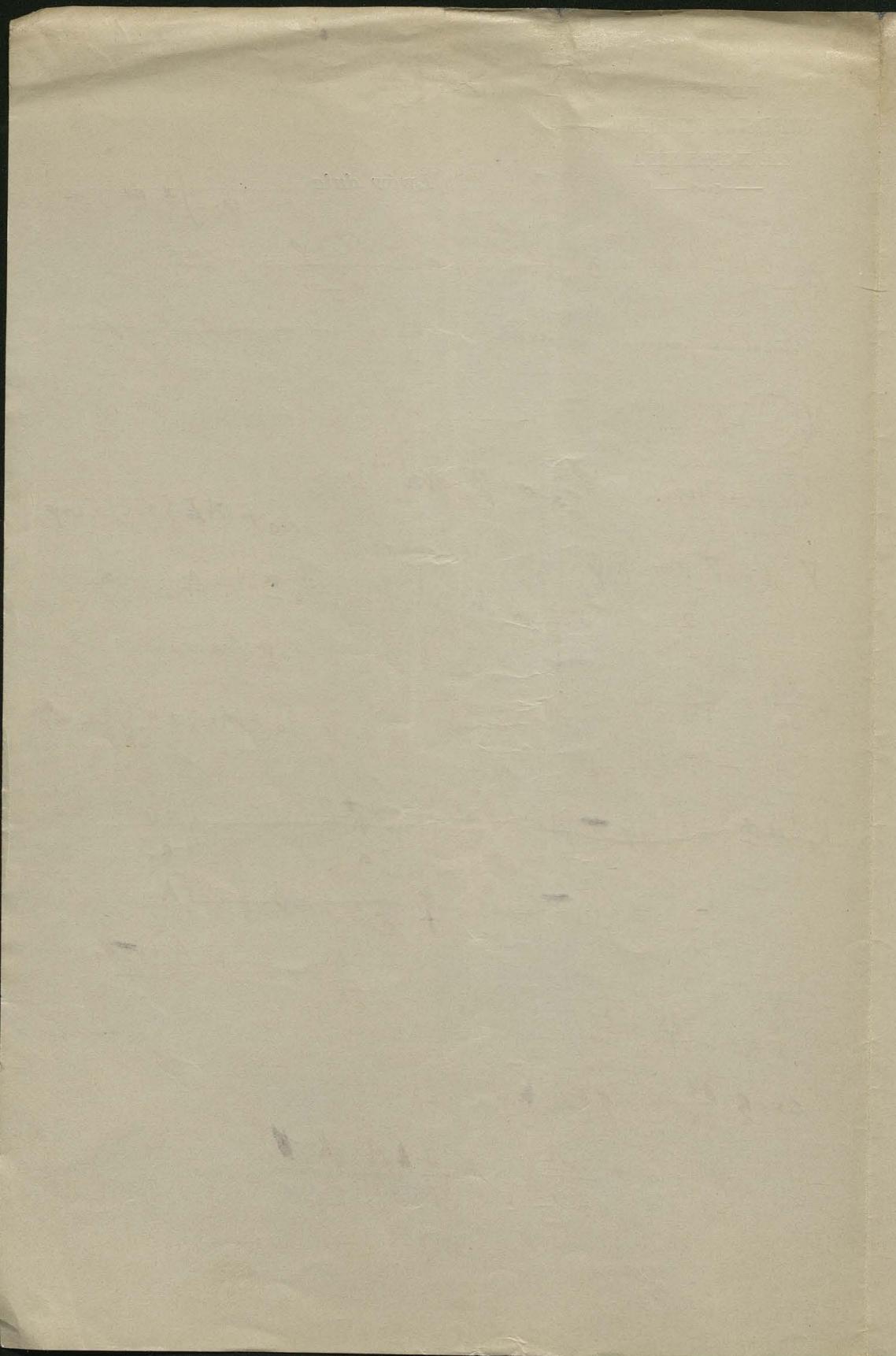
$$(K+1) A + \cancel{\frac{4}{3} \pi a^3 c} \cancel{\frac{8}{3} \pi a^3 c} \frac{4}{3} \pi c [K]$$

$$\cancel{\frac{4}{3} \pi c} = + \frac{A (K+1)}{2}$$

$$C = -\xi \left( \frac{\partial V}{\partial x} + \frac{\partial Y}{\partial x} \right)$$

$$C = -\xi \left( -A + + \frac{4}{3} \pi c \right)$$

$$C = + \frac{\xi A}{1 + \frac{4}{3} \pi \xi} = \frac{3}{4 \pi} \frac{A (K+1)}{2 + K}$$





$$\sum_{\mu \neq \lambda} \left[ \frac{1}{r^{\lambda}} - \frac{1}{r^{\mu}} \right] = \sum_{\mu \neq \lambda} \frac{\partial U_{\mu}}{\partial x} = \alpha \, dx \frac{\partial U}{\partial x}$$

$$\varphi = \int \left( \alpha \frac{\partial U}{\partial x} + \dots \right) ds = - \int \frac{1}{r} \left( \frac{\partial \alpha}{\partial x} + \dots \right) ds + \int \frac{\alpha \omega_{\text{rot}} + \dots}{r} df$$

$$\alpha = \varepsilon \frac{\partial U}{\partial x} = \int \rho'' \frac{ds}{r} + \int \sigma'' \frac{df}{r}$$

$$\begin{aligned} \rho' &= - \left( \frac{\partial \alpha}{\partial x} + \frac{\partial f}{\partial y} + \frac{\partial U}{\partial r} \right) & \sigma'' &= -(\alpha \cos \vartheta + \rho' \sin \vartheta) \\ &= + \varepsilon \nabla^2 U + \left( \frac{\partial \varepsilon}{\partial x} \cdot \frac{\partial U}{\partial x} + \dots \right) & &= + \left( \varepsilon_1 \frac{\partial U_1}{\partial x} + \varepsilon_2 \frac{\partial U_2}{\partial x} \right) \end{aligned}$$

~~$$U = \int \rho' \frac{dr}{r} + \int \sigma' \frac{df}{r} = V + \int \rho'' \frac{dr}{r} + \int \sigma'' \frac{df}{r}$$~~

$$4\pi \rho' = (\rho + \rho'')_{\text{in}}$$

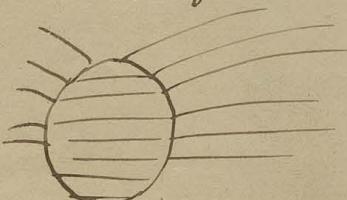
$$4\pi \rho' = 4\pi \left[ -K \nabla^2 U - \dots + 4\pi_2 \nabla^2 U + \dots \right] = -4\pi \nabla^2 U$$

$$4\pi \sigma' = \cancel{4\pi} \left[ K_1 \frac{\partial U_1}{\partial x} + K_2 \frac{\partial U_2}{\partial x} + \varepsilon_1 \frac{\partial U_1}{\partial x} + \varepsilon_2 \frac{\partial U_2}{\partial x} \right]$$

$$= \left( \frac{\partial U_1}{\partial x} + \frac{\partial U_2}{\partial x} \right)$$

vise  $\rho''$  no  
 zrok pravimy  
 do  $\rho' \sigma'$   
 i p zrok  
 pravimy do  $U$

Kula je polna jidrovodnic



Fräzerny je one bydru polazovani  
jidrovodnic

$$\text{tj. je } \frac{\partial U}{\partial x} + \dots = 0$$

$$\alpha \cancel{r^{\alpha}} = c$$

$$\rho = 0$$

$$\sigma = 0$$

$$(\alpha \nabla) Z + [\alpha \text{curl } Z] = \dots$$

47

$$\nabla(\alpha Z) = (\alpha \nabla) Z + (Z \nabla) \alpha + [\alpha \text{curl } Z] + [Z \text{curl } \alpha]$$

$$\text{curl } [\alpha Z] = (Z \nabla) \alpha - (V \nabla) Z + \alpha \text{div } Z - Z \text{div } V$$

$$\text{div } [\alpha Z] = Z \text{curl } \alpha - V \text{curl } Z$$

$$\sum \left( b - m \frac{d^{\alpha} v}{dt^m} \right) dt^m = 0$$

$$\begin{aligned} \sum f dt^m &= \sum m \frac{d^{\alpha} v}{dt^m} dt^m \\ &= \frac{d}{dt} \sum \frac{m}{m} \left( \frac{d^{\alpha} v}{dt^m} \right) dt^m \\ P_1 &= E_1 \end{aligned}$$

$$\begin{aligned} \sum m \frac{d^{\alpha} v}{dt^m} &= 0 \\ \sum m \frac{dv}{dt^m} &= 0 \end{aligned}$$

$$(v \nabla) v = \frac{1}{2} D(v^2) - [v \text{curl } v]$$

$$\frac{dv}{dt} = \frac{\partial v}{\partial t} +$$

$$\frac{\partial \text{curl } v}{\partial t} = \alpha$$

$$\frac{d \text{curl } v}{dt} = \frac{\partial \text{curl } v}{\partial t} - \text{curl } [v \text{curl } v]$$

$$(v \nabla) v - (v \text{curl } v) = \frac{\partial \text{curl } v}{\partial t} + (v \nabla) \text{curl } v$$

$$\begin{aligned} R &= U_0 + V_a(v \cdot U) + V \cdot \text{curl } U v = U_0 + \underbrace{\frac{1}{2} V \text{curl } U v}_{Z} + \underbrace{\frac{1}{2} V \text{curl } U v + P_a(v \cdot U)}_{\text{curl } C = 0} \\ &= \frac{1}{2} U_0 + \frac{1}{2} V(v \cdot U) + V \text{curl } U v \end{aligned}$$

$$\sum f_i (\alpha_{i0} + V_{i0} \omega_i)$$

$$\sum f_i d\omega_i = \sum m \frac{d\tilde{\omega}_i}{dt} d\omega_i$$

$$v = v_0 + V_{r0} \omega$$

$$\frac{dv_0}{dt} + V_{r0} \frac{d\theta}{dt} \quad \frac{d\theta}{dt} = \frac{d\omega_0}{dt} + V_r \frac{d\tilde{\omega}}{dt}$$

$$V_r \gamma = V_{r0} m \frac{d\tilde{\omega}}{dt} d\omega$$

" "   
  $\frac{d\omega_0}{dt}$



$$r = \frac{a}{2} + \alpha V_{r0} N = \frac{z}{2} + y V_{s0} N = a + z \frac{c}{2} V_{s0} N$$

$$\frac{a}{2} + \alpha V_{r0} V_{s0} Z =$$

$$a \sqrt{a^2 - z^2} \alpha^2 = \frac{a}{2} + y \left\{ z \sqrt{z^2 - a^2} - a \cdot z \right\}$$

$$= a + 2 \frac{a-z}{2}$$

$$\frac{a}{2} + \alpha \sqrt{a^2 - z^2} = -y \cdot z^2$$

$$-a^2 = \frac{a}{2} + y \sqrt{a^2 - z^2}$$

Jaki prawidłowy jest?

$$\sqrt{y_2 - y_1} = \frac{1}{\sqrt{q}}$$

48

$$\frac{dx}{dt} = \sqrt{2c \log \frac{a}{x}} \quad -\frac{1}{2} \frac{\sqrt{2c}}{\sqrt{y \frac{a}{q}}} \cdot \frac{1}{q} \frac{a}{y^2} \frac{dy}{dt} \quad X = \frac{c}{x}$$

~~dziedzina~~

$$t = \frac{2k}{a} \left[ \sqrt{s(a-s)} + \frac{a}{2} \arcsin \frac{a-2s}{a} \right]$$

$$dt = \frac{2k}{a} \left[ \frac{1}{2} \frac{a-2s}{\sqrt{s(a-s)}} + \frac{a}{2} \frac{1}{\sqrt{a^2 - (a-2s)^2}} \cdot \frac{-2}{a} \right] ds = -\frac{2}{a} \frac{ks}{\sqrt{s(a-s)}} ds = -\frac{2k}{a} \sqrt{\frac{s}{a-s}} ds$$

$$\frac{ds}{dt} = \frac{a}{2k} \sqrt{\frac{a-s}{s}}$$

$$\frac{ds}{dt} = \frac{a}{2k} \frac{1}{2} \sqrt{\frac{s}{a-s}} \left( -\frac{1}{s} - \frac{a-s}{s^2} \right) ds = -\frac{a}{4k} \sqrt{\frac{s}{a-s}} \frac{2}{s^2} \frac{ds}{dt} = \frac{a^2}{8k^2} \frac{s}{s^2}$$

$$x = \frac{a}{k} (1 - e^{-kt})$$

$$X = -k v_x$$

$$y = \frac{g + bh}{k^2} (1 - e^{-kt}) - \frac{g}{k} t$$

$$Y = -kv_y - gy$$

Zachowani energii wobla, prawo Keplera, Komety  $U + \frac{mv^2}{2} = \text{const}$

W których przypadkach istnieje potencjalny jaka?

1).  $X = +ax$        $U = -\frac{a}{r}(x^2 + y^2) + gy$       2).  $X = ax + by$

~~$y = -bx + g$~~

$Z = +az^2$

~~$Y = -bx + cz$~~

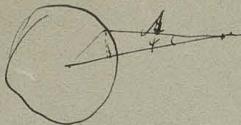
$Z = bz$

3).  $X = +a \sin \alpha y$

$Y = +a \alpha x \cos \alpha y$

$U = -ax \sin \alpha y$

Blaumie sith beprobedis



$$2\pi a^2 \sin \varphi d\varphi \text{ Ma wyr}$$

$$\cos \varphi = \frac{r-a \sin \varphi}{r}$$

etw

$$s^2 = a^2 + r^2 - 2ar \cos \varphi \quad \text{etw}$$

etw

$$\frac{a^2 + r^2 - s^2}{2ar} = \sin \varphi$$

$$r \sin \varphi = -\frac{\partial s}{\partial r}$$

$$2\pi \int \left( \frac{r-a \sin \varphi}{(a^2+r^2-2ar \cos \varphi)^{1/2}} \right)^{1/2} \sin \varphi d\varphi = \int \frac{r - \frac{a^2+r^2-s^2}{2r}}{s^3} \frac{1}{ar^2} \frac{ds}{dr} =$$

$$= \int \frac{r^2 - a^2 + s^2}{2ar^2 s^2} ds = \frac{1}{2ar^2} \int ds + \underbrace{\frac{r^2 - a^2}{2ar^2} \frac{1}{s}}_{\frac{1}{a+r} - \frac{1}{r-a}} \\ \frac{1}{r^2} + \frac{1}{r^2} = \frac{4\pi r}{r^2}$$

---

Blaumie rörmere  $V^2 / (a^2 - r^2)$  up die perihel zim, da n moose

O Frenditegi

Nagnorma tungs kugige: Dron:

Frans punce alle planet wuz würtzige redn

$$\frac{1}{r^2} = 0.00000004$$

die perihel: Nekton:  $T_C = 27^d 7^h 4^m = 2360580 \text{ sec}$

$$R_C = 60^a$$

$$\left( \frac{2\pi R}{T} \right)^2 \frac{1}{R} : g = \frac{1}{R^2} = \frac{1}{a^2}$$

$$g = \frac{4\pi^2}{T^2} \frac{R^3}{a^2} = 4 \cdot \left( \frac{\pi}{T} \right)^2 \cdot 60 \cdot 6370000 \cdot 3600 = 9.8088$$

also ay ti wein alle muijjeus würtzige antike perihel zim?

Juli gestri unius:

Nico & granite

49

$$U = \frac{2\pi^2 \theta mg da}{r} = \frac{4\pi^2 n_6}{r} \quad | \quad \text{Gated}$$

$$\int \frac{4\pi^2 n_6 da}{r} = M \int \frac{\theta da}{r}$$

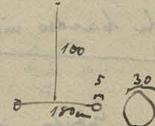
wg - alle punkte zwischen zwei Objekte

so do 2 hemi imputis meridiana pars videtur, perpendic p = 2.5, distm = 5.6

et kqd vienit to?

Peter mister

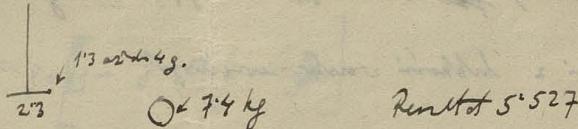
Cavendish sagit meri 5.45



Drys

" " Stokke kvarme

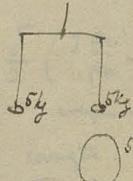
moment kvarme 2  
ann vekten i moment  
berörden



Peter Braun s prisimi: 5.5271      Primi: 5.985 . 10<sup>27</sup>

Litter's turbid pendulum 5.55

Wag enkelt



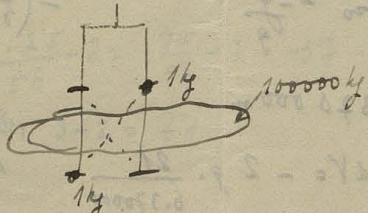
$$\Delta p = 0.589 \text{ mg} \quad \Delta = 5.7$$

Jolly

Rashnik!

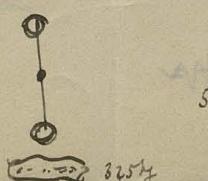
Pozting 5.48

Kjær Russell (granula)



$$\Delta = 5.675$$

Wilking Differential pendulum



Rashnik!

Wiele mamy do dodać innego:

Zborowic pionem Donyue (1749) Chimborazo

Marklynne (1775) Shekhellion  $\Delta = 4' 7$

James & Clarke (1856) Arthurs Seat 5' 32

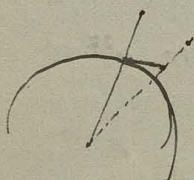
Dwight star body neptuniany 5' 1

Wobacco: Newdehall (1880) Fusi-yama  $\Delta = 5' 77$

Takie (do bardziej nieodpowiednie) re zmiany g w grawitacji

szczególnie gdyby zmiana główcoła, to g zmienia się zgodnie z zmianą grawitacji  
Przykład (Sturmek) ~~z~~ wzrost ~~10000~~ 991 m:  $g = 1.0000885 g_0$

co pochodzi z likwidacji warstw ciekłej



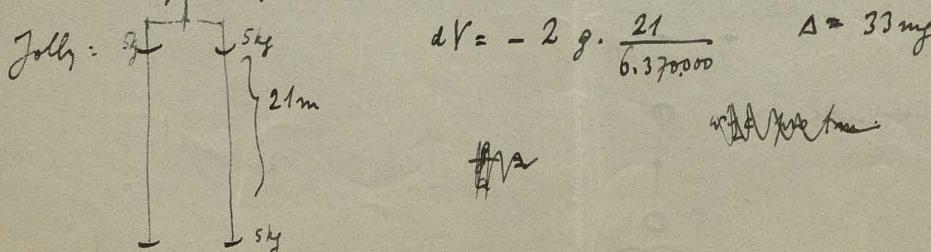
$$V = -g \frac{a^2}{r^2} = g \frac{a^2}{(R+y)^2}$$

$$X = -g \frac{a^2}{(R+y)^2} \cdot \frac{x}{\sqrt{a^2+x^2}}$$

$$\frac{\partial V}{\partial y} = +2g \frac{a^2}{(R+y)^3} \quad |_{y=0} = +2g \frac{a^2}{a^3} = -$$

$$\frac{\partial X}{\partial x} = -g \frac{a^2}{\sqrt{a^2+x^2}} + g \frac{a^2 x}{\sqrt{a^2+x^2}} \Big|_{x=0} = -g \quad -\left(\frac{\partial V}{\partial x} + \frac{\partial V}{\partial y} \frac{\partial y}{\partial x}\right) = -2g + g \frac{a^2}{a^2} = 0$$

zmiana g w głębokości:  $a = 6370000 \text{ m}$



We wachten auf. w.  $\rho_e$  beobachtet mehr:  $\downarrow$  zu progress.

$$\Delta V = + \frac{4\pi k}{a}$$

$$\frac{\frac{4}{3} \rho_e^3 \pi k^2}{a^2} = g_0$$

$$a\rho_m = \frac{3g_0}{4\pi k}$$

$$\frac{\partial V}{\partial r} - \frac{2g}{a} = -4\pi$$

$$\frac{\partial V}{\partial r} = -4\pi + \frac{2g}{a}$$

$$4\pi c \frac{\partial V}{\partial (c\gamma)} = 4\pi k - \frac{2g}{a}$$

$$\text{Faktor berücksichtigt: } V = \cancel{g_0 \frac{M k}{r}} = \frac{M_0 - 4\pi \rho_e \delta}{(a-\delta)} k = g_0 \left[ 1 - \frac{\frac{4\pi \rho_e \delta}{3} k}{(1-\frac{\delta}{a})^2} \right]$$

$$\cancel{V} = g_0 \frac{1 - \frac{3\delta \rho_e}{a \rho_m}}{(1 - \frac{\delta}{a})^2} = g_0 \left( 1 - \frac{3\delta \rho_e}{a \rho_m} \right) \left( 1 + \frac{2\delta}{a} + \dots \right)$$

$$= g_0 \left[ 1 - \delta \left( \frac{3\rho_e}{a \rho_m} - \frac{2}{a} \right) + \dots \right]$$

$$= g_0 \underbrace{\left[ 1 - \delta \left( \frac{3\rho_e}{a \rho_m} - 2 \right) \right]}$$

$$k = 0.000000067 \text{ g/cm}^3$$

$$\frac{6.7 \cdot 10^8 \cdot 12.6}{10^3} - \frac{2}{6.37 \cdot 10^8}$$

$$= 8 \cdot 10^{-10} - 3 \cdot 10^{-9}$$

$$V = g_0 \left[ 1 - \frac{\delta}{a} \left( \frac{3\rho_e}{\rho_m} - 2 \right) + \dots \right]$$

$$\text{erstes: } -2$$

$$\text{minimale jährl. } \rho_e > \frac{2\rho_m}{3}$$

$$\text{zweites: } \frac{3}{5.6} - 2 = -1.4$$

$$\text{drittes: } \frac{3 \cdot 2.5}{5.6} - 2 = \frac{7.5}{5.6} - 2 = -0.7$$

$$\text{w. Rennjährl.: } 3 - 2 = +1$$

$$\text{n.p. } \delta = 1000 \text{ m}$$

$$a = 6.370 \text{ km}$$

$$\frac{1}{64} \% \text{ pro 1 km}$$

Natur oblicie zgodnie z wzorem jasne mi bolo lec wizual:

N.p. Plateau, wysokosci gruboscia  $\delta$

wzory 2 kuli i 2 kugle:

$$V = g_0 \left[ 1 - \frac{2\delta}{a} \right] + \underbrace{\frac{2\pi k T}{2\pi k p_m} \delta}_{p_e} \quad 4\pi k p_m = \frac{3g_0}{a}$$

$$= \frac{3g_0}{2a} \delta \frac{p_e}{p_m}$$

$$= g_0 \left[ 1 - \frac{\delta}{2a} \left( 4 - \frac{3p_e}{p_m} \right) \right]$$

$$\frac{3 \cdot 2}{5 \cdot 6} = 1/3$$

$\underbrace{2/7}$  wyc z umiagniem ~~zapisano~~ na wzorze, ale nie tok zgodny  
jako u Bolomie

umygnajsc przybliznie  $\frac{p_e}{p_m} = \frac{1}{2}$

$$\text{takie } V = g_0 \left[ 1 - \frac{\delta}{a} \left( 2 - \frac{3}{4} \right) \right] = g_0 \left[ 1 - \frac{5\delta}{4a} \right]$$

Formule Bouguera wzorany jest od redukcji "wysokosci i wizual" na poziom mora

etwiazek skutku drogi ziem:



$$g = g_{90} - \left( \frac{2\pi a \sin \varphi}{T} \right)^2 \frac{\sin^2 \varphi}{\cos^2 \varphi}$$

$$= g_{90} \left( 1 - \underbrace{\frac{4\pi^2 a}{T^2} \sin^2 \varphi}_{\frac{1}{290}} \right)$$

Do tego wracajc do wzoru:

zapisz udowodnij

$$g = g_{90} \left( 1 - \frac{1}{391} \sin^2 \varphi \right) \text{ zatem}$$

$$g = g_{90} \left( 1 - \frac{1}{191} \sin^2 \varphi \right)$$

Przez tyle redukcja na poziom mora i na  $45^\circ$  ser. pol. rezultuj w wyniku wzoru skup. skup.

Ma trojan 5, i q tunt. alle kaidys myga oblygi j; rūvica negr =  $\Delta$  51

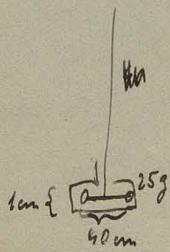
Nip framework  $\Delta=0$   $g = 981.264$

Warden	$g = 980.913$	$\Delta = +26$
Warren	$g = 981.224$	$-20$
Ondex	$g = 980.887$	$+64$
Trojai (Tyrol)	$g = 980.570$	$-167$
Zandek "	$g = 980.380$	$-154$
Salt Lake City	$g = 980.050$	$-262$
Dover Col.	$g = 979.983$	$-252$
Mosk (Ind- 46°6m)	$g = 979.169$	$-498$
Alma Ray	$g = 980.275$	$+56$
Cape	$g = 980.263$	$+169$
Shetland	$g = 980.229$	$+88$
St. Helena	$g = 978.786$	$+225$
Manitou	$g = 978.959$	$+229$
Honolulu	$g = 979.059$	$+257$

$$\begin{aligned}
 g_p &= g_g + g_{\text{rel}} - g_{\text{gal}} \\
 g_{\text{rel}} &= 980.116 \\
 g_g &= 979.057
 \end{aligned}$$

Clement  
 zem.  
 zem.  
 po obliku  
 $g_0$   
 + leg.-gal  
 $g_g$

Intade lotom.



nos užināt! ~~50 cm!~~  
 10-20 min!

Toki užtūzī ukrasātājī  $5 = \frac{1}{2}''$

platīt v ar obliku! 1 m od mosa  
 mosa ir pārikošo 1 mm

Turbinas Sensus do vento português:

$$-4\pi \cdot 4\pi \cdot \delta \cdot p_c = 4\pi$$
$$\delta = 1.9 \cdot 10^{33}$$
$$\delta = 6 \cdot 10^{-7} g$$

$$Mora \odot = 324.050$$
$$\delta = 17^{\circ} 6'' 2 \odot$$
$$\odot = 31^{\circ} 2 \delta$$
$$2.5 \frac{g \text{ col}}{\text{min}}$$
$$= 2.8 \cdot 10^{32} \frac{\text{kg}}{\text{sec}}$$

$$C_m = 0.0122 m^5$$
$$n = 0.27 m^3$$
$$g = 0.167 g^3$$
$$\rho = 0.62 \text{ ps}$$

484"

$$\frac{324.050}{108.6} = 27$$
$$\rho = 0.25 \text{ ps}$$

~~$$K_M$$~~
$$\frac{K_M}{a} = g^2$$
$$\sqrt{2ag} = \sqrt{2 \cdot 6 \cdot 10^7}$$
$$= 112 \cdot 10^4 = 112 \text{ km}$$

~~Lord~~ Poynting & Thomson Propulsion of matter  
planetary C

$$\frac{150 \cdot 10^6}{20 \cdot 10^3} = \frac{1500}{2} = 52$$

$$\frac{K m m}{r^2} = m r \omega^2 r$$

$$\frac{m \odot}{m_\oplus} = \left( \frac{27}{365} \right)^2 \left( \frac{150 \cdot 10^6}{6.760 \cdot 10^6} \right)^3 = 300,000$$

gastro ① 0.25

~~$g = g_0 \cdot 3626 \neq 60^2$~~

K rotation also gives other mass terms

1740 Tongue Pen Chambers 8" from side gastro in - 92°

1772 Narkulym Shishchikov 12"

26"

rate of turn  $\frac{1}{3}$  = per min  
 $\frac{1}{2} K_2$

$$\frac{14}{5} \cdot 2 \frac{1}{2} = 5$$

Ninth 9. 60 min max is per min

Reville

Cadet 1798

$$\frac{K M m}{r^2} l = m \theta$$

$$\tau = 2\pi \sqrt{\frac{K}{l}}$$

$$\left\{ \begin{array}{l} \frac{4\pi^2 K \theta}{\tau^2} = \frac{K M m l}{r^2} \\ g = \frac{4}{3} \pi \frac{R^3 \rho}{R^2} K = \frac{4}{3} \pi K R \rho \end{array} \right.$$

$$l_2 = 3 \text{ sec}$$

$$0^{\text{m}} \cdot 26 = 2 \text{ sec}$$

$$( ) \cdot 12 \text{ sec}$$

$$\rho = 6.45$$

$$\rho = \frac{1}{2}$$

Reville, Dark, Cormier Reville 5.5  
1870

Days from first maximum to perihelion 1895  $\theta = 3.51 - 5.77$  (calculated)

in An ~~22~~ 5 mm

$$l = 2.2 \text{ cm}$$



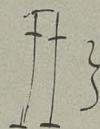
$$K = 6.6576 \cdot 10^{-8}$$

$$\rho = 5.5270$$

Dream 1896 *primitivo.*  
 $\rho = 5.52725$

Wilms 1886 5.579

Jolly 1878



21m

$\frac{32 \text{ m}}{5 \text{ kg}}$

5.69

Richer Kugler 1898

1.2m

$\frac{1.2453 \text{ m}}{1 \text{ kg}}$

5.505

Poettig

0.901

350.66

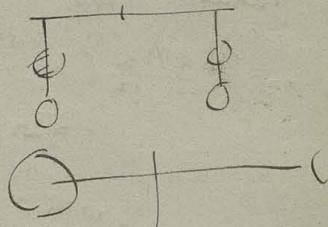
$5 = \frac{4}{10} \text{ kg}$

$\theta = 5.4934$

verso le grandi voci che parlano  
d'urto & frangere 1897 permesso

Poettig & Gray not d'urto 1899 ~~ma~~ rule 2 Fratture

Chinese work Landolt, Hydrostatic



$\frac{f}{1 \text{ cm}} \rightarrow f$

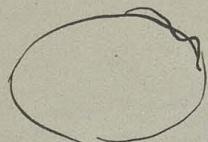
$$F = \frac{\rho g m}{15 \cdot 10^6}$$

$$\begin{array}{r} 10 \\ 2 \end{array} : \begin{array}{r} 15 \\ 3 \end{array} = 6$$

Pozzi 1903

53

zurück  
durch periodische Schwingungen wird die Zeit verkürzt



$$\bar{W}_1 = V_1 + v \leftarrow \text{tot. velocity}$$

$$\bar{W}_2 = V_2 + v$$

$$u = W_1 - W_2 = V_1 - V_2 \quad \rightarrow \text{periodisch} \approx 0$$

$$\Delta W = \text{konst} \quad \Delta u = 0 \quad \rightarrow \text{schwingende part.}$$

$$f = g + l + \frac{2l}{R}$$

Winkel



$$g = \frac{\omega^2 r}{l} \text{ a wavy line}$$

$$\frac{\partial \frac{\omega^2}{l} - g}{\delta \omega} = \frac{5}{2} \frac{\omega^2}{l} - g$$

Conducente libante Period. schwing.

Dot. undur libante rotante

Die Schwing. dagegen

$$\text{Festheit: } g = 978.046 [1 + 0.005302 \sin^2 \varphi] = 978.046 [1 + 0.005302 \cdot 1] = 978.046$$

$$1884 \quad g = 978.000 [1 + 0.005310 \sin^2 \varphi]$$

$$e = \frac{l}{298.25}$$

Herr der oceanische Hypothese

1803

Leibniz avon dem (Stimme) Komp.  $\partial g / \partial \varphi = 0.06$

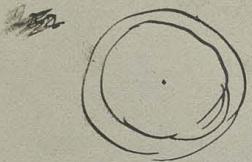
Pratt (Kompensation)

Sly antarctica  $\partial g / \partial \varphi = -0.12$

in oceanic Herr der

Leibniz dist.

Croesus schismoni



$$g_0 = g - \frac{4\pi G h}{R}$$

Wavelength  $\lambda = 276$

0	7.61 - 12.16	<i>Stellfis</i>  <i>Wavelength</i> $7.9 \times 10^{-6}$
0.1	: - 11.28	
0.2	{ 8.0 - 9.3	
0.3	{ - 10.63	
0.4	7.61 - 8.53	
0.5	7.87 - 8.33	
0.6	6.87 - 7.84	
0.7	6.00 - 7.05	
0.8	5.42 - 5.81	
0.9	4.05 - 4.58	
1.0	2.60 - 2	
		$\left\{ \begin{matrix} 1/5 \\ 1/5 \end{matrix} \right.$ $3 - 35$

$$U_e = \frac{E}{\sqrt{r^2 + \mu^2 - 2pr\cos\theta}} - \frac{E_a}{\mu\sqrt{r^2 + (\frac{e^2 p}{\mu} - 2pr)^2 \sin^2\theta}}$$



$$E = c\mu^2$$

$$= c\mu \left[ 1 + \left( \frac{r}{\mu} \right)^2 - 2 \frac{r}{\mu} \cos\theta \right]^{-\frac{1}{2}} - \left[ 1 + \left( \frac{r}{\mu} \right)^2 + 2 \frac{r}{\mu} \cos\theta \right]^{-\frac{1}{2}}$$

$$- c\alpha_p \left[ r^2 + \frac{e^2 p^2}{\mu^2} \right]^{-\frac{1}{2}} = [$$

$$= c\mu \left\{ 1 + \frac{r}{\mu} \cos\theta - \frac{1}{2} \left( \frac{r}{\mu} \right)^2 \quad - A + \frac{r}{\mu} \cos\theta - \dots \right\}$$

$$- c\alpha_p \left\{ 1 + \frac{e^2}{\mu^2} \cos^2\theta \dots \quad - A + \frac{e^2}{\mu^2} \cos^2\theta - \dots \right\}$$

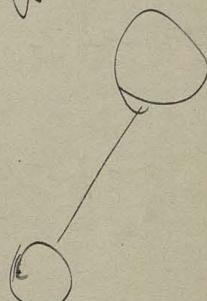
$$= 2 \left( c \cos\theta - c \frac{e^2}{\mu^2} \cos^2\theta \right)$$

$$U = c \left( x - \frac{e^2 x}{\mu^2} \right)$$

$$\frac{\mu^2}{\mu}$$

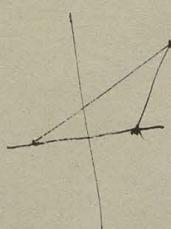
$$\frac{e^2}{\mu}$$

constant



continuity

$$S = - \frac{d \ln U}{dx} = - \cancel{c \cos\theta} \left( 1 + \frac{e^2}{\mu^2} \right)$$



$$U = \frac{1}{\sqrt{(x-a)^2 + y^2}} - \frac{1}{\sqrt{(x+a)^2 + y^2}} = c$$

$$\frac{1}{(x-a)^2 + y^2} = c^2 + \frac{1}{(x+a)^2 + y^2} + \frac{1}{c^2}$$

$$U_e = \frac{a}{2} V + \frac{E}{R} - \frac{a}{2} \frac{E}{\rho_f} \left[ 1 + \frac{a^2}{\rho_f} P_1 + \frac{a^4}{\rho_f^2} P_2 + \dots \right]$$

$$= \frac{a}{2} V + \frac{E}{R} - \frac{a E}{\rho_f} \left[ 1 + 2 \frac{a^2}{\rho_f} \cos \theta + \frac{a^4}{\rho_f^2} \right]^{-\frac{1}{2}}$$

$$= \frac{a}{2} V + \frac{E}{\sqrt{\rho_f^2 + 2 a^2 \rho_f \cos \theta + a^4}} - \frac{a E}{\sqrt{\rho_f^2 + 2 a^2 \rho_f \cos \theta + a^4}}$$

$$\frac{\partial U_e}{\partial r} = -\frac{a}{r^2} - \frac{E (r - \rho_f \cos \theta)}{\sqrt{(r - \rho_f \cos \theta)^2}} + a \frac{E (r \rho_f^2 - a^2 \rho_f \cos^2 \theta)}{\sqrt{(r - \rho_f \cos \theta)^2}}$$

$$= -\frac{V}{a} - E \frac{a - \rho_f \cos \theta + \frac{a^2}{a} + \rho_f \cos \theta}{(a - \rho_f \cos \theta)^2} = \cancel{-\frac{V}{a}} + \frac{E (a^2 - a^2)}{R^3}$$

$$= -\frac{1}{2} \left( V - \frac{E (1 - e^2)}{R^3} \right)$$

$$\int r \theta \, dr$$

$$E_1^2 (p_2^2 + s^2) = \sum_2^L (p_1^2 + s^2) \quad \sum_1^L p_2 = \sum_2^L p_1$$

$$\frac{p_1}{p_2} (p_2^2 + s^2) = p_1^2 + s^2$$

$$p_1 p_2^2 - p_1^2 p_2 = s^2 (p_2 - p_1)$$

$$p_1 p_2 = s^2$$

$$p_2 = \frac{s^2}{p_1}$$

$$\sum_1^L = \frac{\sum_1^L s^2}{p_1^2}$$

$$U = \frac{\sum_1}{\sqrt{p_1^2 + a^2 - 2 a p_1 \cos \theta}} - \underbrace{\frac{\sum_1 a}{p_1 \sqrt{\left(\frac{p_1}{a}\right)^2 + a^2 - 2 \frac{a^2}{p_1} \cos \theta}}}_{\cancel{\text{WAA}}} \quad \sum_2 = \frac{\sum_1 s}{p_1}$$

Tyber:

Potentiol: Travers Potentiol.

Clausius Rethaff & Pot.

Dotti Libet. d. Pot. Thermo. s. galv., Electrotach & Regn

Nernstoss pos & Th. o. Pot. s. o. Kugel.

Korn Libet. d. Pot. Th.

Korn A.H.

Zimmer Driesslet  $\xrightarrow{\text{pos}}$   
Gantt Otar. Pot. & C. 21.12.2. 1912 C. V. P. M.

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Dear Einheit, d. E. Regn s. H. dyne

Riemann Schwer. d. s. Regn

Moscat-Joubert

Morrell

Fippel

Cohn d. d. dyn. Fall

J. J. Thomson

S. Thompson (math.)

Euler ~~Electrostatic~~ Electrostat.

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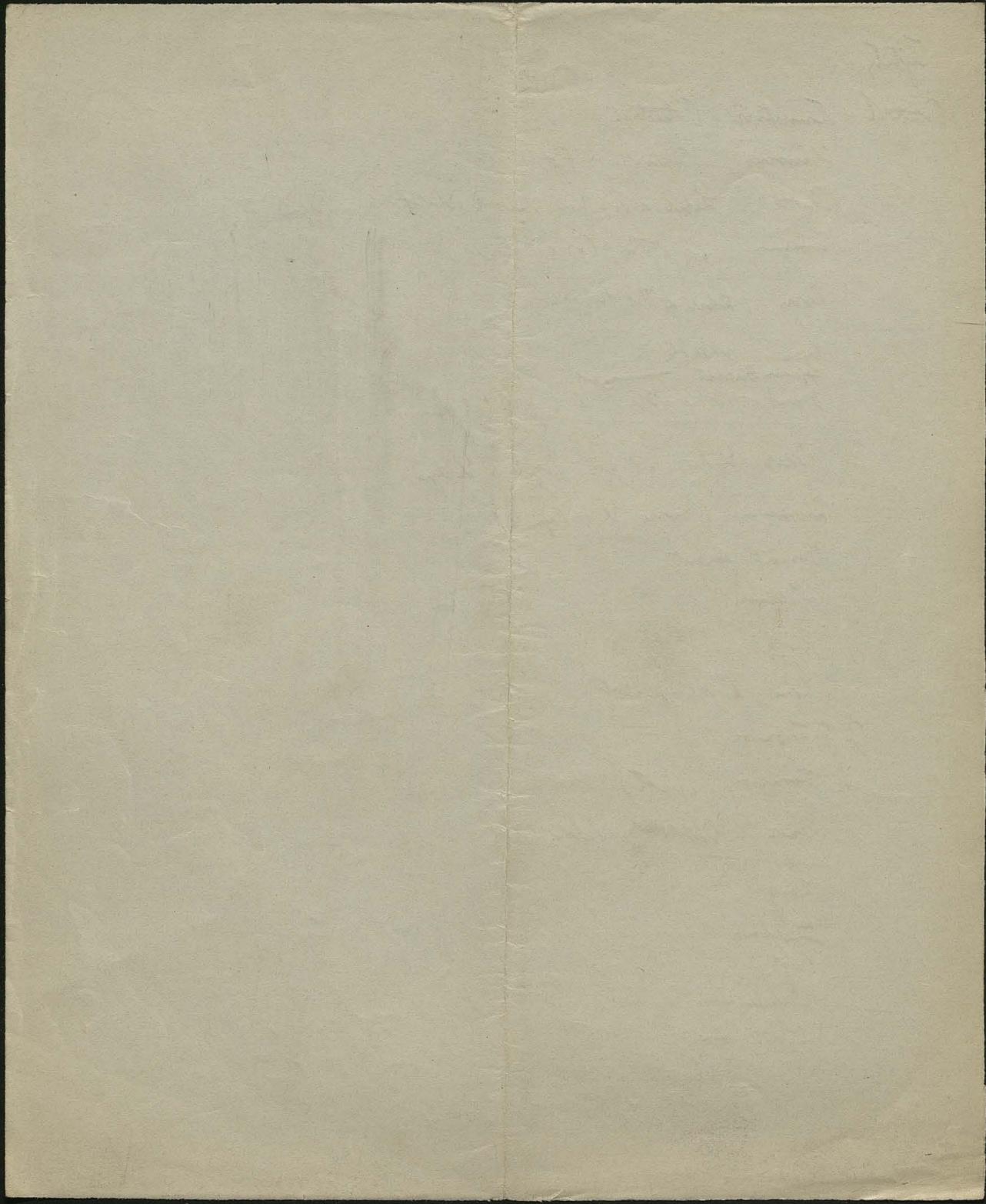
Lang

Auerbach

Vongt

Winkler

Christiansen



$$(1 + \gamma n k_1) \frac{\partial U_1}{\partial n_1} + \frac{\partial U_2}{\partial n_2} = -\gamma n k_1 \frac{\partial V}{\partial n_1}$$

P = H - V

$$(1 + \gamma n k_2) \frac{\partial U_1}{\partial n_1} + \frac{\partial U_2}{\partial n_2} \neq 0$$

$$-\gamma n k_1 \frac{\partial U_1}{\partial n_1} - \frac{\partial V_2}{\partial n_2} = -\gamma n k_2 \frac{\partial V_1}{\partial n_1}$$

$$= 0$$

$$\frac{\partial (U_1 - V_1)}{\partial n_1} + \frac{\partial (U_2 - V_2)}{\partial n_2} = -\gamma n k_1 \frac{\partial U_1}{\partial n_1} - \gamma n k_2 \frac{\partial U_2}{\partial n_2}$$

$$\mu_1 \frac{\partial U_1}{\partial n_1} + \mu_2 \frac{\partial U_2}{\partial n_2} = \frac{\partial V_1}{\partial n_1} + \frac{\partial V_2}{\partial n_2} = 0$$


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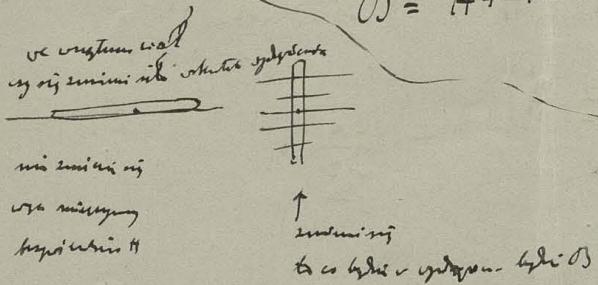
DV induks.

~~$\mathcal{B} = \mu H = (1 + \gamma n k) H$~~

~~$I = \kappa H$~~

$I = \kappa H$

$\mathcal{O} = H + \gamma n I$



je zollnung wgn.  
K periodisch = "

we untersuchen

$\mathcal{B} \propto H$

periodisch

$I \propto H$

wirken  $\mathcal{B}$  auf  $I$  und  $H$  periodisch

$\mathcal{O}$  } weicht ab periodisch

Karta. Która relatywnie jest tanie i taka powoduje, iż na Tabela wynosi  
Twój negatyw wydaje się w kierunku nieskończoności

$$K \quad \begin{array}{l} \rho_i \\ \rho_6 \\ H_2O \end{array} \quad \begin{array}{l} -14 \cdot 10^{-6} \\ -5 \cdot 10^{-6} \\ -0.8 \cdot 10^{-6} \end{array}$$

$$H_f \quad -2.6 \cdot 10^{-6}$$

$$\rho_2 \quad +0.12 \cdot 10^{-6}$$

$$H_2 \quad -0.034 \cdot 10^{-6}$$

$$U_c = cx \left[ 1 - \frac{\mu-1}{\mu+2} \frac{a^3}{r^3} \right] \quad -cx \left[ - \right]$$

~~$$U_i = cx \frac{3}{\mu+2}$$~~ 
$$-cx \frac{3}{\mu+2}$$

$$U_c = cx \left[ 1 - \frac{\mu-1}{\mu+2} \left( \frac{a^1}{r^3} - \frac{a_{\infty}}{r^3} \right) \right] \quad + \left[ 1 - \frac{\mu-1}{\mu+2} \frac{a^3}{r^3} \right]$$

$$U_i = cx \left[ \frac{3}{\mu+2} + \frac{\mu-1}{\mu+2} \frac{a^1}{r^3} \right]$$

$$U_i = cx \frac{3}{\mu+2} -$$

wyjątkiem

$$\frac{q}{\mu}$$

$$q_{\mu+2}(\mu-1)^2(1-\beta)$$

$$\mu = 300$$

$$\beta = \frac{R_1}{R_2}$$

$$\frac{q}{2f_m} \frac{3}{10}$$

$$\frac{31}{20} = 1.55$$

dwukrotnie  $\frac{3\mu}{\mu+2} > 1$   
indeksji

223

potentiell wirkende Kräfte innerer Elemente  
innerhalb eines

$$U = \frac{\alpha}{r^3} \leq M$$

56

wie physikalisch es  $\leq M$

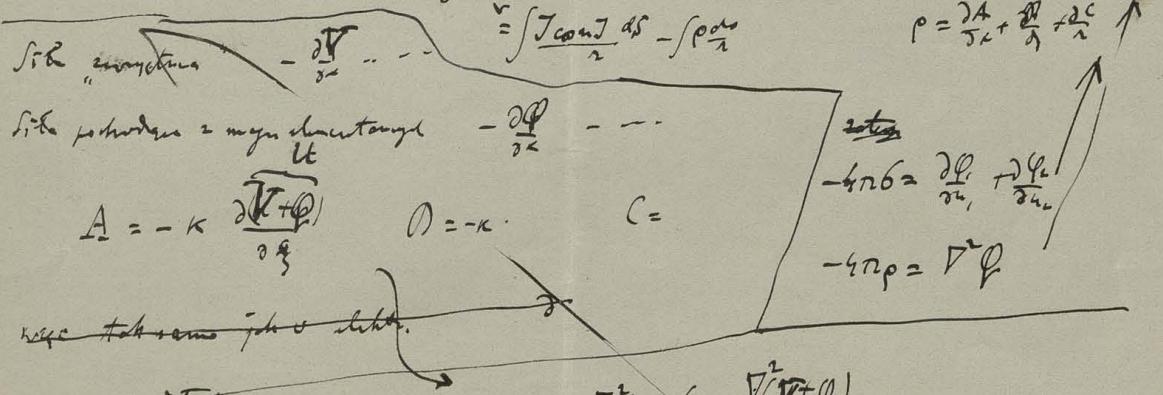
zweitergliedriges Modell der Elemente

der Kettenelemente

$$U = \sum_{i=1}^n m_i \frac{1}{r_i^3} \quad r_i = r_{i+1} - r_i$$

~~Modell~~  
~~Modell~~

$$\begin{aligned} \Phi &= \int \frac{1}{r^2} \left( c_{11} \epsilon_{11} + c_{12} \epsilon_{22} + c_{13} \epsilon_{33} \right) dV \\ &= \int \frac{A (\sigma_{xx} \partial_{x_1} \eta + \sigma_{yy} \partial_{x_2} \eta + \sigma_{zz} \partial_{x_3} \eta)}{r^2} dV = \int \left[ A \frac{\partial(\eta)}{\partial x_1} + \sigma_{yy} \frac{\partial \eta}{\partial x_2} + C \frac{\partial \eta}{\partial x_3} \right] dV \\ &= \int \left( \frac{A \sigma_{yy} + C_n}{r^2} \right) dV - \iiint \frac{\partial \sigma_{yy}}{\partial x_1} \left[ \frac{\partial A}{\partial x_1} + \frac{\partial \sigma_{yy}}{\partial x_2} + \frac{\partial C}{\partial x_3} \right] \\ &= \int \frac{G}{r^2} dV - \int \rho \frac{du}{r} \quad G = A \sigma_{yy} + C_n - \text{Jahns} \\ &= \int J_{\text{const}} \frac{dV}{r^2} - \int \rho \frac{du}{r} \quad \rho = \frac{\sigma_{yy}}{G} + \frac{C}{A} + \frac{C}{r} \end{aligned}$$



~~$J = -k \frac{\partial \eta}{\partial x_1} = +k R$~~

~~$J = k \frac{\partial \eta}{\partial x_2} = -k R$~~

~~$\frac{\partial \eta}{\partial x_1} + \frac{\partial \eta}{\partial x_2} = 0$~~

$$\frac{\partial \eta}{\partial x_1} + \frac{\partial \eta}{\partial x_2} = -G \frac{\partial \eta}{\partial x_1} + G \frac{\partial \eta}{\partial x_2} = G \frac{\partial \eta}{\partial x_1} - G \frac{\partial \eta}{\partial x_2}$$

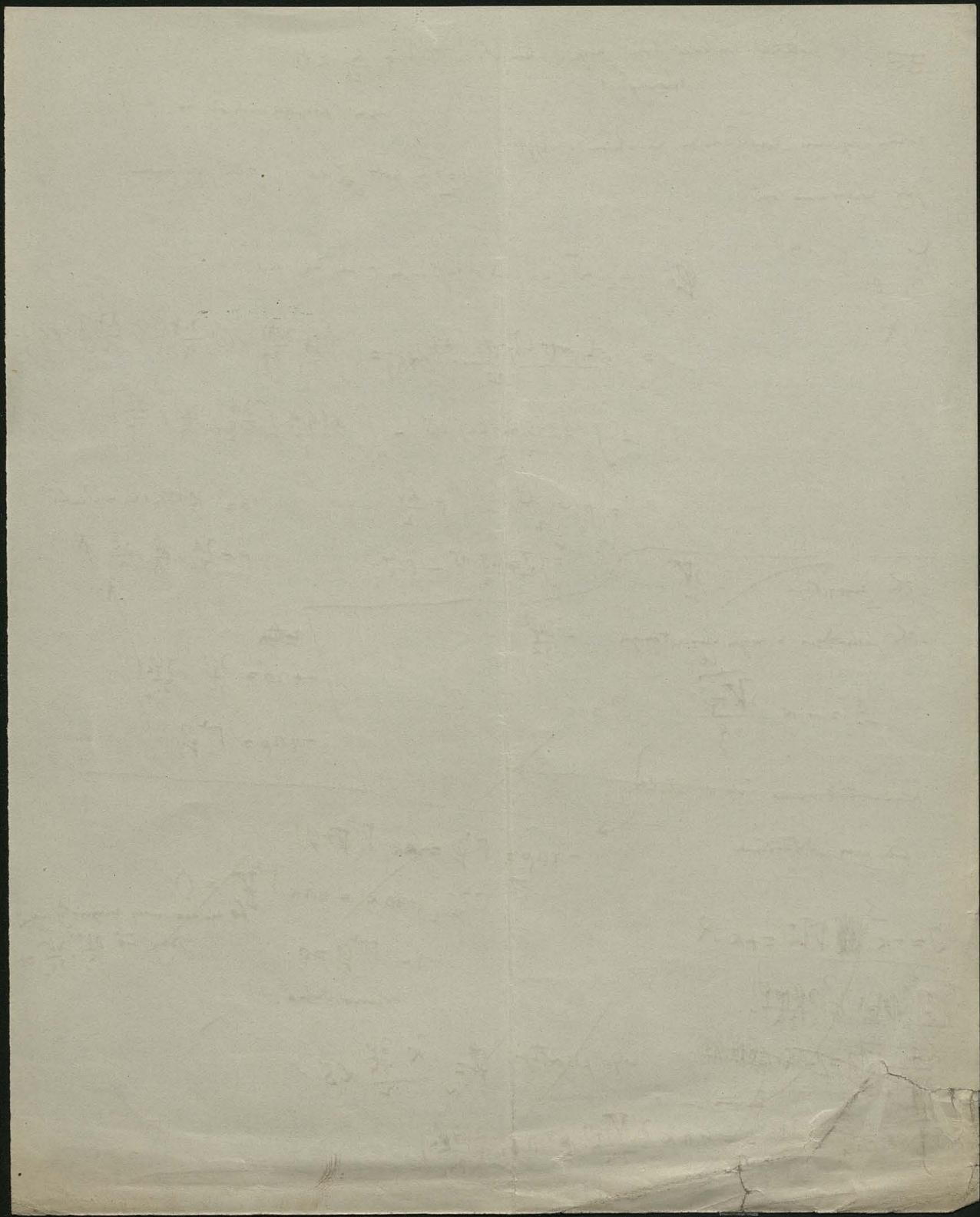
~~$\eta = \int \frac{k}{r^2} \frac{\partial \eta}{\partial x_i} dV$~~

~~$\omega_{xz} = \nabla^2 \eta = 0$~~

rechtsdrehend

keine auswärts gerichtete Kraft

die die  $\frac{\partial V}{\partial x_1}, \frac{\partial V}{\partial x_2} = 0$



Optim  $\varphi = \int \underbrace{\left( T \sin \theta \right) ds}_{\frac{6}{2}} - \int \rho \frac{av}{2}$

Colle minimum  $\nabla V$  to line we make strength and time, is dangerous to us  
 no time necessary, very good

$G = [A + \rho_m + c_1]$   
 $\rho = \frac{\rho_1}{\eta} + \frac{\rho_2}{\eta}$   
 just because something  
 has to work

---

~~$-4\pi\rho = \frac{\partial \varphi}{\partial t} + \frac{\partial \varphi}{\partial r}$~~   
 $-4\pi\rho = \nabla^2 \varphi$

2nd eqn.  $A = -\kappa \frac{\partial (V + \varphi)}{\partial x} = -\kappa \frac{\partial U}{\partial x}$   $\nabla U = \mathcal{L}$  !

$$\begin{aligned} D &= -\kappa \frac{\partial U}{\eta} \\ C &= \end{aligned}$$

$G = \kappa + \kappa \left( \frac{\partial U}{\eta} x + \frac{\partial U}{\eta} z + \frac{\partial U}{\eta} u \right) = +\kappa \frac{\partial U}{\partial x} + \kappa \frac{\partial U}{\partial z}$  arbitrary constant

$\rho = -\kappa \nabla U$

---

we have boundary:

$$-4\pi\rho = -4\pi\kappa_1 \frac{\partial U_1}{\eta_1} - 4\pi\kappa_2 \frac{\partial U_2}{\eta_2} = \frac{\partial (U_1 - V)}{\partial \eta_1} + \frac{\partial (U_2 - V)}{\partial \eta_2}$$

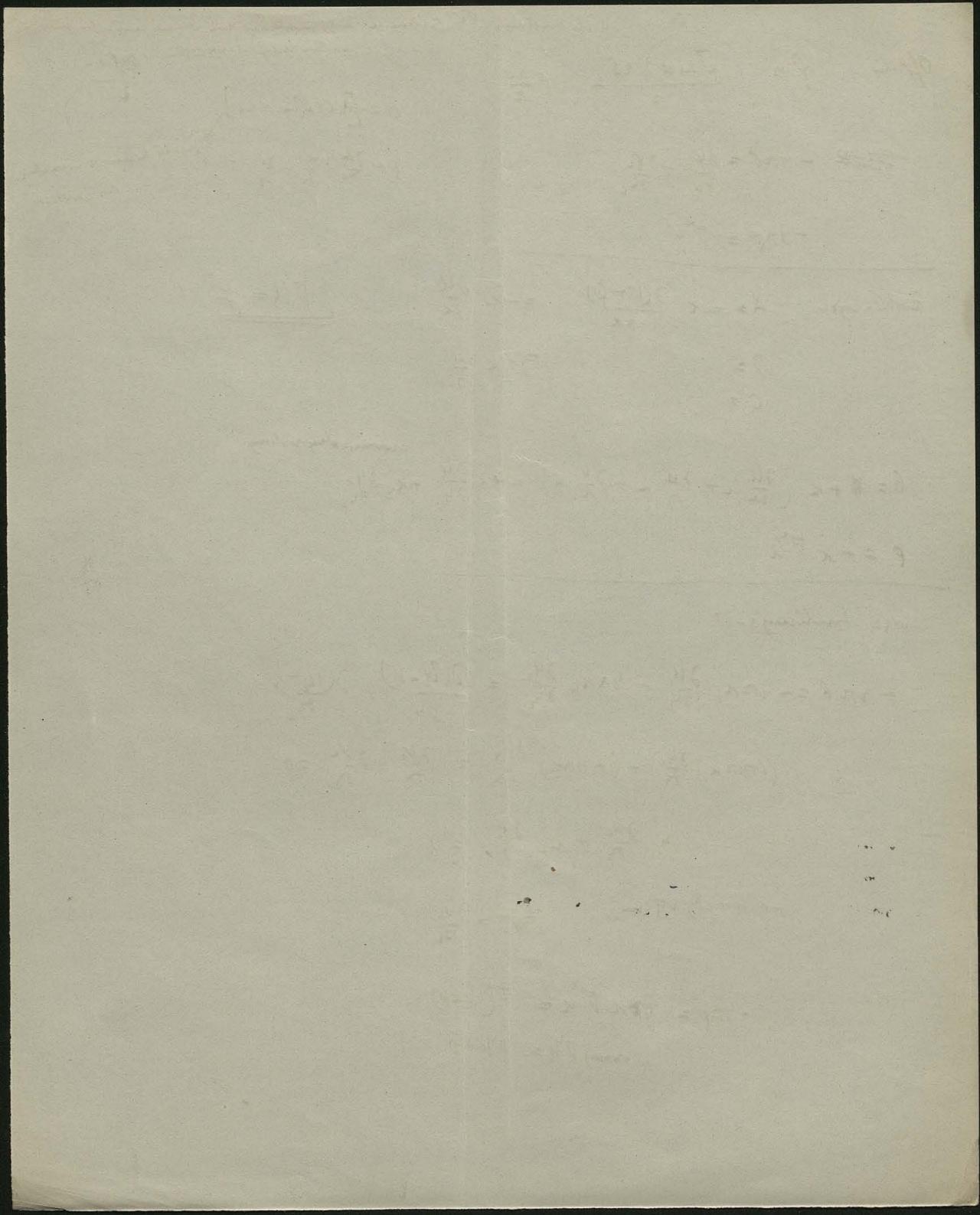
$$(4\pi\kappa_1) \frac{\partial U_1}{\eta_1} + ((1 + 4\pi\kappa_2) \frac{\partial U_2}{\eta_2}) = \frac{\partial V_1}{\eta_1} + \frac{\partial V_2}{\eta_2} = 0$$

$$\mu_1 \frac{\partial U_1}{\eta_1} + \mu_2 \frac{\partial U_2}{\eta_2} = 0$$

produces system  $\frac{\partial U_1}{\eta_1} = \frac{\partial U_2}{\eta_2}$

$$-4\pi\rho = 4\pi\kappa \nabla^2 U = \nabla^2 (U - V)$$

$$(1 + 4\pi\kappa) \nabla^2 U = \nabla^2 V = 0$$



wyks u bardszych

$$Bi \quad K = -15 \cdot 10^{-5}$$

$$Hg \quad -2 \cdot 6 \cdot 10^{-6}$$

$$H_2O \quad -0.8 \cdot 10^{-6}$$

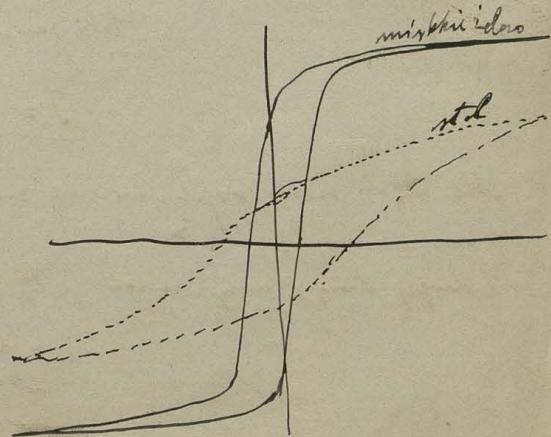
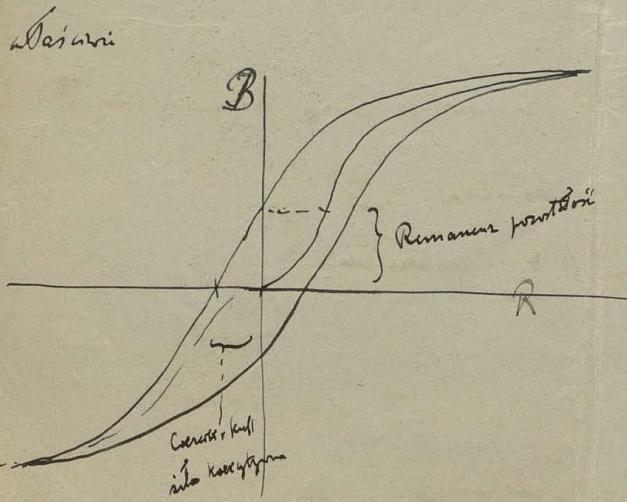
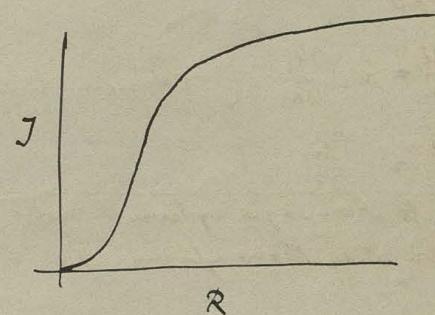
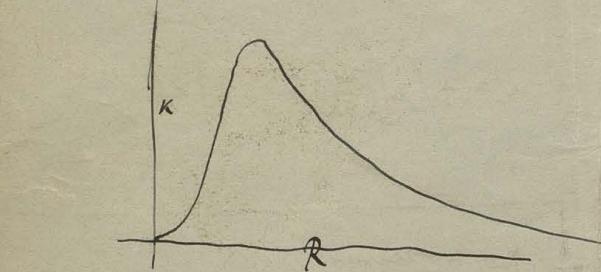
$$CO_2 \quad -0.8 \cdot 10^{-6}$$

$$FeSO_4 \quad +6 \cdot 10^{-6}$$

$$O_2 \quad +0.157 \cdot 10^{-6}$$

$$H_2 \quad +0.0003 \cdot 10^{-6}$$

Fe	$\frac{R}{K}$	mixtura							
		K	0	9	43	179	266	122	58
R	0	0.32			2.14	3.24	4.50	8.79	21.7



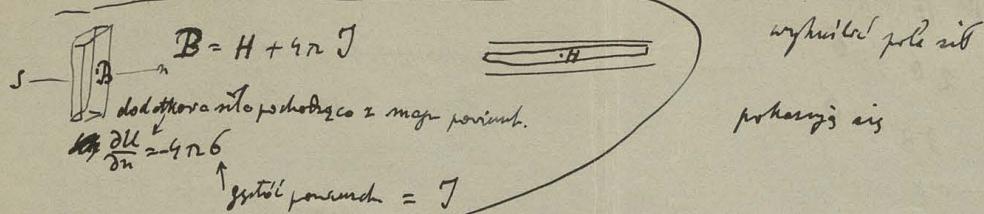
$$Ni = \frac{1}{3} - \frac{1}{2} Fe$$

Co unmix Ni i Fe

mixtura potencjałowa gęstość drąz - 1

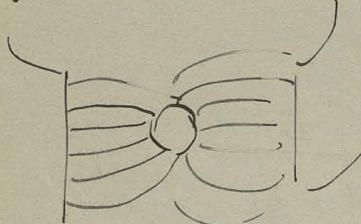
Wysoka gęstość

Ponieważ siły Newton - równe  $\Delta^2 U = 0$  w przestrzeni symetrycznej (przy mniej nienaturalnych warunkach)



pochodzi z nich

Zasada indukcji magnetycznej n.p.



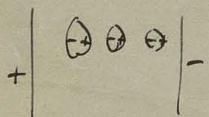
więcej hypothetycznych analogii z fizyką atomową  
zgodnie z obliczeniami sprawa dechnie  
analogicznego typu:

$\Delta^2 U = 0$

$$\mu \frac{\partial U}{\partial n} = \mu_0 \frac{\partial U_0}{\partial n} \quad \left. \begin{array}{l} \text{z danymi linijkami} \\ \frac{\partial U_0}{\partial n} = \frac{\partial U_0}{\partial s} \end{array} \right\} \quad W = \frac{1}{2} \int \mu \left[ \left( \frac{\partial U}{\partial n} \right)^2 + \dots \right] ds$$

to właściwie jasne wystarczy dać mimo

Tak zrobili studiów bionaukowych K : Faraday - Maxwell - Elensus



tak samo tutaj: je porządkuje prawo magnesowania  $J$

$$J = K H \quad \text{hipoteza}$$

Ale o jaki sposób wojciech mówiąc mówią H kiedy wewnętrzne siły?

z drugiej strony z naszych równań  $\mu \frac{\partial U}{\partial n} = \mu_0 \frac{\partial U_0}{\partial n}$ :

$$\mu H = B = H + 4\pi J = H (1 + 4\pi K)$$

$$\mu = 1 + 4\pi K \quad \text{podstawniemy...}$$

(prawdziwe magnetyzm) z dalszymi wyjaśnieniami

*Ostotoma graminea* 2

H	B	J	K	n
3630	24700	1680	0.46	6.80
9500	10200	1650	0.17	3.18
11180	31560	1620	0.15	2.82

die folgt ist (Drei)

H	J	K
0.0158	0.263	16.5
0.0308	0.547	17.6
0.0700	1.673	23.0

Early & Low

24500	$\frac{45350}{24500}$	1660	0.07	1.85	$\frac{1.80}{12.566}$	$\frac{166}{1.986}$
	$\frac{20850.4}{52105}$	1660 Stimme			$\frac{1.80}{12.566}$	$\frac{166}{1.986}$

wie  $I_{max} + 1700$

Ende mit jenem fiktiven durchs D/H, ob man nun mögliche  $dh = \frac{1}{\pi n} \int H dB dv$

$$W = \frac{1}{8\pi} \int n \frac{dB}{dr} dr = \frac{1}{8\pi} \int B \frac{dH}{dr} dr$$

jedes fiktive:

$$= \frac{B}{8\pi} \frac{dH}{dr}$$

ist phys. prozess hängt von  $r$  ab

= "der engl. response"

$$\text{Stimme } W_{sys} = 0.002 \cdot R^{1.6}$$

wie tanzt am vorn meiste

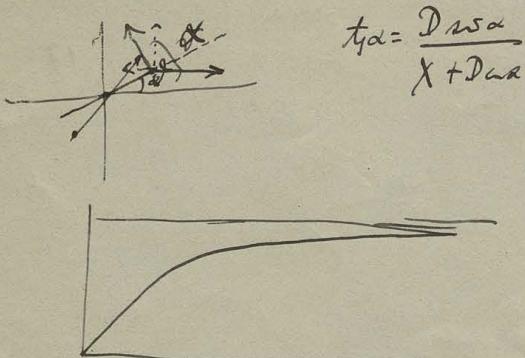
Cy mde. odgeschworei unter neueren 2

- 1). rechte rechte  $\uparrow$
- 2). ~~rechte~~ ganz vorne  $800^{\circ}$

Prozesse meiste (Bsp. Klarinette)

Mitler Prismen wend.

Weber Skewness durch



$$t_{\alpha} = \frac{D_{25\alpha}}{X + D_{25\alpha}}$$

Reckl in Form von der Form folgt Typus der Wirkungszyklen  $\leq \rho$ .

Die Zyklen in Form von Form

Ewing weijne isty Languis

Arb da manuatu.  $W = -\frac{1}{m} \int K H^2 dv$

Seite u pol dicht. i verange.

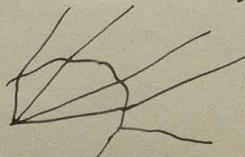
$$T = \frac{1}{\rho n} \int K \left(\frac{\partial h}{\partial v}\right)^2 dv = \frac{1}{\rho n} \int D E dv$$
$$= \frac{1}{\rho n} \int \mu \frac{\partial h}{\partial v} dv = \frac{1}{\rho n} \int B H dv$$

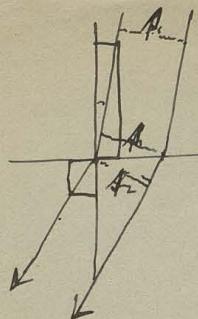
der Linie folgen dicht  
zyklen z. max recuperat. mit  
stet. be. regeln. stet. form

$$\delta = -\frac{1}{4n} K \frac{\partial h}{\partial v} = \frac{D}{\rho n}$$

zu dicht wagen ihm zu nahmen  $D_{1,2,3}$

der min. notiz. u. kürz. normale des formen  
to 25 min. zu





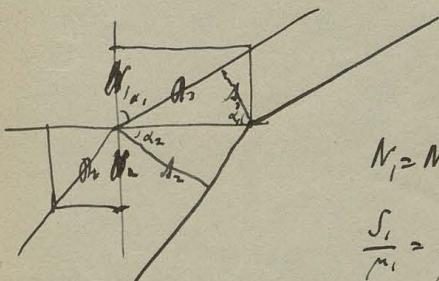
$$\frac{H}{F_1} : \frac{H}{F_2} = \frac{1}{\mu \alpha_1} : \frac{1}{\mu \alpha_2}$$

$$S_1 : S_2 = \mu \alpha_1 : \mu \alpha_2$$

$$\frac{H}{F_1} : \frac{H}{F_2} = \frac{1}{\mu \alpha_1} : \frac{1}{\mu \alpha_2}$$

$$\frac{B_1}{B_2} = \frac{\mu \alpha_1}{\mu \alpha_2}$$

$$\begin{aligned} \frac{B_1}{B_2} &= \frac{\mu_1}{\mu_2} \frac{\mu_2}{\mu_1} = \frac{\mu_1}{\mu_2} \frac{\mu_2}{\mu_1} \\ &= \frac{\mu \alpha_2}{\mu \alpha_1} = \frac{\alpha_2}{\alpha_1} \end{aligned}$$



$$N_1 = N_2$$

$$\frac{S_1}{\mu_1} = \frac{S_2}{\mu_2}$$

$$B_1 = \frac{N_1}{\mu \alpha_1}$$

$$\frac{\alpha_1}{\alpha_2} = \frac{\mu \alpha_2}{\mu \alpha_1} = \frac{\mu_2}{\mu_1}$$

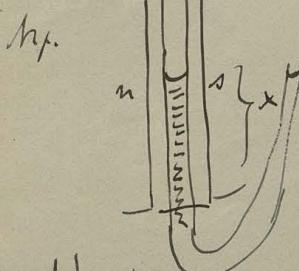
$$\frac{1}{8n} \left[ B_1^2 (V - v) + B_2^2 \frac{v}{\mu} \right]$$

$$\alpha_1 s_1 = \alpha_2 s_2$$

nie zatrzymać w tym momencie ponieważ grotów mniej

jeżeli tak jest to w tym momencie to  $\approx B$  to ilość lii nie zmienia

$\frac{1}{8n} \int \frac{B^2}{\mu} dv$  znam pierścienek <sup>zunadaj</sup> przy którym jest minimum energii potencjalnej  
jednorodne pole noga



$$\frac{B^2}{\mu} dv$$

$$\frac{1}{8n} B^2 \left[ q \frac{\delta x}{\mu} + q \frac{(h-x)}{1} \right] + W_0 = W$$

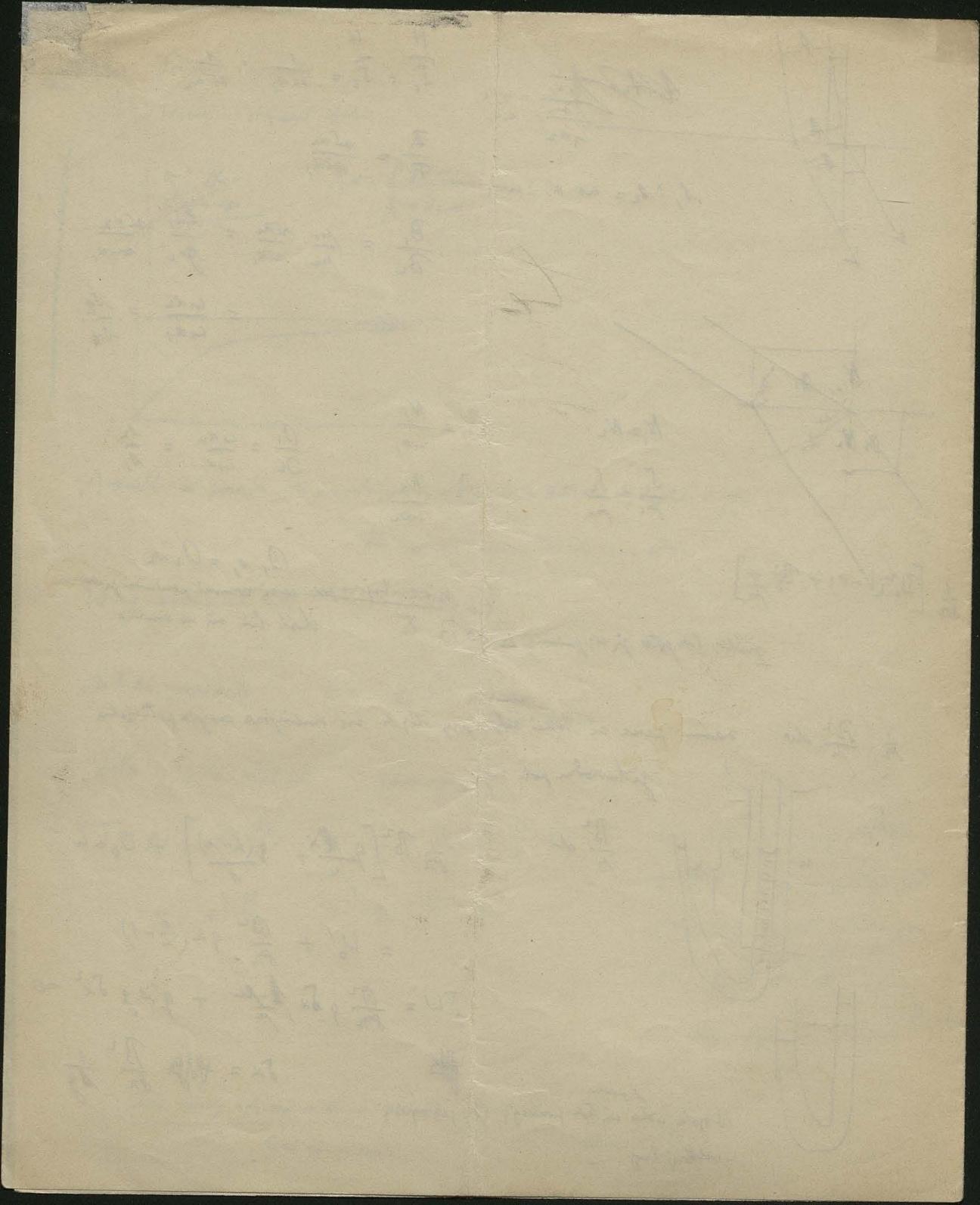
$$= W_0' + \frac{\partial^2}{\partial n} q x \left( \frac{1}{\mu} - 1 \right)$$

$$\delta W = \frac{\partial^2}{\partial n} q \delta x \frac{1-\mu}{\mu} + q s g \delta x^2 = 0$$



$$\delta x = \pm \sqrt{\frac{\mu - 1}{\mu}} \frac{B^2}{8n} \frac{1}{sg}$$

wysokość noga jest praważnie zbyt jednorodny  
wysoką linię ~



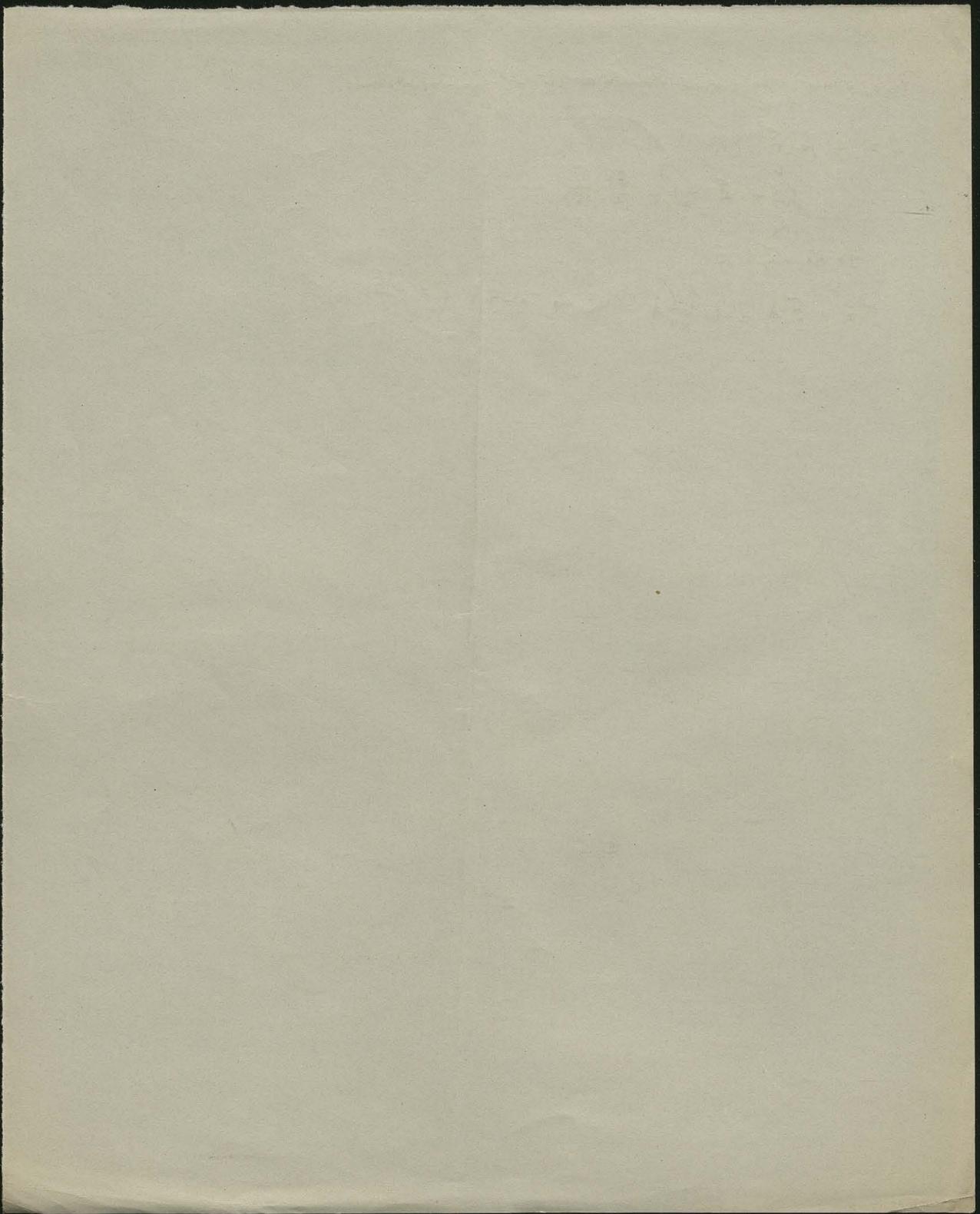
Piave Ohm as always requires a prior approximation:

$$J = g \cdot f_0(E)$$

$$f_0 + \frac{d}{dx}(f_0)_{\circ} + \frac{d^2}{dx^2}(f_0)_{\circ} + \dots$$

$\approx$   
as the initial  $E$

$$J = g \tilde{I} A = -g \frac{\partial U}{\partial n} A \quad \text{on the other } J = g \frac{A E}{L} = \frac{E}{\omega}$$



~~U<sub>1</sub> = R<sub>1</sub> + R<sub>2</sub> + R<sub>3</sub>~~



$$R_1 = \frac{4}{3} \pi J_x$$

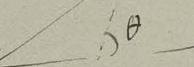
$$R_2 = \frac{4}{3} \pi J \frac{a^3}{r^3}$$

$$R_3 = + \frac{3}{n+2} cx$$

$$R_a = \left(1 - \frac{n-1}{n+2} \frac{a^3}{r^3}\right) cx$$

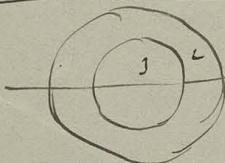


$$S = \left(1 + 2 \frac{n-1}{n+2} \frac{a^3}{r^3}\right) c \cos \theta$$



$$T = \left(1 - \frac{n-1}{n+2} \frac{a^3}{r^3}\right) c \sin \theta$$

$$A\theta = \frac{1 - \frac{n-1}{n+2} \frac{a^3}{r^3}}{1 + 2 \frac{n-1}{n+2} \frac{a^3}{r^3}} t\gamma$$



$$U_1 = cx \left[ 1 + \frac{a^3}{r^3} + \beta \frac{b^3}{r^3} \right]$$

~~$$U_2 = cx \left[ 1 + \alpha \frac{a^3}{r^3} + \beta \frac{b^3}{r^3} \right] -$$~~

$$U_1 = cx \left[ 1 + \alpha \frac{a^3}{r^3} + \beta \frac{b^3}{r^3} \right] \quad \left[ 1 - 2\alpha - 2\beta \frac{b^3}{a^3} \right] = n \left[ 1 + \alpha - 2\beta \frac{b^3}{a^3} \right]$$

$$U_2 = cx \left[ 1 + \alpha \frac{a^3}{r^3} + \beta \frac{b^3}{r^3} \right] \quad n \left[ 1 + \alpha - 2\beta \right] = \left[ 1 + \alpha + \beta \right]$$

$$U_3 = cx \left[ 1 + \alpha + \beta \right]$$

$$1 - \mu = \alpha (2 + n) + \beta \frac{2b^3}{a^3} (1 - \mu) \quad \left| \begin{array}{l} 1 + \mu \\ 1 - \mu \end{array} \right. \quad \frac{b^3}{a^3} = \varepsilon$$

$$1 - \mu = \alpha (\mu - 1) - \beta (1 + 2\mu) \quad (1 - \mu) 2\varepsilon$$

$$(1 - \mu)(1 + \mu) = \alpha \left[ (2 + \mu)(1 + \mu) + (\mu - 1)(1 - \mu) \right]$$

$$(1 - \mu) \left[ (1 + \mu) + 2\varepsilon (1 - \mu) \right] = \alpha \left[ (1 + \mu)(2 + \mu) - 2\varepsilon \mu(\mu - 1) \right]$$

$\frac{2 + 8\mu + 7\varepsilon^2}{-2 + 4\mu - 5\varepsilon^2}$

$$\alpha = \frac{3\mu - 1}{2\varepsilon^2} + \dots$$

winding pole

$$\frac{q_n}{q_n + 2(n-1)^2(1-\varepsilon)} c$$



$$\int \Sigma_m^i x_i d\sigma = \underbrace{\int x_m d\sigma}_{\int \Sigma_m} \\ M_p f \gamma d\sigma = M_p (1 - c \rho)$$

~~Σ m<sub>i</sub> x<sub>i</sub> dσ = Σ m~~

$$\Sigma m_i x_i d\sigma = \eta \Sigma m$$



$$-2\pi R^2 \rho \frac{d\varphi}{dx^2}$$

$$F = 2\pi R^2 \rho (\frac{L}{x} - \frac{1}{x}) = \frac{1}{x} \omega \varphi =$$

63

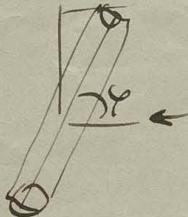
$$\frac{d\varphi}{dx} = \frac{2\pi R^2 \rho}{x^2}$$

$$\Omega_x = \frac{\partial \mathcal{H}}{\partial x}$$

$$\begin{aligned}\Omega_x &= -\pi \rho (R^2 + 2a \frac{dy}{dx}) + \pi \rho l^2 - \pi \rho (R^2 + 2y \frac{dx}{dy}) - \pi \rho l^2 \\ &= \pi \rho (l^2 - a^2) = 2\pi \rho [l^2 - (l - \delta_{xy})] = 2\pi \sqrt{a}\end{aligned}$$

$$\pi \frac{\partial \mathcal{H}_i}{\partial x} = \frac{\partial \mathcal{H}_0}{\partial x}$$

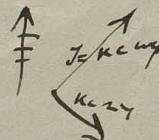
$$J = \frac{1}{2\pi} \frac{a-1}{a+1} c = \frac{\kappa}{1+2\pi\kappa} c$$



$$A = \frac{1+2\pi\kappa a^2 \rho}{1+2\pi\kappa} \kappa c$$

$$\Omega = \frac{\pi \kappa a^2 \varphi}{1+2\pi\kappa} c$$

$$J = \kappa c$$



$$W = -\frac{\kappa}{2} \int R^2 dx \quad X = \frac{\kappa}{2} \int \frac{\partial R^2}{\partial x} dx$$

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$$(\xi - x) \omega \lambda + (\eta - y) \omega \mu + \dots = 0$$

$$\xi \omega \lambda + \eta \omega \mu + \underbrace{(\alpha \mu - (\xi \omega \lambda + \eta \omega \mu + 2\omega))}_{=0}$$

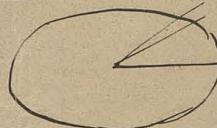
$$\frac{2(x^2/a^2 + y^2/b^2 + z^2/c^2)}{\sqrt{x^2/a^2 + y^2/b^2 + z^2/c^2}} = \frac{1}{\sqrt{x^2/a^2 + y^2/b^2 + z^2/c^2}}$$

$$\cos \theta = \mu \frac{\left[ 1 - \left( \frac{x x'}{a^2} + \frac{y y'}{b^2} + \frac{z z'}{c^2} \right) \right]}{\sqrt{(x - x')^2 + (y - y')^2 + (z - z')^2}}$$

$$\cos \theta' = \mu' \frac{\left[ 1 - \frac{x x'}{a^2} - \frac{y y'}{b^2} \right]}{\sqrt{\dots}}$$

$$G : G' = \cos \theta : \cos \theta' = \mu : \mu'$$

Ajuda: digram da orbita



$$\int \frac{G ds}{r} \text{ dla } \text{innych} =$$

$$\int \cancel{G ds} \frac{E_p ds}{4\pi abc r} = \frac{3E}{4\pi abc} \int \frac{dr}{r^2} = \frac{3E}{4\pi abc} \int \frac{r dr}{r^3} = \frac{E}{4\pi abc} \int r dr$$

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1 \quad r = a \sin \theta$$

$$y/r = b \cos \theta$$

$$\frac{\sin^2 \theta}{a^2} + \frac{\cos^2 \theta}{b^2} = \frac{1}{r^2}$$

$$U = \frac{E}{4\pi abc} \int_0^{\frac{\pi}{2}} \frac{2r \sin \theta dr}{\frac{\sin^2 \theta}{a^2} + \frac{\cos^2 \theta}{b^2}}$$

$$\int \frac{r^{-1} dr}{\frac{1}{a^2} + \left( \frac{b^2}{a^2} - \frac{1}{b^2} \right) \cos^2 \theta} = \int \frac{dr}{\frac{1}{b^2} + \left( \frac{b^2}{a^2} - \frac{1}{b^2} \right) u^2} = U_B \int \frac{du}{1 + \left( \frac{b^2}{a^2} - 1 \right) u^2} = \frac{b^2}{\sqrt{a^2 - b^2}} \arctg \left( u \sqrt{\frac{b^2}{a^2} - 1} \right) =$$

~~$$U = \frac{E}{\sqrt{b^2 - a^2}} \arctg \left( \sqrt{\frac{b^2}{a^2} - 1} \right)$$~~

$$6 ds = 6' ds'$$

Tużo jaki stosunek  $ds : ds'$ ?

z równaniem kuli:  $\frac{x^2 + y^2 + z^2}{r^2} = 1$

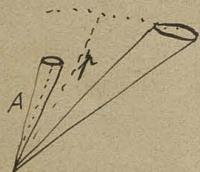
dyskrety:  $\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1$

które stoją w równaniu

Kiedy skróci się dziesiątka powierzchni i stromek

$$\frac{abc}{A^3}$$

zatem w wyniku tego jaka jest dla dostatek powierzchni w tym stromku, mówiąc w j. Tekstowej skróty stromek  $ds$

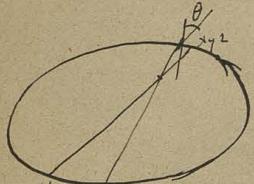


$$\frac{A ds}{3} : \frac{ds'}{3} = A^3 : abc$$

$$\frac{ds'}{ds} = \frac{abc}{A^2 r}$$

$$6' = 6 \frac{ds}{ds'} = 6 \frac{A^2 r}{abc} = \frac{E p}{4\pi abc}$$

Inna metoda: (zgodnie)



$$\frac{6 ds}{r^2} = \frac{6 dw}{cos \alpha}$$

$$\frac{6' dw}{cos \beta}$$

w tym samym czasie:  $6 \text{ prop } cos \beta$

$$\cos \lambda = \frac{\partial f}{\partial x}$$

$$= \sqrt{\left(\frac{\partial f}{\partial x}\right)^2 + \dots}$$

$$\cos \alpha = \frac{x - \star}{\sqrt{(x - \star)^2 + \dots}}$$

$$\star = \sqrt{\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} - 1}$$

$$\cos \theta = \frac{\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2}}{\sqrt{\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2}}} - \left( \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} \right)$$



entwad. dts. la styrax

Ostryg' slzy. *xylosteum* : *jugumoni*

Site mechan. ne konstrukcji taki (brak wydłuż. na lekkozawarcie)

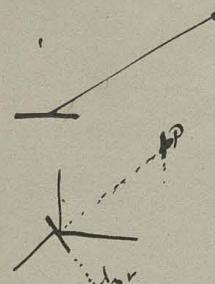
wysokie konstrukcje kubiczne

$$U = \cancel{M} \frac{M \omega}{r^3} = M \frac{m \theta}{r^2}$$

junk we can neglect when

$$U = M(\text{constant} + \frac{1}{r} \text{constant})$$

$$= \cancel{M} \frac{A x + \partial_y + C_z}{r^3} = A \frac{\partial \varphi}{\partial x} + \partial \frac{\partial \varphi}{\partial y} + C \frac{\partial \varphi}{\partial z}$$



$$\nabla \left( r \frac{dx}{dt} \right) = \frac{d}{dt} \left( \nabla r \frac{dx}{dt} \right)$$

$$\sum_m \left[ r \frac{dx}{dt} \right] = \text{const}$$

$$m = \sum_i \cancel{v}_i \quad \sum_i \cancel{v}_i \cancel{a}_i = 0$$

$$\sum_i \cancel{a}_i \cancel{v}_i = 0$$

$$\cancel{\frac{db}{dt}} \cancel{\sum_i v_i} = 0$$

$$\int db \sum_i v_i = \int b_0 [bc] \sum_i v_i = 0$$

$$\sum_i v_i \perp [bc]$$

$$b \leq w$$

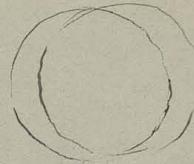
$$b = B \propto$$

$$\frac{db}{dt} =$$

$$U_e = ce \left(1 - \frac{a^3}{r^3}\right) = c \cdot 2 \cos \theta \left(1 - \frac{a^3}{r^3}\right)$$

$$-4\pi b^2 = c \cos \theta \left[1 + \frac{2a^3}{r^3}\right]^{1/2} = -3c \cos \theta$$

$$b = 3c \frac{\cos \theta}{4\pi}$$

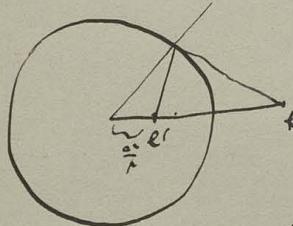


66

$$\text{outer Tadpole} + \int_{r_1}^{r_2} 2\pi b r^2 dy = \frac{2\pi a^2}{4\pi} c \int_{r_1}^{r_2} r^2 \cos^2 \theta dy = 3a^2 c \frac{r_2}{4}$$

$$\text{inner ring Tadpole} + \frac{\int_{r_1}^{r_2} 2\pi b r^2 \cos^2 \theta dy}{\int_{r_1}^{r_2} 2\pi b r^2 dy} = \frac{\int_{r_1}^{r_2} r^2 \cos^2 \theta dy}{\int_{r_1}^{r_2} \cos^2 \theta dy} = \frac{a^3 r_2}{\frac{r_2^3 - r_1^3}{3}} = \frac{a^3 r_2}{\frac{r_2^2 + r_1 r_2 + r_1^2}{3}} = \frac{2}{3} a$$

$$\text{Moment} = \frac{3a^2 c}{4} \cdot \frac{4}{3} a = \cancel{\text{crosses}} \quad \cancel{\text{crosses}} \quad \cancel{\text{crosses}} \quad ac$$



$$U_e = \frac{e}{r} + \frac{e'}{r'}$$

$$U_i = \frac{e''}{r} + \frac{e'''}{r''}$$

$$e + \frac{e' p}{a} = e'' + \frac{e''' p}{a}$$

$$(e - Ke'')_a + (e' - Ke''') \frac{p^3}{a^2} = 0$$

$$(e - Ke'')_p + (e' - Ke''') \frac{p^2}{a} = 0$$

$$Ke'' = R$$

$$Ke''' = e'$$

$$e + \frac{e' p}{a} = \frac{1}{R} [e + e' \frac{p}{a}]$$

$$e' = -\frac{a}{R} e$$

$$\left. \begin{aligned} \frac{e}{p^2 + a^2 - 2ap \cos \theta} + \frac{e'}{p^2 + a^2 - 2a^2 \cos^2 \theta} &= \frac{e''}{p^2 + a^2 - 1} \\ &= \frac{e' p}{a^2 + p^2 - 2ap \cos \theta} \end{aligned} \right\} U_i = U_e \Big|_{r=a}$$

$$e + \frac{e' p}{a} = e'' + \frac{e''' p}{a}$$

$$\frac{e(r - p \cos \theta)}{\sqrt{R^3}} + \frac{e' p(r - \frac{a^2}{p} \cos \theta)}{a^2 \sqrt{R^3}} = K \left[ \frac{e''(a - p \cos \theta)}{\sqrt{R^3}} + e''' \frac{p^3}{a^3} (-) \right]$$

$$\cancel{(e - Ke'')}(a - p \cos \theta) + \cancel{e' \left( \frac{p^3}{a^2} - \frac{p^2}{a} \cos \theta \right)} = 0$$

$$e' \frac{p^2}{a^2} (p - a \cos \theta)$$



$$U_1 - U_2 = x \frac{\partial U_1}{\partial x} + (l-x) \frac{\partial U_2}{\partial x}$$

$$= \frac{\partial U_1}{\partial x} \left[ x + (l-x) \frac{U_2}{U_1} \right]$$

$$= \frac{b_1}{a_1} \left[ x + \frac{l-x}{K_1} \right]$$

$$W = \frac{I}{2} \frac{b_1^2}{a_1^2} \left[ \frac{x}{K_1} + \frac{l-x}{K_2} \right]$$

$$U_1 = c x \left( 1 - \frac{c^3}{x^3} \right) = c x - c x^3 \frac{9}{2}$$

~~$$\frac{\partial U_1}{\partial x} = \sqrt{\frac{2}{x}} \left( \frac{\partial x^3}{\partial x} \right)$$~~

$$\frac{\partial U}{\partial x} = \frac{\partial V}{\partial x} - \frac{\partial W}{\partial x} \quad \text{Natural unit}$$

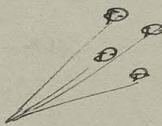
$$\nabla U = 0$$

$$\begin{cases} \frac{\partial U}{\partial x} \\ \frac{\partial U}{\partial y} \\ \frac{\partial U}{\partial z} \end{cases}$$

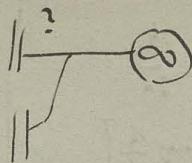
$$\varphi = \int_{\text{bottom}}^{\text{top}} \left[ \frac{\partial V}{\partial x} \frac{\partial u}{\partial x} + \frac{\partial V}{\partial y} \frac{\partial v}{\partial y} + \frac{\partial V}{\partial z} \frac{\partial w}{\partial z} \right] dw$$

~~$$= \int_{\text{bottom}}^{\text{top}} \nabla \cdot \mathbf{V} \cdot \mathbf{H} dw + \int_{\text{bottom}}^{\text{top}} \mathbf{H} \cdot \nabla \mathbf{V} dw$$~~

~~$$= \int_{\text{bottom}}^{\text{top}} \frac{1}{2} \frac{\partial \mathbf{V}}{\partial n} \cdot \mathbf{H} dS = \frac{1}{2} S$$~~



Ik mögliche Leistung und:



Feraday 1837

positive induction capacity  
negative dielectric常数

~~Alla~~ 26

Work 18 Paraffin 2

Lorke 3

Hele 3

Rika 6

Erka 3 - 8

(Thin  
reinforced)

Tugentz 2.2

Benzel 2.3

Anthe 7.2

Slk. 2.6

WW. 88

Alum.

parite 1'000 590

H<sub>2</sub> 1'000 264

C<sub>62</sub> 1'000 946

—

1. V

2.  $\frac{V}{K}$

3.  $V - \frac{V}{K}$

Silber

Tannenbaum

$$\begin{aligned}
 W &= \oint \frac{\partial U}{\partial x} dx = \sum EK = -\frac{1}{2} \int U \left[ \frac{\partial (K \frac{\partial U}{\partial x})}{\partial x} + \dots \right] dx \\
 &= \underbrace{\frac{\partial}{\partial x} \left( U K \frac{\partial U}{\partial x} \right) + \dots + K \left( \frac{\partial U}{\partial x} \right)^2}_{=0} \\
 &= - \int U K \frac{\partial U}{\partial x} dx + \int \left[ K \left( \frac{\partial U}{\partial x} \right)^2 \dots \right] dx
 \end{aligned}$$

W mierniku pole jui nie moze byc

$$2e \frac{e'}{r}$$

$$F = \frac{ee'}{kr^2}$$

$$\text{ani } X = \sqrt{\frac{x-f}{kr^2}}$$

68

tylko rozkladajmy:

$$W = \frac{1}{2} \int K \left[ \left( \frac{\partial U}{\partial x} - T \frac{\partial U}{\partial r} \right) + T \left( \frac{\partial U}{\partial r} \right) \right] dr$$

$U = \text{wysokosc}$ ;  $\frac{\partial U}{\partial r}$  moga byc w poziomie;  $\frac{\partial U}{\partial x}$

$$\int \frac{\partial U}{\partial x} K \frac{\partial U}{\partial r} dr = 2W + \int U \frac{\partial^2 (K \frac{\partial U}{\partial r})}{\partial x^2} dr - \int 4\pi K d\sigma$$

$$\int K \frac{\partial U}{\partial r} d\sigma = -4\pi m$$

$$\int K \frac{\partial U}{\partial r} d\sigma$$

$$\downarrow \quad \frac{\partial (K \frac{\partial U}{\partial r})}{\partial x} + \frac{\partial (K \frac{\partial U}{\partial r})}{\partial y} + \frac{\partial (K \frac{\partial U}{\partial r})}{\partial z} = -4\pi p$$

$$K_1 \frac{\partial U_1}{\partial n_1} + K_2 \frac{\partial U_2}{\partial n_2} = -4\pi p$$

druga warunek graniczny

$$\delta_1 \frac{\partial U_1}{\partial x_1} + \left( \delta_1 \frac{\partial U_1}{\partial n_1} + \delta_2 \frac{\partial U_2}{\partial n_1} \right) \delta_2 \frac{\partial U_2}{\partial n_2} + \left( \delta_2' \frac{\partial U_2}{\partial n_2} + \delta_1' \frac{\partial U_1}{\partial n_2} \right) = 0$$

$$\text{wtedy } \frac{\delta}{\delta} \text{ miern. male: } \frac{\partial U_1}{\partial n_1} = \frac{\partial U_2}{\partial n_2}$$

$$K_1 \frac{\partial U_1}{\partial n_1} = -4\pi p \text{ reprezentuje}$$

$$K_1 \frac{\partial U_1}{\partial n_1} = K_1 K_2 \frac{\partial U_2}{\partial n_2} \text{ nie izol. miniat.}$$

Na poziomie nie jest.

$$t_{\alpha_1} = \frac{\frac{\partial U_1}{\partial x_1}}{\frac{\partial U_1}{\partial n_1}}, \quad t_{\alpha_2} = -\frac{\frac{\partial U_2}{\partial x_2}}{\frac{\partial U_2}{\partial n_2}}$$

$$t_{\alpha_1} = -\frac{\frac{\partial U_2}{\partial n_1}}{\frac{\partial U_1}{\partial n_1}} = \frac{K_1}{K_2}$$

$$\frac{vol}{Vol} = \frac{n-1}{n+2} \quad \text{troye kant.} \quad \lambda = \frac{1}{\sqrt{n+2}\sqrt{2}} = \frac{\mu}{(\frac{1}{3})\rho c}$$

$$= \frac{k-1}{k+2} =$$

$$\alpha = \frac{1}{6} \sqrt{n+2}^3$$

$$\alpha \lambda = \frac{1}{6} \frac{1}{\sqrt{2}} \neq \frac{1}{10}$$

$$N_p \quad \lambda_{H_2} = 0.000018$$

$$\lambda_{O_2} = 0.000010$$

$$k = 1.000264$$

$$590$$

$$\alpha = 0.000088$$

$$0.000166$$

$$0.14 \cdot 10^{-7} \text{ cm}$$

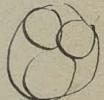
$$0.16 \cdot 10^{-7}$$

$$0.23$$

CH<sub>3</sub>

przyber 5 cm<sup>3</sup> masyne nie wtedy brzegi metalu

wysokość jest co zawsze nieznana bo np.  $k=80$  ale jest masywnie



$$\frac{R}{3\sqrt{2}} = \frac{3.14}{4.2} + \frac{3}{4} = \frac{k-1}{k+2} = \alpha$$

$$\frac{R}{3\sqrt{2}}$$

$$k-1 = \alpha k + \frac{1}{2} \alpha$$

$$K = \frac{2\alpha+1}{1-\alpha} = \frac{10}{1} = 10 = \text{największa wartość reakcji}$$

do reakcji w stanie troye nie ma żadnej jasności o którym jednakże nie mamy żadnych danych

o której typie innego kształtu metalu

"Poterzycia dylekt."

"Przemiany dylekt."

$$\begin{aligned} \chi_d &= \frac{n-1}{n+2} = \rho \\ \frac{n+1}{n-1} \rho &= \text{wartość} \end{aligned}$$

$$f = \frac{ee'}{K r^2}$$

$$U = \int \frac{\rho dr}{K r^2}$$

$$\nabla U = -\frac{4\pi\rho}{K} = p$$

$$k \frac{\partial U}{\partial n} = -4\pi b$$

ne unendlich

rotiere ~~um~~  $C = k C_0$

Abstand zwischen den Platten  $V$  Tiefen  $\varphi$

$$\text{pot. zentrale des dielektr. pot.} = V \frac{e_0}{K}$$

a dopp. Ladung  
jede Platte Ladung  $\frac{1}{2} Q$   
jed. w. dopp. Ladung  $\approx K$

Energie pro dielekt.  $W = \frac{1}{2} \iint \frac{\rho \rho' dr}{K r^2} = \frac{1}{2} \int \rho U dr$

Dielectrico zwischen zwei durch einen dielektr. isolator?

na neutral

$$\underbrace{K_1 \frac{\partial U_1}{\partial n} + K_2 \frac{\partial U_2}{\partial n}}_{\delta W} = 0$$

$$\frac{\partial U_1}{\partial n} + \frac{\partial U_2}{\partial n} = \frac{\partial U_1}{\partial n} \left( 1 + \frac{K_2}{K_1} \right) = -4\pi b'_1$$



$$\delta_1 = -\frac{1}{4\pi} K_1 \frac{\partial U_1}{\partial x}$$

$$\delta_2 = \frac{1}{4\pi} K_2 \frac{\partial U_2}{\partial x}$$

$$U_2 - U_1 = (x-a) \frac{\partial U_2}{\partial x} + a \frac{\partial U_1}{\partial x}$$

$$= \frac{\partial U_1}{\partial x} \left[ x + (a-x) \frac{K_1}{K_2} \right]$$

$$\delta_1 = \frac{K_1}{4\pi} \frac{V-U_1}{x} = -\delta_2 = \frac{K_2}{4\pi} \frac{U_2-V}{l-x}$$

$$V = \frac{K_1 U_1}{x} + \frac{K_2 U_2}{l-x}$$

$$\text{wegen } U_1 = 0 \quad \frac{K_1 U_1}{x} = 0$$

$$K_1 U_1 + K_2 U_2 = \frac{K_1 U_1}{x}$$

$$W = \frac{1}{2} \int (U_1 \delta_1 + U_2 \delta_2)$$

$$= \frac{\int}{8\pi} \left[ -K_1 U_1 \frac{\partial U_1}{\partial x} + K_2 U_2 \frac{\partial U_2}{\partial x} \right] = \frac{\int}{8\pi} \left[ -U_1 + U_2 \right] \underbrace{K_1 \frac{\partial U_1}{\partial x}}$$

$$= \frac{\int}{8\pi} (U_2 - U_1) K_1 \left[ x + (a-x) \frac{K_1}{K_2} \right]$$

$$\frac{\partial W}{\partial x} = \frac{\int}{8\pi} (U_2 - U_1) \left[ K_1 - \frac{K_1}{K_2} \right]$$

so es passen nur gradiung mit raus

$$\text{Zaten: } \frac{\partial V_1}{\partial n_1} = - \frac{\partial V_2}{\partial n_2}$$

$$\frac{1}{K_1} \frac{\partial V_1}{\partial x_1} = \frac{1}{K_2} \frac{\partial V_2}{\partial x_2}$$

$$K_1 \frac{\partial U_1}{\partial n_1} = - K_2 \frac{m_2}{m_1}$$

$$\frac{\partial U_1}{\partial n_1} = \frac{\partial U_2}{\partial n_2}$$

$$-q_{AB}^2 = \left(1 - \frac{K_1}{K_2}\right) \frac{\partial U_1}{\partial n_1}$$

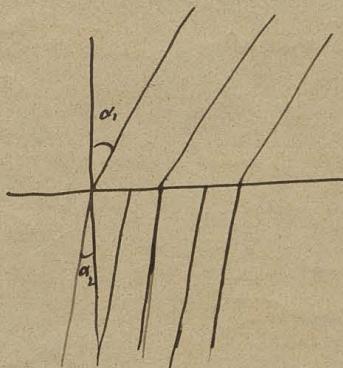
Nun ist mir ziemlich schlecht  
wie kann ich dringend jah  
wieder nicht weiterdrin!

$$\frac{1}{K_1} t_{pd_1} = \frac{1}{K_1} \frac{\partial V_1}{\partial x_1} \neq \frac{\partial V_1}{\partial n_1} = \frac{1}{K_2} t_{pd_2}$$

tatsache same zustand

die passiert hier ich kann sie es passieren

$\approx 6'$



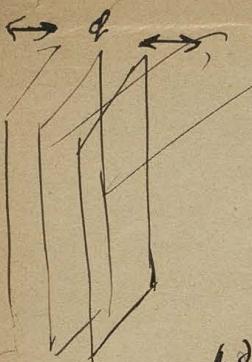
Na passen nicht mehr konduktoren:

$$\int \sigma V dx = q_{AB} = K \frac{\partial U}{\partial n}$$

$$\frac{\partial V}{\partial x} = K \frac{\partial U}{\partial x} = \cancel{\frac{\partial U}{\partial x}} + \cancel{\frac{\partial U}{\partial n}} \frac{\partial U}{\partial x} (1 + \epsilon \sigma) \left( \frac{\partial V}{\partial x} - \frac{\partial \varphi}{\partial x} \right)$$

$$\cancel{\frac{\partial U}{\partial x}} = \cancel{\frac{\partial U}{\partial n}} \frac{\partial U}{\partial x} - (1 + \epsilon \sigma) \frac{\partial \varphi}{\partial x}$$

$$\frac{\partial \varphi}{\partial x} = \frac{\partial V}{\partial x} - \frac{\partial U}{\partial x} = (K-1) \frac{\partial U}{\partial x} - q_{AB} \epsilon \sigma \frac{\partial U}{\partial x}$$



$$F = \frac{V^2}{8\pi s^2}$$

$$\varphi = 2 \frac{V - V' f}{4\pi s} f$$

$$\frac{\partial}{\partial x} \left( K \left[ \frac{e_1}{x_1} + \frac{e_2}{x_2} \right] \right) = \mathcal{H} = \frac{\partial K}{\partial x}$$

~~$\# H$~~

Maximowyzna rotacja K



$$\frac{\partial}{\partial x} \left( \frac{e_2}{x_2} \right) = V$$

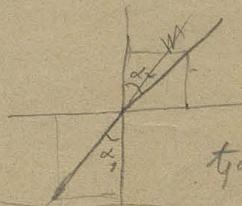
= right part  
was swapped

$$x_1 > x_2$$

~~$K_1 \frac{\partial U}{\partial x_1} = K_2 \frac{\partial U}{\partial x_2}$~~  , jakaś mityka nie działa.

$$\left( \frac{\partial U}{\partial x_1} \right)_t = \left( \frac{\partial U}{\partial x_2} \right)_t$$

następne zetknięcie linii H



$$t_{q,x} : t_{q,x} = \frac{\partial U}{\partial x}, \frac{\partial U}{\partial x} = K_1 \cdot K_2$$

Jedzi robi utwierdzony pochodne  $\frac{\partial U}{\partial x}$  etc. to one natychmiastowe zetknie

zatem  $B \left\{ \begin{array}{l} \frac{\partial V}{\partial x} \\ \frac{\partial V}{\partial y} \\ \frac{\partial V}{\partial z} \end{array} \right.$  pozostały

Indukcja nie zmienia

linii nida kijy przechodząc przez zetknięcie

zatem i-kap jok dawnyj =  $\frac{\partial V}{\partial x} + \dots = \frac{\partial(K\mathcal{H})}{\partial x} + \frac{\partial(KY)}{\partial y} + \frac{\partial(KZ)}{\partial z}$

$L^{-k}_{\text{nap}} = K D^2 U + D^2 V$

With this more generalization the job becomes the Gauss


$$dI \left( \frac{\partial V_1}{\partial n_1} + \frac{\partial V_2}{\partial n_2} \right) = -4\pi dI b$$

$$-4\pi b = K_1 \frac{\partial U_1}{\partial n_1} + K_2 \frac{\partial U_2}{\partial n_2}$$

were no boundary condition  $\boxed{-4\pi b = K \frac{\partial U}{\partial n}} = \frac{V}{b}$

Here  $U$  and  $V$  [V] are weighted shifts.

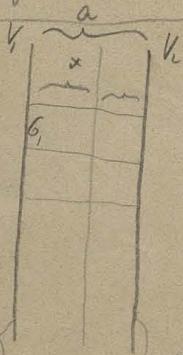
process poly. site (no junction many) strings  $v_i = H(U)$

Type of condensator noted does not type source pot.  $U$  there must

f. know where exactly bar smooth shell.

From job Faraday magnet  $K$

$$\text{Energy} = \frac{1}{2} \sum Q U = \frac{1}{2} \iint \nabla V \cdot U \, d\sigma$$



$$G_1 = \frac{1}{4\pi n} - \frac{1}{4\pi n} \frac{\partial V}{\partial x} = -\frac{1}{4\pi n} \frac{V_2 - V_1}{a}$$

$$G_2 = \frac{1}{4\pi n} \frac{\partial V}{\partial x} = \frac{1}{4\pi n} \frac{V_2 - V_1}{a}$$

~~$$V_2 - V_1 = K_2 \frac{\partial U_2}{\partial x} = K_1 \frac{\partial U_1}{\partial x} = \frac{\partial V}{\partial x} = 0$$~~
$$U_2 - U_1 = \alpha \frac{\partial U_1}{\partial x} + (\alpha - 1) \frac{\partial U_2}{\partial x}$$

~~$$V_2 - V_1 = K_2 \frac{\partial U_2}{\partial x} = K_1 \frac{\partial U_1}{\partial x} = \frac{\partial V}{\partial x} = 0$$~~

$$U_e = \frac{4}{3} \pi a^3 J \frac{x}{r^3} + cx = \left( \frac{4}{3} \pi a^3 J \frac{x}{r^2} + cx \right) \cos \varphi$$

$$U_i = \frac{4}{3} \pi J x + cx = \left( \frac{4}{3} \pi J + c \right) \cos \varphi$$

$$\mu \left( \frac{4}{3} \pi J + c \right) = - \frac{8}{3x} J + c \quad | \cdot r \quad \frac{\partial U_i}{\partial r} = \frac{\partial U_e}{\partial r}$$

$$\frac{4}{3} \pi J = \frac{c(1-\mu)}{\mu+2}$$

$$U_e = cx \left\{ 1 + \frac{1-\mu}{\mu+2} \frac{a^3}{r^3} \right\} = cx \left\{ 1 - \frac{\mu-1}{\mu+2} \frac{a^3}{r^3} \right\}$$

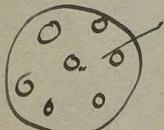
$$U_i = cx \left\{ 1 + \frac{1-\mu}{\mu+2} \right\} = cx \frac{3}{\mu+2}$$

do kuli purnama:  $\frac{\partial U_i}{\partial r} = 0 \quad (R=\infty)$

$$U_i = 0$$

$$U_e = cx \left( 1 - \frac{a^3}{r^3} \right)$$

~~jedna~~



$$\sum cx \frac{a^3}{r^3} = \sum c a^3 \frac{\partial \left(\frac{1}{r}\right)}{\partial r} \dots = n \frac{ca^3 x}{R^3} \rightarrow \text{redukce a součet výšek}$$

jednotlivé výšky:

$$n a^3 = \frac{k-1}{k+2} a^3$$

$$n \frac{a^3}{3} = \frac{k-1}{k+2} \frac{4a^3}{3}$$

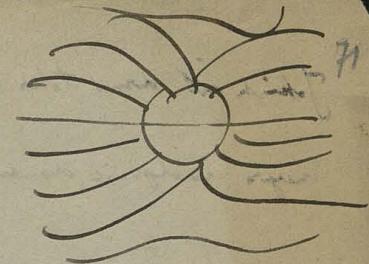
$$\text{střední výška} = \frac{k-1}{k+2}$$

Počítání hmotnosti:  $\frac{\partial U_i}{\partial r} = \frac{3c}{r^2}$

počítání hmotnosti:  $c = \frac{m}{4\pi R^3}$

$$U_e = cx - \frac{3c n}{R^2} \frac{a^3}{r^3}$$

zatím  $3 \cdot n a^3 = (k-1)$



jiné dílky kuli purnama  
vložit  $c = 1 - \frac{2a^3}{R^3}$   
počítat vzdálosti  
zatím  $a^3 = \frac{4}{3} \pi R^3$   
 $\Rightarrow R^3 = \frac{3a^3}{4\pi}$

to tykají se výšky vzdálostí  
vzdálosti mezi vodorovnými polosférami  
je tedy srovnatelná

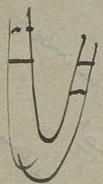
~~jedna~~  
jedna výška vzdálosti mezi vodorovnými polosférami  
kuli purnama je tedy to jistě

$$\rho \approx \frac{k-1}{k+2}$$

Tjekk nu denne tekniske ?  $\hat{z}$ -dugang !

Bruger analogien da en. stat. :  $W = \frac{1}{\rho n} \int u f_z dv = \frac{1}{\rho n} \int f_z dv = \underline{\underline{\underline{\frac{1}{\rho n} \int f_z dv}}}$

med  $\hat{z}$  drejning  
param. v. virkende poler



$$W = W_0 + \frac{B^2}{\rho n} \left( \frac{1}{\mu} - 1 \right) g x + \rho g \frac{x^2}{2} g$$

$$\frac{\partial W}{\partial x} = 0 : \quad \frac{1-\mu}{\mu} \frac{B^2}{\rho n} = - \rho g x g$$

$$x = \left( \frac{n-1}{\mu} \frac{B^2}{\rho n \rho g} \right)^{\frac{1}{2}} = \frac{\kappa H^2}{2 \rho g}$$

$$K_{H=0} = -10^6$$

$$H = \frac{-10^6}{20.000}$$

$$\frac{4 \cdot 10^8 \cdot 10^6}{2 \cdot 10^3} = \frac{8}{10} = 2 \text{ mm}$$

$$U_c = cx + \alpha \frac{x}{x^3} = \cancel{cx} \left( c + \frac{\alpha}{x^2} \right) = \cancel{c} \ln \varphi \left( cx + \frac{\alpha}{x^2} \right)$$

$$U_i = cx + \beta x = x(c+\beta) = \cancel{x} \ln \varphi \left( c + \frac{\alpha}{x^2} \right)$$

$$\beta = \frac{\alpha}{x^3}$$

$$U_c = cx + \alpha \frac{x}{x^3}$$

$$U_i = cx + \alpha \frac{x}{x^2}$$

$$U_c = cx \left\{ 1 + \frac{a^3}{x^3} \frac{K_i - K_c}{2K_i + K_c} \right\}$$

$$U_i = cx \left\{ 1 + \frac{K_i - K_c}{2K_i + K_c} \right\}$$

$$\cancel{K_i} \left( c - \frac{2\alpha}{x^3} \right) = \left( c + \frac{\alpha}{x^2} \right) K_c$$

$$\frac{\alpha}{x^3} = \frac{c(K_i - K_c)}{2K_i + K_c} x$$

$$\frac{\left[ c \left( \frac{x^2}{x^3} \right) - 1 \right] \frac{w}{(1-w)} \frac{b}{2} + 1}{2} = E$$

$$\frac{e^x}{x^2} / + \frac{e^x}{x^2} \cancel{K_i} + x^2 = 1$$

$$\tilde{y} = \frac{\cancel{3}kc}{\cancel{3}\mu} = \frac{kc}{\mu} = \frac{kc}{1+knk}$$

$$U_1 = \left| \begin{array}{c} \cancel{\frac{1-\alpha}{\mu+2} c/k} \\ \cancel{\frac{c}{\mu+2} \alpha^3} \end{array} \right| \frac{3kc}{k+2}$$

$$U_2 = \left| \begin{array}{c} \cancel{\frac{1-\alpha}{\mu+2} c/k} \\ \cancel{\frac{c}{\mu+2} \alpha^3} \end{array} \right| c \times \left[ 1 - \frac{\alpha^3}{\mu} \frac{k-1}{k+2} \right]$$

$$U_4 = c \times \left[ 1 - \frac{\alpha^3}{\mu} \frac{k-1}{k+2} \right] + c' \times \left[ 1 - \frac{\alpha^3}{\mu} \frac{k-1}{k+2} \right]$$

$$U_2 = \frac{3cx}{k+2} - c' \times \left[ 1 - \frac{\alpha^3}{\mu} \frac{k-1}{k+2} \right]$$

$$U_3 = \cancel{\frac{3cx}{k+2}} - \frac{3c'x}{k+2}$$

$$(c - \cancel{c}) \ln \theta \left[ 1 + \frac{\mu-1}{\mu+2} 2 \right] = \mu \left\{ \frac{3c}{\mu+2} \ln \theta - c' \left[ 1 + \frac{2\alpha^3 \mu - 1}{\mu+2} \right] \right\}$$

$$- c' \ln \theta \left[ 1 + \frac{2\mu - 1}{\mu+2} \right] \frac{\alpha^3}{A^3}$$

c

$$W = \frac{1}{2} \varphi U = \frac{1}{2} \frac{\varphi^2}{C} = \frac{1}{2} \varphi^2 \frac{m}{f} \frac{K_1 + (K_2 - K_1)x}{K_1(K_2 - (K_2 - K_1)x)} = \frac{f}{\delta x} \frac{U^2 K_1 K_2}{2K_1(K_1 - K_2)x}$$

$$\frac{dW}{dx} = \frac{1}{2} \frac{\varphi^2 m}{f} \frac{K_2 - K_1}{K_1 K_2} = 2\pi G^2 f \left( \frac{1}{K_1} - \frac{1}{K_2} \right)$$

} Działalność zmienia na poziomie  
przenosząc jądro do stóp

~~Therm~~

$$\frac{dW}{da} = 2\pi G^2 f \frac{K_1}{K_1 K_2} = \frac{2\pi G^2 f}{K_2}$$

} zmienia na poziomie jądra x  
 $K_2$  zaniknie

$$\frac{dW}{d(a-x)} = 2\pi G^2 f \frac{d}{d(a-x)} \left( \frac{K_2 x + (a-x) K_1}{K_1 K_2} \right) = \frac{2\pi G^2 f}{K_1}$$

} - - - jądro  $a-x$   
stopy

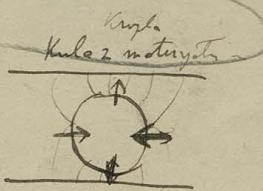
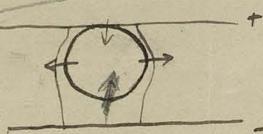
zmianice notowania = zmiany w

Fizyczny wymiar jest zmienny.

$K_1$  zaniknie

Wyk. położenia ciebie mechanizmu o totalnej mierze:

współ. bawka pozioma



$$2W = U \cdot \left[ xU + (a-x)KU \right]$$

$U$

$$\frac{1}{f} \frac{\partial W}{\partial x} = \frac{1}{2} \frac{U^2}{f^2} (1-K)$$

$x$

W polu sruini:



Deflection curve  $\Sigma \lambda_i n_i$   $\Sigma \lambda_i n_i = \Sigma \lambda_i n_i$

# bly corwylt wrt oppellor =  $\Sigma \lambda_i n_i$  & eroddwr nos

$$\therefore \Sigma n_i = \Sigma n_i \quad \therefore \Sigma \lambda_i n_i = \Sigma \lambda_i n_i$$

Parwaith norma mwyd wrth postffordd o phob 2m i wrth  $\Sigma n_i = \Sigma \lambda_i$

Moment o polu sruini = Ffwrdd o'r stegma = beginning

Ffwrdd o'r stegma mwyd wrth ystori. Amser trwm = jisili modd o'r polu corwylt

$$\text{Moment} = I_d \Sigma n_i \cdot \omega \varphi \quad \lambda = \sqrt{\frac{(x-x')^2 + (y-y')^2 + (z-z')^2}{(x-x')^2 + (y-y')^2 + (z-z')^2}}$$

city willtir relativ y byd o'r ffwrdd = moment jigo

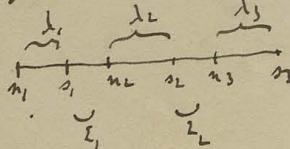
$$V = I_d \Sigma n_i$$

$$H = I_d \Sigma n_i$$

Jisili wahanolys wrth iwrth  $\Sigma n_i$  roedd hysbiliaid i'r jisili o'r stem normolys

$$\text{Moment} \quad \begin{array}{|c|c|c|c|c|c|} \hline & & & & & \\ \hline \end{array} \quad \text{tak i samp jeh} \quad \begin{array}{|c|c|c|c|c|c|} \hline & & & & & \\ \hline \end{array}$$

ba moronniwr o'r polu mabwysiadus wrth iwrth i'r jisili o'r stem normolys  
oppellor



$$\Sigma I_d n$$

$$\lambda_1 n_1 + \lambda_2 n_2 + \lambda_3 n_3$$

$$(n_1 + n_2 + n_3) \Delta$$

$$\Delta = \frac{\lambda_1 (\lambda_1 + \varepsilon_1) n_2 + (\lambda_1 + \varepsilon_1 + \lambda_2 + \varepsilon_2) n_3}{n_1 + n_2 + n_3}$$

$$+ \frac{(\lambda_1 + \lambda_2 + \lambda_3 + \varepsilon_1 + \varepsilon_2) n_1 + (\lambda_1 + \lambda_2 + \varepsilon_1) n_2 + \lambda_1 n_3}{n_1 + n_2 + n_3}$$

$$\Delta = -\lambda_1 n_1 - \lambda_2 n_2 - \lambda_3 n_3 =$$

wyl moment wyrddol y stegma o'r tak i wrth amysys rhodol

wyl horddol elementol o'r tak i wrth amysys rhodol moment  $I_{dw}$ , wrth iwrth

$$\int I_{dw} = \Sigma n_i \Delta \quad \int A dw = \Sigma n_i \lambda_i = \Sigma n_i \lambda_i \omega \varphi \quad \left| \begin{array}{l} \text{up} \\ \text{up} \\ \text{up} \end{array} \right| \quad \int I_{dw} = \Sigma n_i \lambda_i$$

$$\int A dw =$$

$$\int C dw =$$

$$p = \sqrt{\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2}}$$

jedna linia  $b=c=0$

74

$$b = \frac{E p}{4\pi abc} = \lim_{c \rightarrow 0} \frac{E}{4\pi a}$$

$$\sqrt{\frac{x^2}{a^2} + \frac{y^2}{b^2}} = \lim_{c \rightarrow 0} \frac{E}{4\pi a}$$

$$\frac{y^2 + z^2}{b^2} + \frac{x^2}{a^2} = 1$$

$$\frac{x^2 + y^2}{a^2} + \frac{z^2}{b^2} = 1$$

~~lin~~  $c=0$

$$b = \frac{E p}{4\pi abc} = \lim_{c \rightarrow 0} \frac{E}{4\pi a}$$

$$\sqrt{\frac{x^2 + y^2}{a^2} + \frac{1}{c^2} - \frac{x^2 + y^2}{a^2 c^2}}$$

$$= \cancel{\lim_{c \rightarrow 0}}$$

$$= \cancel{\lim_{c \rightarrow 0}} \frac{E}{4\pi a} \sqrt{\frac{1}{a^2} + \frac{2^2}{c^2}}$$

$$= \lim_{c \rightarrow 0} \frac{E}{4\pi abc} \frac{1}{\sqrt{\left(\frac{x^2}{a^2} + \frac{y^2}{b^2}\right)c^2 + 1 - \frac{x^2}{a^2} - \frac{y^2}{b^2}}}$$

$$26 = \frac{E}{2\pi ab} \frac{1}{\sqrt{1 - \frac{x^2}{a^2} - \frac{y^2}{b^2}}}$$

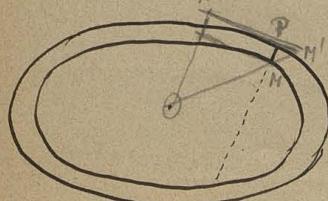
$$a=b : \quad \frac{E}{2\pi a^2} \frac{1}{\sqrt{1 - \frac{2^2}{a^2}}} \quad \text{jed pravdu v mnoz.}$$

Jedna inna metoda:

Widzisz dwojdywne zwarcie mozybly dwojczane homotetii sumi w mnoz. i wyciag na punkty zwarcia

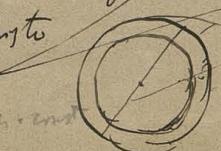
$$\frac{x^2 + y^2 + z^2}{a^2} = 1 \quad \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = 1 \quad \parallel \quad \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} = (1+\varepsilon)^2$$

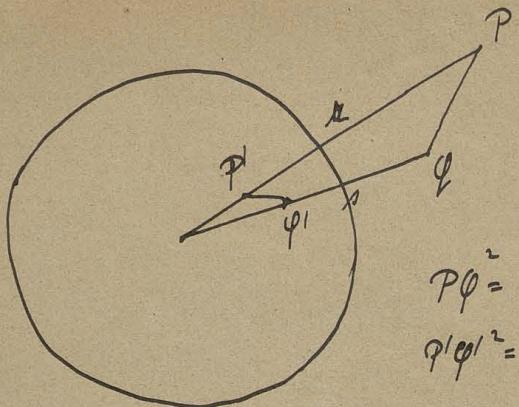
pokazyj si rysunek se grotow' prz. p



Nastecznim powstanie wezgadni linia normalna w t. sam punkt zwarcia

$$S = \frac{MM'}{OH'} = 1 - \cos \alpha$$





Inveraja

$$rr' = a^2$$

$$ss' = a^2$$

$$PQ^2 = r^2 + s^2 - 2rs \cos \theta$$

$$P'Q'^2 = r'^2 + s'^2 - 2r's' \cos \theta' =$$

$$= \frac{a^4}{r^2} + \frac{a^4}{s^2} - \frac{2a^4}{rs} \cos \theta = \frac{a^4}{rs} [s^2 + r^2 - 2rs \cos \theta]$$

$$= \frac{a^4}{r^2 s^2} \bar{P}\bar{Q}$$

$$\bar{P}'\bar{Q}' = \frac{a^2}{rs} \bar{P}\bar{Q}$$

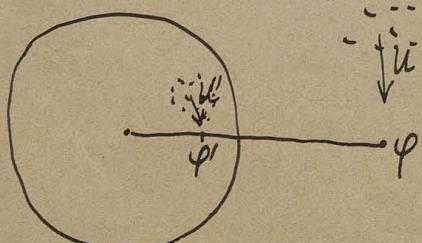
$$\text{Rot. Energy} P \omega \varphi = \frac{E}{\bar{P}\bar{Q}}$$

$$U' = \frac{E'}{\bar{P}'\bar{Q}'} = \frac{E'}{\bar{P}\bar{Q}} \frac{rs}{a^2} = \frac{E'}{E} \frac{rs}{a^2} U \quad \text{jishi tara rotatory}$$

$$E' = E \frac{a}{r}$$

$$U' = U \frac{a}{r} = \frac{a}{s} U$$

wie jishi many tara jahis bdi  
many suratka i odorozijamy ja, zinverja rame sebiri many E u' u'  
spisob, to pereyati tak otym angsh mas u' punkti tara -



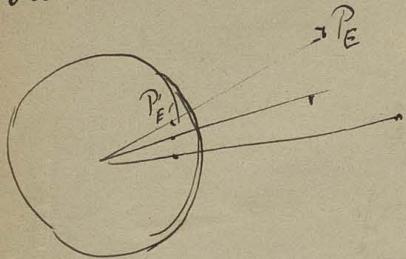
$$U' = U \frac{a}{s}$$

wie jishi tara dotomy jisse may

$U_a$  u' punkti O zemekrem - to

$$V = U' + \frac{U_a}{s} = 0 \text{ rota inverja}$$

Metoda obrazów

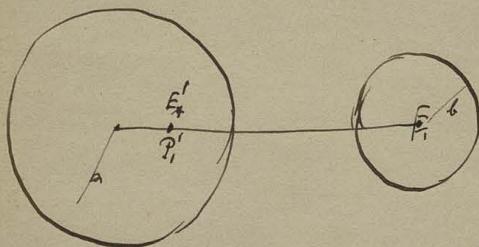


$$rr' = a$$

$$E \propto = E' \frac{a}{a}$$

dystans elektryczny & skutek indukacji  
zwane są określaniem nas  $E'$  --  
czyli jasne! zawsze tym samym daje to zadanym nam  
trudnościom

ale n.p. kula na kuli:



Murphy:

metoda przekształcająca

$E_1$  wyrażają obrazem  $P'_1$

$$E'_1 = \frac{E_1 a}{EP'_1}$$

to określić gęstość  $E_2 = \frac{E'_1 b}{EP'_1} \propto P'_2$

to znaleźć  $E'_2 = \frac{E_2 a}{P_2} = -\text{ktw.}$

pozycja na unikalnym punkcie do której nikt nie przypomni  $V=0$   
dla rozumieć myśląć

Potencjalny punkt:



$$6 \int \frac{ds}{\sqrt{r^2 + s^2}} = 2 \left[ \log(s + \sqrt{s^2 + r^2}) \right]_0^R = 2 \log \frac{R}{s}$$

$2 = \text{const}$

$$\frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} = 0$$

N.p. symmetrische Potenzial

$$\frac{\partial V}{\partial x} = \frac{\partial V}{\partial r} \frac{\partial r}{\partial x} = \frac{\partial V}{\partial r} \frac{x}{r}$$

$$\frac{\partial V}{\partial r} = \frac{\partial V}{\partial r} \cancel{\left( \frac{x^2}{r^2} \right)} + \frac{\partial V}{\partial r} \frac{\partial r}{\partial x} \frac{\partial x}{\partial r}$$

$$= \frac{dV}{dr^2} + \frac{1}{r} \frac{\partial V}{\partial r}$$

$$\left\{ \begin{array}{l} \frac{\partial V}{\partial r} = \frac{dV}{dr} \frac{x^2}{r^2} + \frac{\partial V}{\partial r} \frac{1}{r} - \frac{dV}{dr} \frac{x^2}{r^3} \\ \frac{\partial V}{\partial r^2} = \frac{d^2V}{dr^2} \frac{x^2}{r^2} + \frac{\partial V}{\partial r} \frac{1}{r} - \frac{dV}{dr} \frac{x^2}{r^3} \end{array} \right.$$

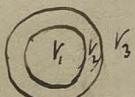
$$= \frac{1}{r} \frac{d}{dr} \left( r \frac{\partial V}{\partial r} \right) = 0$$

$$r \frac{\partial V}{\partial r} = \text{const} = \alpha$$

$$\frac{dV}{dr} = \frac{\alpha}{r}$$

$$V = \alpha \ln r + \beta$$

N.p. Condensator zwischen



$$V_1 = \beta_1, \quad \alpha_1 = 0$$

$$\text{Mit } V_{2A} = \alpha_2 \ln \frac{a}{A} + \beta_2 = V_1$$

$$V_{2A} = \alpha_2 \ln \frac{a}{A} + \beta_2 = V_3$$

$$\frac{\alpha_2 \ln \frac{a}{A}}{\alpha_2 \ln \frac{a}{A}} = V_1 - V_3$$

$$C = \frac{l}{2 \ln \frac{a}{A}}$$

$$\varphi = 2\pi \epsilon_0 l = \frac{(V_3 - V_1) l}{2 \ln \frac{a}{A}}$$

$$G_a = -\frac{1}{4\pi} \frac{\partial V}{\partial r} = -\frac{\alpha}{4\pi r} = -\frac{\alpha}{4\pi a}$$

$$\alpha_2 = \frac{V_3 - V_1}{2 \ln \frac{a}{A}}$$

$$G_a = \frac{V_3 - V_1}{4\pi a \ln \frac{a}{A}}$$

*Festuca verna tridens* Greene

$$I - S = 1 \quad H - K$$

$$\text{II} \quad g = k \quad h = k$$

$$\text{III} \quad S = \frac{1}{4} \quad H = k$$

$$\iiint S \nabla^2 H \, dv = \iint S \frac{\partial H}{\partial n} \, df - \iiint \left[ \frac{\partial^2 H}{\partial x^2} \cdot \hat{r}_x + \dots \right] dv$$

Principles surveying & magnetism

$$\begin{aligned} \iint \frac{\nabla^2 U}{r} d\omega &= \iint \frac{1}{r^2} \frac{\partial U}{\partial n} d\Omega - \iint \left( \frac{\partial^2}{\partial x^2} \frac{\partial U}{\partial x} + \dots \right) d\Omega \\ &= -4\pi U = \iint \frac{1}{r^2} \frac{\partial U}{\partial n} d\Omega + \iint \left[ \frac{\partial U}{\partial x} \frac{\partial r}{\partial x} + \frac{\partial U}{\partial y} \frac{\partial r}{\partial y} + \dots \right] d\Omega \\ &\quad \underbrace{\frac{\partial U}{\partial x} \omega(rx) + \dots}_{= \frac{\partial U}{\partial x}} = \frac{\partial U}{\partial x} \end{aligned}$$

$$dv = r^2 dw = r^2 \sin \varphi dy dx dr$$

$$U_0 = -\frac{1}{4\pi} \iint \frac{\partial U}{\partial n} \cdot \hat{n} d\sigma - \frac{1}{4\pi} \iint d\omega (U_{x_2} - U_{x_1})$$

Jidi teror pasti menyengsar ~~teror~~ = povi. priornu to  $H_1 = H_2$

$$\text{rot} \mathbf{v} = -\frac{1}{4\pi\alpha_0} \nabla \times \left( \frac{1}{r} \mathbf{M} \right)$$

A girls must serve many:

$$U_1 = -\frac{1}{4}n$$

between the two provinces, so that both authority states set themselves jointly  
against each other.

$$U_0 = -\frac{1}{4\pi n} \left[ \left( \frac{\partial U}{\partial n} \right)_{\text{ext}} - \frac{1}{4\pi n} \int d\omega (U_n - U_0) \right]$$

$$\Sigma_1 \quad \cancel{\text{Diagram}} \quad p + s^2 - 2$$



$$\frac{\Sigma_1}{2} + \frac{\Sigma_2}{2} = c_{20}$$

$$\Sigma_2 s^2 = \Sigma_1 s^2$$

$$\Sigma_1^2 (p_1^2 + s^2 - 2ps \sin \theta) = \Sigma_2^2 (p_2^2 + s^2 - 2ps \sin \theta)$$

punkthypoth. d'ordre 2  
wzg.  $\Sigma_1 p_1 = \Sigma_2 p_2$

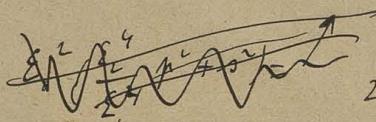
welche entst. Hypothese: punktig

$$\Sigma_1^2 (p_1^2 + s^2) = \Sigma_2^2 (p_2^2 + s^2)$$

$$p_1' = \frac{\Sigma_1^2 p}{\Sigma_1^2}$$

$$\Sigma_1 p_1 - \Sigma_2 p_2 = (\Sigma_1^2 - \Sigma_2^2)$$

$$= \frac{\Sigma_1^2}{\Sigma_1^2} \Sigma_1 p_1 - \Sigma_2 p_2 =$$



zater s = const zater knaak kft inadko systeem

vrijke dwars  $\frac{\partial u}{\partial x}$  moza dwongen rapport  $\frac{\partial u}{\partial s}$

moza toek. p  $\Sigma_1$ , s moza ro dann

$$M = \frac{\Sigma_1}{p^2 + s^2 - 2ps \sin \theta}$$

2 dwys symmetrie:

$$\Sigma_2^2 = \Sigma_1^2 \frac{p_1'}{p}$$

$$p_1^2 + s^2 = (p_1^2 + s^2) \frac{p_2}{p_1}$$

$$p_1 p_2^2 - p_2 p_1^2 = (p_2 - p_1)^2 \quad || \quad s^2 = \frac{p_1 p_1^2 - p_1' p_1^2}{p_1' - p_1} = p_1 p_1'$$

$$\text{zater } p' = \frac{s^2}{p}$$

$$\Sigma_2^2 = \frac{\Sigma_1^2 s^2}{p^2}$$

$$\Sigma_2 = \frac{\Sigma_1 s}{p}$$

$$U = \frac{\Sigma_1}{\sqrt{p^2 + s^2 - 2ps \sin \theta}} -$$

$$\frac{\Sigma_1'}{\sqrt{(p_1')^2 + s^2 - 2 \frac{p_1'}{p} s \sin \theta}}$$

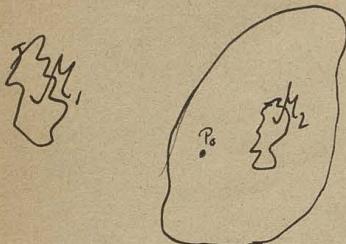
$$= \frac{\Sigma_1'}{\sqrt{p^2 + s^2 - 2ps \sin \theta}}$$

2 dwys dwingende zuks  
is in dwys moza te dwys  
dwys punkten, a van de  
6 toek. een jch jci mukking

paravodice ravnijeze raste nos

$$U_0 = U_1 + U_2$$

77



$$U_{\text{ext}} = - \iint \frac{\partial(U_1 + U_2)}{\partial n} d\Omega = \cancel{- \iint \frac{\partial U_1}{\partial n} d\Omega} - U_p + U_0$$

$$U_p = U_1 + \iint \frac{\partial(U_1 + U_2)}{\partial n} d\Omega = \text{const}$$

zatim tvoz potencijet  $U_1 + \int \delta \sim = \text{konstanta}$  u ravnopravju

$$\text{Kont: } U_{\text{ext}} = - \frac{1}{m} \int \delta$$

To predstavlja nam tvoz maličinu ravnopravju povišenje ravnopravju

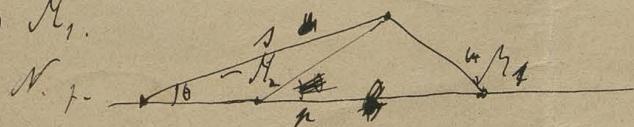
n.p. uzravnjujući tvoz potencijet  $U_2$  povišenje ravnopravju  $R_1, R_2$ ,

zatim obično tvoz jednog početnog potencijeta je na miji uvidljiv

masa  $- \frac{1}{m} \frac{\partial U}{\partial n}$  to je to nekakao ~~zatim~~ zatim u ravnopravju pot

zatim u svakoj maličini  $R_1$ , zato = skup potencija ravnopravju u bilo

masi  $M_1$ .



$$U = \frac{\Sigma_1}{R_1} - \frac{\Sigma_2}{R_2} = \text{const.}$$

uzravnjujući uzravnenje stupnjeva  $\Sigma_1 = \frac{(x-a)^2 + y^2}{R_1^2}$

$$\text{tako želis } U=0: \quad \frac{\Sigma_1}{R_1} = \frac{\Sigma_2}{R_2}$$



$$\Sigma_1^2 R_2^2 = \Sigma_2^2 R_1^2$$

$$\Sigma_1^2 = \frac{(x-a)^2 + y^2}{R_1^2}$$

$$\Sigma_2^2 = \frac{x^2 + (y-a)^2}{R_2^2}$$

$$\frac{\partial U}{\partial \alpha} = \frac{\varepsilon_1 (a - \rho \omega t)}{[r^2 + a^2 - 2\rho r \cos \theta]} \beta_L - \frac{\varepsilon' (a^4 - \rho' \omega t)}{[r^2 + a^2 - 2\rho r \cos \theta]} \beta_R$$

$$f = \frac{a^2}{r}$$

$$= \frac{\varepsilon_1 (a - \rho \omega t)}{[r^2 + a^2 - 2\rho r \cos \theta]} - \frac{\varepsilon \left( a - \frac{a^2}{r} \cos \theta \right)}{\left[ \left( \frac{a^2}{r} \right)^2 + a^2 - 2\rho \frac{a^2}{r} \cos \theta \right]} \beta_R$$

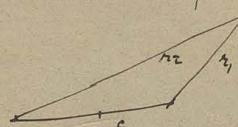
$$= \frac{\varepsilon (a - \rho \omega t) - a^2 \frac{a^2}{r} \cos \theta}{[r^2 + a^2 - 2\rho r \cos \theta]^{3/2}} = \frac{\varepsilon (a - \rho \omega t) \cos \theta}{r^3} \int \frac{dx}{\sqrt{1+x^2}} = \frac{\varepsilon (a - \rho \omega t) \cos \theta}{r^3} \int \frac{dx}{\sqrt{1+(x/c)^2}}$$

$$= \frac{\varepsilon (a - \rho \omega t)}{a (r^2 + a^2 - 2\rho r \cos \theta)^{3/2}}$$

$$\int \frac{dx}{\sqrt{1+(x/c)^2}} = \frac{c \arctan(x/c)}{x/c} = \frac{c \arctan(x/c)}{x/c}$$

W problemie oznacza, jaka dana wartość rozmieniona na prosty pierwiastek będzie

$$\text{tak } U = \frac{b}{r_1 + r_2 - 2c}$$



wtedy powierzchnia skrz. = objętość skrz.

$$\text{mającą się } -\frac{1}{2n} \frac{\partial U}{\partial r} = \text{miejsc. maks. 2 wówk. na}$$



$$r_1 + r_2 - 2c = a(r_1, r_2, \alpha)$$

$$(r_1 + r_2)(\cancel{r_1 + r_2}) = \frac{2c(1+\alpha)}{1-\alpha}$$

$$\frac{x^2}{a^2} + \frac{y^2}{a^2(1-\alpha)} > 1$$



Dowody na twierdzenie o mozy i kondensatorach

$$b = \frac{1}{4\pi} \frac{V_3 - V_1}{\delta}$$

78

$$Q = \frac{F}{4\pi\delta} (V_3 - V_1) \quad C = \frac{F}{4\pi\delta}$$

$$\text{Intej } \ln \frac{A}{a} = \ln \left(1 + \frac{\delta}{a}\right) = \frac{\delta}{a} - \frac{1}{2} \left(\frac{\delta}{a}\right)^2 + \dots$$

$$F = 2\pi a l$$

$$\frac{l}{2\frac{\delta}{a}} = \frac{2\pi a l}{4\pi\delta} \quad \text{p.e.d.}$$

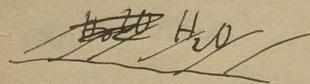
$$\text{wzór wynika } C = \frac{l}{2\ln \frac{A}{a}}$$

~~Funkcja to nie~~

wzór pozwala A stworzyć matkę

np.

Wówczas dla kablew jednej strony np. C zwróci funkcjonowanie



$$\text{np. } a = 3 \text{ mm}$$

$$A = 15 \text{ m}$$

$$C = \frac{l}{2\log 5} = \frac{l}{2} \cdot \frac{1}{2 \cdot 3 \dots 0.699}$$



$$A = \frac{30}{2} \text{ mm}$$

$$C = \frac{l}{2} \cdot \frac{1}{\ln 10} = \frac{l}{2} \cdot \frac{1}{23 \dots 1}$$

wzór np.  $C = \frac{l}{4}$

$$l = 5000 \text{ km} \quad C = \frac{5000}{4} = 1000 \text{ km}$$

wzór nowy C jed. kabelu  $a = 1000 \text{ km}$

szczególnie  $a = 6,360 \text{ km}$ . wzór 6 takich kablew = pojazd 2 km!

$$A = 60 \text{ m}$$

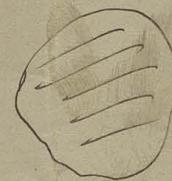
$$C = \frac{l}{2} \cdot \frac{1}{\ln 20} = \frac{l}{2} \cdot \frac{1}{2 \cdot 3 \cdot 13}$$

~~Funkcja te~~ rozwiązać dowody, opisać jak kondensator mać mozy zastosowane, by zatrzymać w tym samym czasie

$$W = \frac{1}{2} \sum V \varphi = \frac{1}{2} \sum \frac{e e'}{r}$$

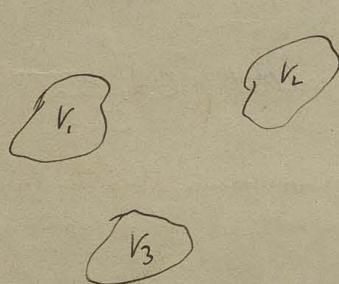
Wizzi jidli cito purodegu:

$$V = \text{const.}$$



$$W = \frac{1}{2} \pi V \varphi$$

Jidli roze cito purodegu w roomusolu elha.



$$W = \frac{1}{2} (\varphi_1 V_1 + \varphi_2 V_2 + \varphi_3 V_3)$$

Buy premijan eniemu uj upordui mi  $\varphi$ , jidli cito izolowane ale  $V$   
Lame  
Enyoi min' potei state

$$dW + dA = 0$$

$$\text{Fds} = -dW$$

$V_i$  hdi reljek od  $\varphi_n$ ; ujaki  $\eta^{\frac{1}{2}}$   
Jedz jidli wazthi wto izolowane, ale jidliem odzien Tadunk  $d\varphi_i$  joh ni  
zmieni  $W$ ?

$$\begin{array}{ccc} \varphi_1 & \varphi_2 & \varphi_3 \\ V_1 & V_2 & V_3 \end{array} \quad \begin{array}{c} \cdots \\ - \end{array}$$

$$\begin{array}{ccc} \varphi_1 + d\varphi_1 & \varphi_2 & \varphi_3 \\ V_1 + dV_1 & V_2 + dV_2 & V_3 + dV_3 \end{array} \quad \begin{array}{c} \cdots \\ - \end{array}$$

$$\begin{aligned} \delta W &= \sum \frac{1}{2} \sum \frac{e e'}{r} = \frac{1}{2} \sum \sum \left( \frac{e \delta e'}{r} + e' \frac{\delta e}{r} \right) = \sum e \frac{\delta e'}{r} = \sum \delta e' \sum \frac{e}{r} \\ &= \sum \varphi \delta V = \sum V \delta \varphi \end{aligned}$$

2 drayn strong:

$$Fw = \frac{1}{2} [\varphi_1 \delta V_1 + V_1 \delta \varphi_1 + \cancel{\delta \varphi_1 \delta V_1} + \varphi_2 \delta V_2 + \varphi_3 \delta V_3 + \dots] \\ = V_1 \delta \varphi_1$$

79

$$V_1 \delta \varphi_1 = \varphi_1 \delta V_1 + \varphi_2 \delta V_2 + \dots$$

$$\left\{ \begin{array}{l} V_1 = \varphi_1 \frac{\partial V_1}{\partial \varphi_1} + \varphi_2 \frac{\partial V_1}{\partial \varphi_2} + \dots \\ V_2 = \varphi_1 \frac{\partial V_2}{\partial \varphi_1} + \varphi_2 \frac{\partial V_2}{\partial \varphi_2} + \dots \\ \dots \end{array} \right. \quad \text{Potential coefficients}$$

to take  $\frac{\partial V_2}{\partial \varphi_1}$  or vice versa?

jidi vystan  $\varphi_2 = 0$  myi ethen  $\varphi_2 \cancel{\frac{\partial V_2}{\partial \varphi_1}} = 1$  &  $V_1 = \frac{\partial V_2}{\partial \varphi_1}$

otherwise take

$$\left\{ \begin{array}{l} \varphi_1 = V_1 \frac{\partial \varphi_1}{\partial V_1} + V_2 \frac{\partial \varphi_1}{\partial V_2} + \dots \\ \varphi_2 = - \end{array} \right. \quad V_1 \dots = 0 \quad V_2 = 1$$

$$\varphi_1 = \frac{\partial \varphi_2}{\partial V_1} =$$

rodzaj pionomu

ojohni nazwan pionomu

$$\frac{\partial \varphi_2}{\partial V_1} \quad \text{jidi vystan wiek konduktivity} = 0.$$

Twarz co do ist mechanizmch:  $Fw = \delta A = -\delta W = -\frac{1}{2} \sum V \delta \varphi = -\frac{1}{2} \sum \varphi \delta V$   
jednak wazne A stara jsi byc > 0 , zatem  $\delta V < 0$

piony i tzw. zasada odrzucania pionow

W obecnym przypadku: potencjalny mocy potencjalne statej mocy potencjalnej  
w swoim transmitem zwołanym elektrycznym

To zredukujemy na grawitacyjny

najprostszym mechanizmem  $\delta A$ , przez co energię sił obciążających o  $\frac{1}{2} \sum \vec{F} \cdot \vec{d}$   
 $= \frac{1}{2} \sum q \delta V$

także jednak potencjalny zwołany przez nasz zwołany elektryczny, takiże potencjalny  
porównując na grawitacyjny wysokość stady

potencjału energii  $\delta W = \sum q dV$  wedle tego co przedstawiono powyżej  
zatem w celu podniesienia energii o  $\frac{1}{2} \sum q \delta V = \frac{1}{2} \sum V \delta q$

więc aby przeprowadzić energię poruszającą się, dojść do minimum, na koniec  
zwołany elektryczny zwołany.

Jedli odwrotnie postępujemy:

○ ○ mechanizmy mogą oddziaływać na system:

$$\delta P_e = -\delta A$$

$\delta W = \delta P_e$  energia elektryczna poruszająca się

$= \frac{1}{2} \sum q \delta V$  tzw. mocą wykorzystaną elektryczną typu  
aż do samej potencjalnej co przedstawiono

$\delta W = -\sum q \delta V$  zatem według obliczeń my mamy do o  
 $\frac{1}{2} \sum q \delta V$

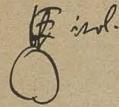
ale twarz bierze dobra

więc natok potencjalny  $\frac{1}{2} \sum q \delta V$

a o której rzeźce jest się mowa do

więc  $\sum q \delta V$  stracone mocy do zwołania w mocy elektrycznej i  
mocy statycznej konduktorów

Miejsce tzw. potencjalniaki praca:



80

I).  $V \rightarrow \infty$        $\varphi = -\frac{Ea}{r}$        $V=0$

II. izolowane do  $\infty$        $\varphi = -\frac{Ea}{r}$        $V = \varphi = -\frac{Ea}{r}$

wyznaczamy       $\varphi = -\frac{Ea}{r}$

III. zavor do ...       $\varphi = 0$

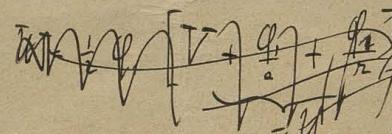
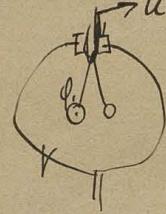
potencjał -- wyznacz       $\varphi = +\frac{Ea}{r}$

Coś daje ~ mniej więcej  
mniej więcej!  
Rzec zupełnie!

### Metryka inflacyjna

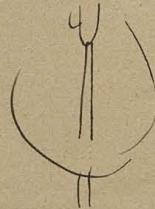
Zastosowanie elektrometry      strzałki do mierzenia potencjałów

Elektroskop



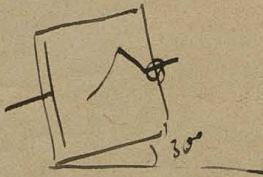
$$\varphi_1 = \alpha(U-V)$$

$$\text{to } \frac{\varphi_1}{a} + V = U$$



Przem

Wiel



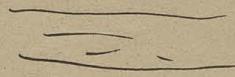
Metryka typu empirycznego i dobrane

do tego strzały biegły da

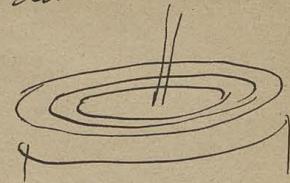
Kurles kuli trudno pochywić ...

absolut  
latajca elektryczna Przewo

Tele jadłostyczne



Spiralny



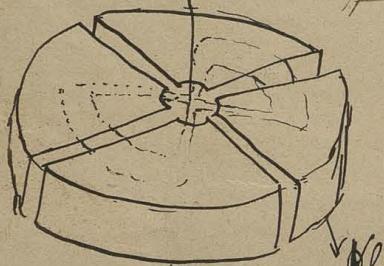
$$\delta W = \mathbb{F} \delta s = \frac{1}{2} \cancel{\mathbb{F} \delta s} = \frac{1}{2} \sum V \delta \varphi$$

$$Q_i = \frac{V}{4\pi d} f$$

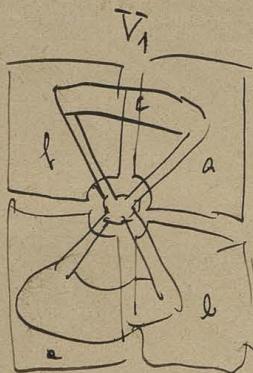
*to ziemiany, wylew do napełnienia  
ne parowarzchni (przemek wodny)  
kotek, t.j. spławnia  
ciśnienie powietrza, brak napełniania  
ciśnieniem*

$$\mathbb{F} \delta s = \frac{1}{8\pi} V^2 f \delta \varphi = \frac{V^2}{8\pi d^2} f \delta s$$

alto F minima' wktodajce ciśnieniu  
napełnienia spławnia  
alto f minima' wktu  
gdyż istnieje



$$\delta W = \sum Q \delta V = \sum V \delta \varphi$$



poz. wyjściowej i końc:

$$a' = a + k\varphi(V - V_a)$$

$$b' = b + k\varphi(V - V_b)$$

$$c' = c + k\varphi(V_a - V_b) - k\varphi(V - V_a)$$

$$c' = c + k\varphi(V_a - V_b)$$

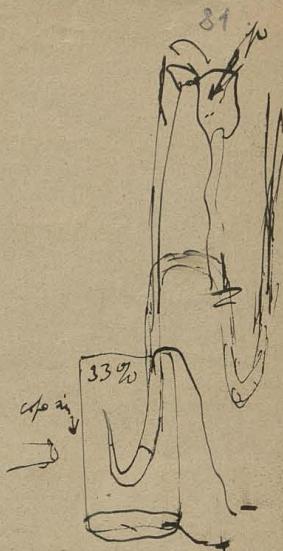
$$W' = \frac{1}{2} (a' V_a + b' V_b + c' V_c)$$

$$= \frac{1}{2} \underbrace{[a' a + \dots]}_{W'} + k\varphi \underbrace{[V_a(V - V_a) + V_b(V - V_b) + V_c(V - V_c)]}_{[2V(V_a - V_b) + V_b^2 - V_a^2]}$$

$$\begin{aligned} \bar{W}' - \bar{W} &= \frac{k\varphi}{2} [2V(V_a - V_b) + V_b \cdot V_a] = \\ &= k\varphi [V(V_a - V_b) + \frac{1}{2}(V_b - V_a)(V_b + V_a)] \\ &= k\varphi (V_a - V_b) \left[ V + \frac{V_b + V_a}{2} \right] = IA \end{aligned}$$

$$F = \frac{A}{2\varphi} = K (V_a - V_b) [- - -]$$

Jedli  $V$  bedzie wielki to  $\frac{F}{K_F} V (V_a - V_b)$

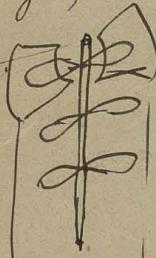


Stosunek rejestrujacy do mierzenia  $\frac{1}{100} V$  - kilka Volt

moins notwendig wizy i do wyjazdnych vol.

multiple van-de-catherometer (elektrontest voltmeter)

~~Wzajemny do lamp ziarowych itc. v technice 50-200V~~

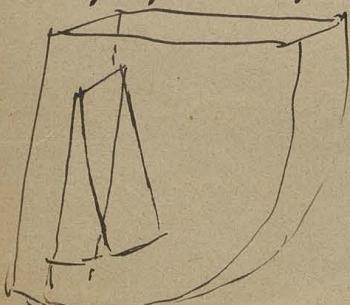


wizy si wystarcza pod  
a co najmniej je taka do  
pedois przedstawiony

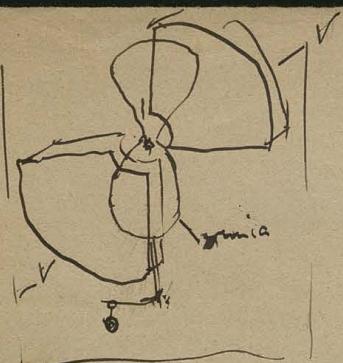
Torison Electrometer Kohlrausch

do wyjazdnych potr. wizy

Hartman - Braun



korzyst do little tryzy



Hahn  
Vertical electrometer

Potencjometr z grawitacyjnym kulem V

wzorowany na dawnych wąskich wachterskich mierzących napięcie do 2000V

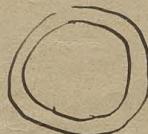
przy napięciu tyciągu 2000V

przy stałej sile grawitacji

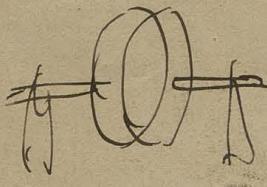
Akcelerometr aby mierzyć siłę grawitacji jasne znak pionowy



Kula migrująca



Wadensauer Kühnemann



trudno wykonać w tym stopniu skomplikowanej struktury

Szukaj my wadensauer

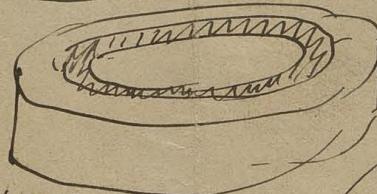


Abb. 21 rekonstrukcja  
wadensauer

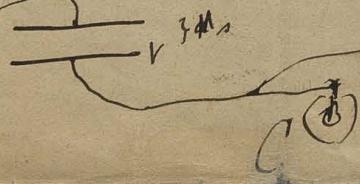
$$(C + c + \frac{M}{4\pi}) V_1 = \text{const.}$$

$$(C + c + \cancel{\frac{M}{4\pi}}) V_2 = \text{const.}$$

$$C + c = \dots$$

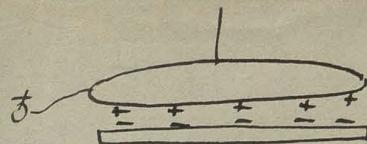
toż samo dla drugiej

$N_2$  toż:

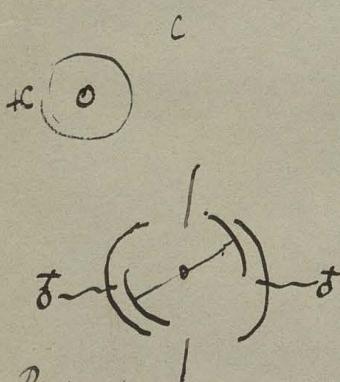
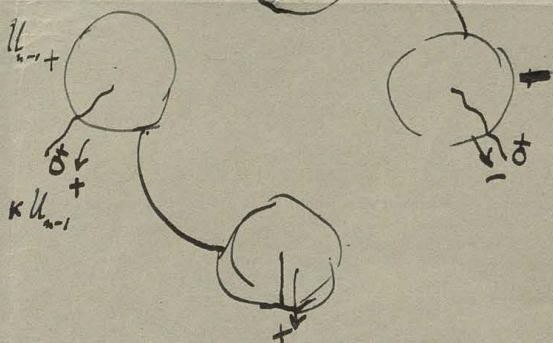
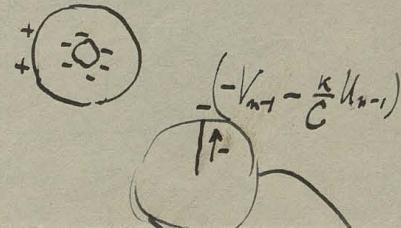
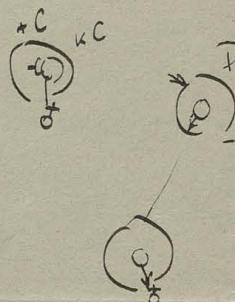
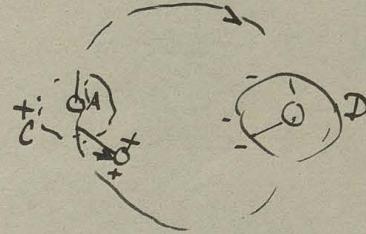
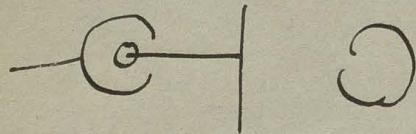


Elaston.

Elektrofor wird passiv induziert



Maschine mit einem motor



Reziproker

$$\delta = R_{n-1} + R_n$$

$$U_n = (1+\alpha) U_{n-1}$$

$$= (1+\alpha)^n U_0$$

$$-V_n = -V_{n-1} - \frac{k}{C} U_{n-1}$$

$$U_n = U_{n-1} + \frac{k}{C} V_{n-1}$$

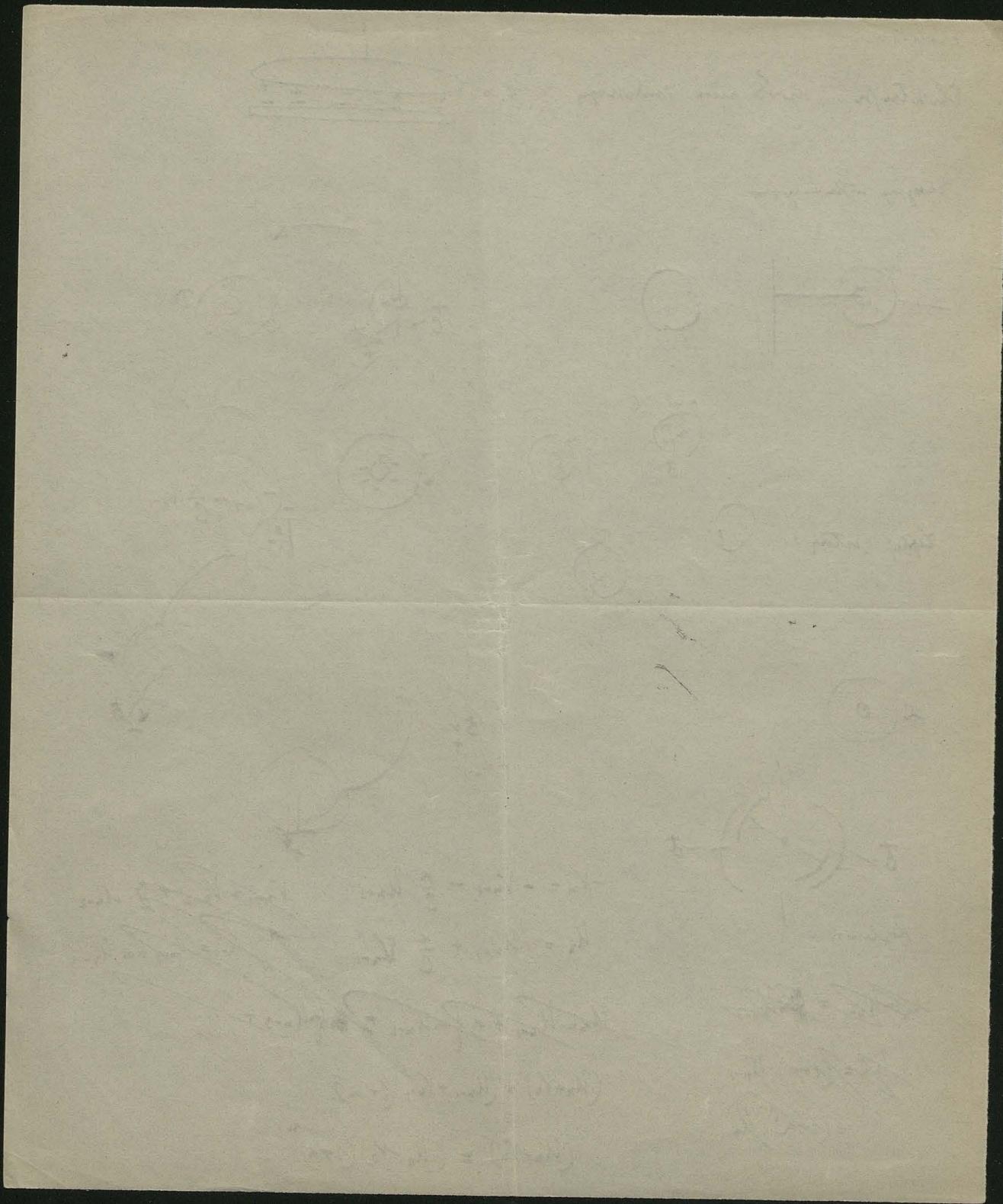
$$V_{n-1} = V_{n-2} + \frac{k}{C} U_{n-2}$$

$$V_{n-2} = V_{n-3} + \alpha U_{n-3}$$

$$U_n = U_{n-1} + \alpha R_{n-1} + \alpha R_{n-2} + \alpha R_{n-3} + \dots$$

$$(U_n + V_n) = (U_{n-1} + V_{n-1})(1+\alpha)$$

$$(U_n + V_n) = (U_0 + V_0)(1+\alpha)^n$$



Deklinator

Powystawianie Tadekina  $Q = K C (V_1 - V_2)$

$$-4\pi G = k \frac{\partial U}{\partial n} = k F_n = D_2$$

główne depresje  
linij rury

$$-4\pi m = \sqrt{k F_n} = \sqrt{D_2} \quad \leftarrow \text{przestawiany deklinator}$$

$$\rho = \operatorname{dis} \theta =$$

przeciwnie Tadekini

$$2 \operatorname{masy} m \operatorname{wykonaj} \\ 4\pi m \operatorname{linij} polaryzacji = 4\pi K m \\ \operatorname{linij} rury$$

przeciwnie Tadekini

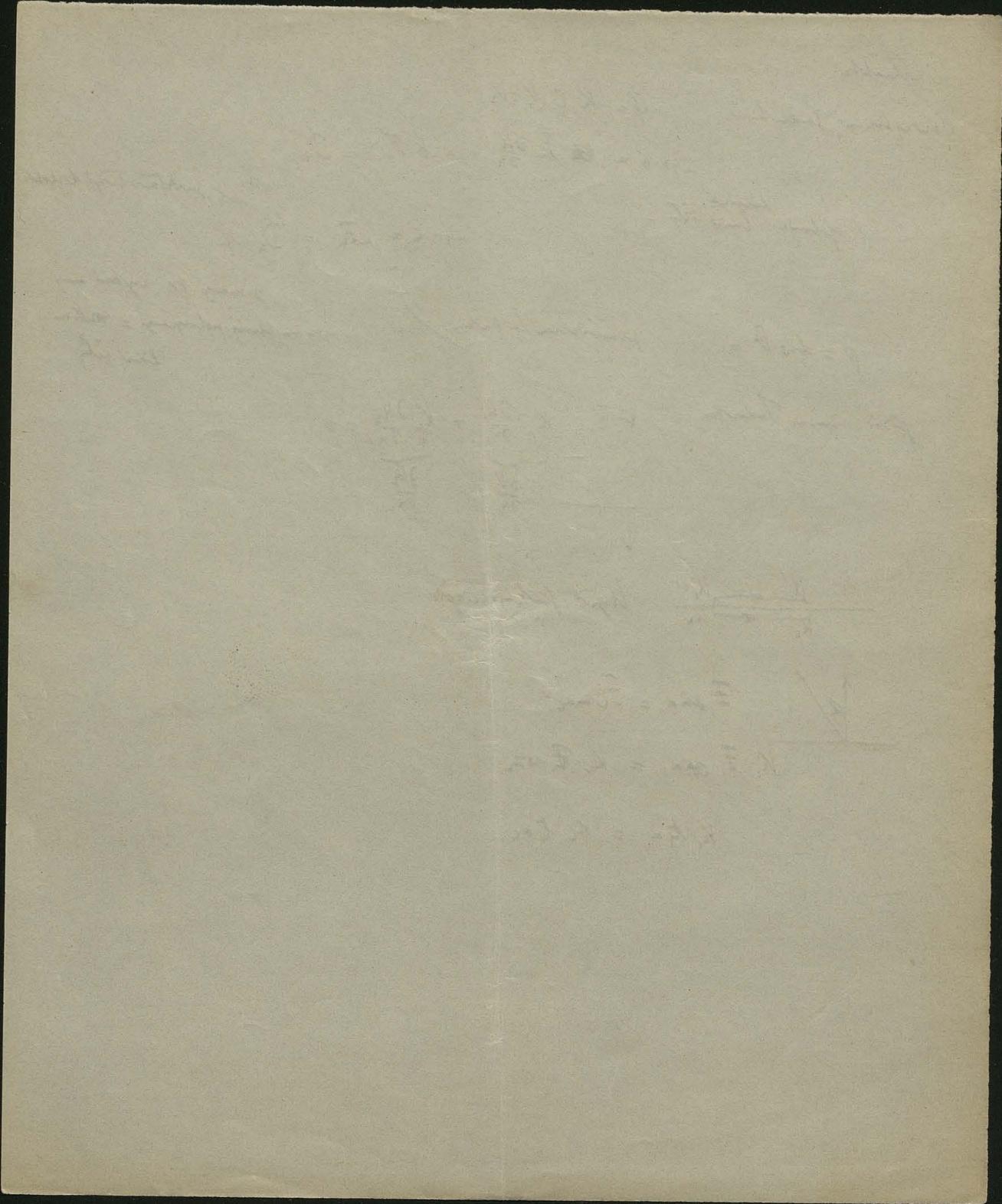
$$K_1 \frac{\partial U_1}{\partial n_1} + K_2 \frac{\partial U_2}{\partial n_2} = 0$$

Ujemne funkcja wagi

$$\begin{array}{c} \nearrow \\ z \end{array} \quad F_{\text{waga}} = F_{\text{mag}}$$

$$K_1 F_{\text{waga}1} = K_2 F_{\text{waga}2}$$

$$K_1 t_{\text{waga}1} = K_2 t_{\text{waga}2}$$



$$x' = \frac{x}{n} n' = \frac{x a^2}{n^2} =$$

$$y' = \frac{y a^2}{n^2}$$

$$z' = \dots$$

$$x = \frac{x' n}{n'} = \frac{x' a^2}{n^2}$$

N.p. kula:

$$(x'^2 - m^2) + y^2 + z^2 = n^2$$

$$\cancel{\frac{n^2}{a^2}} - \cancel{m^2}$$

$$\left( \frac{x' a^2}{n^2} - m \right)^2 + \left( \frac{y' a^2}{n^2} \right)^2 + \dots = n^2$$

~~Kula~~

$$x' a^2 -$$

$$\frac{x'^2 + y'^2 + z'^2}{n'^2} a^4 - 2m \frac{x' a^2}{n^2} + m^2 = n^2$$

}

$$a^4 - 2m x' a^2 + (m^2 - n^2)(x'^2 + y'^2 + z'^2) = 0$$

Kula legden zwon kulaq the.

$$\left[ x' - \frac{ma^2}{n^2 - m^2} \right]^2 + y'^2 + z'^2 = \frac{m^2 a^4}{(n^2 - m^2)} - \frac{a^4}{m^2 - n^2} = \frac{a^4 n^2}{(m^2 - n^2)^2}$$

N.p. Kula <sup>A</sup> zwongter 6

$$\text{Potency of } j_3 \text{ v punktek zwongter wongter wongter} = \frac{4\pi b A}{A} = \frac{E}{A}$$

$$\text{junks odrzonijung } j_3 \text{ v tui } \frac{1}{r} \text{ iu } dE = 6' df' = \frac{6df}{r} a$$

$$\text{to junks v punktek zwongter wongter wongter} = 4\pi b A \cdot \frac{a}{r}$$

$$\text{rotation } \omega = 0 \text{ junks v punktek o pugjumung read mass} - \frac{E a}{A}$$

$$\text{Tenu kula zwongter wongter} \rightarrow \delta' df' = \frac{df a}{r} \frac{E}{4\pi A^2}$$

Tuan junks stonuk df': df?

$$P'Q' = \frac{a^2}{rs} PQ \quad ds' = \frac{a^2 ds}{r^2}$$

$$df' = \frac{a^4}{r^4} df$$

It's known  
because in the  
hydro project we know

$$G' = \frac{a}{r} \frac{E}{4\pi A^2} \quad \frac{r^4}{a^4} = \frac{r^3}{a^3} \frac{E}{4\pi A^2} = \frac{a^3}{r^3} \frac{E}{4\pi A^2} = \frac{a^2 E'}{r^3 \cdot 4\pi A}$$

$A'$  = promi' kuli' niverting  
turbely jen u wypres' to jen  $A'$  th.

de wystarczaj na ty ujem reakcji je woj.  $\frac{1}{r^3}$

$$A' = \frac{a^2 A}{m^2 - A^2}$$

$$m' = \frac{m a^2}{m^2 - A^2}$$

$$G' = \frac{\cancel{E'}}{\cancel{r^3} \cdot 4\pi a}$$

$$\frac{A' h}{m'} = \frac{A}{m}$$

$$A' = \frac{a^2 \frac{A' m}{m}}{m^2 - A'^2 \frac{m}{m^2}}$$

$$m - \frac{m}{m'^2} A'^2 = \frac{a^2}{m'}$$

$$m = \frac{a^2}{m' \left[ 1 - \frac{A'^2}{m'^2} \right]} = \frac{a^2 m'}{m'^2 - A'^2}$$

$$A = \frac{a^2 A'}{m'^2 - A'^2}$$

$$\sigma = \frac{E'}{r^3 \cdot 4\pi} \left( \frac{m'^2 - A'^2}{A'} \right)$$



